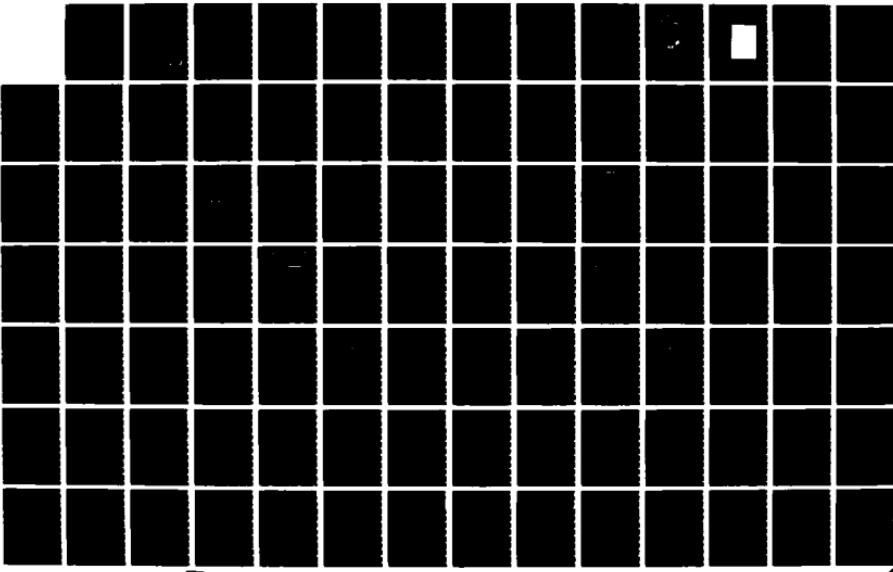


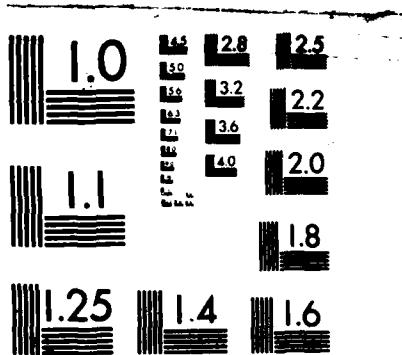
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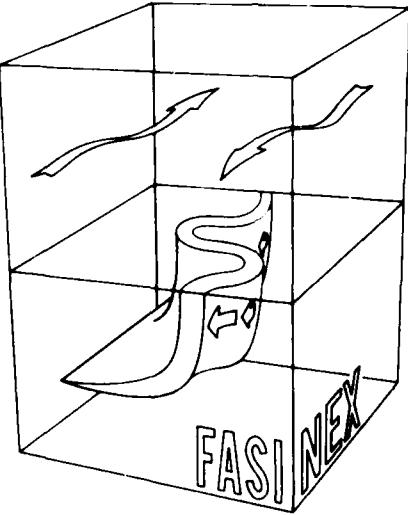
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FASINEX

(Frontal Air-Sea Interaction Experiment)

AD-A177 776



Cruise Summaries for FASINEX Phase Two

R/V Oceanus Cruise 175
R/V Endeavor Cruise 141

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Nancy J. Pennington
Robert A. Weller

October 1986

FASINEX Technical Report #14

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F A S I N E X
Frontal Air-Sea Interaction Experiment
(January - June 1986)

Cruise Summaries for FASINEX Phase Two

R/V OCEANUS Cruise 175
R/V ENDEAVOR Cruise 141

by

**Nancy J. Pennington
Robert A. Weller**

**Woods Hole Oceanographic Institution
Woods Hole, Massachusetts 02543**

October 1986

FASINEX Technical Report #14

**Funding was provided by the Office of Naval Research
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Robert C. Beardsley

**Robert C. Beardsley, Chairman
Department of Physical Oceanography**

Abstract

The Frontal Air-Sea Interaction Experiment (FASINEX) was a study of the response of the upper ocean to atmospheric forcing in the vicinity of an oceanic front in the subtropical convergence zone southwest of Bermuda, the response of the lower atmosphere in that vicinity to the oceanic front, and the associated two-way interaction between ocean and atmosphere. FASINEX began in the winter (January 1986), concluded in the early summer (June 1986) and included an intensive period in February and March. The experiment took place in the vicinity of 27°N, 70°W where sea-surface-temperature fronts are climatologically common.

Measurements were made from buoys, ships, aircraft and spacecraft. This report summarizes the shipboard work done on R/V OCEANUS and R/V ENDEAVOR during Phase Two, the dual ship/multi-aircraft measurement period. The two ships worked individually, jointly and as ground truth for the aircraft during the month. Each ship carried specialized instrumentation for measuring oceanographic and meteorological parameters. Information describing the sampling strategy, station positions and times are included. This report contains summaries of the data collected and some preliminary results.

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I. Introduction

The Frontal Air-Sea Interaction Experiment (FASINEX) (see Stage and Weller, Bulletin of the American Met. Soc., Vol 66, No.12, 1985 and Vol 67, No. 1, 1986 for further detail on the background scientific objectives, and the experimental plan of FASINEX) was planned to investigate local air-sea interaction processes at an oceanic front. North of about 25°N in the mid-Atlantic Ocean the prevailing westerly winds tend to carry the surface water to the south. South of about 25°N the trade winds carry surface water to the north. In the region southwest of Bermuda the cooler water from the north meets the warmer water from the south, a series of oceanic fronts are formed. The fronts are marked at the surface by abrupt changes in sea surface temperature. The surface temperature may change by as much as 3°C in less than a kilometer. Associated with these fronts are surface currents with speeds of approximately 1.5 knots.

The FASINEX field experiment began on January 7, 1986 when R/V KNORR sailed on cruise 119. This was designated FASINEX Phase One, the mooring deployment cruise. Once a sea surface temperature front was located by satellite imagery and an extensive XBT survey, the mooring instrumentation was set, and began recording and telemetering data. Meteorological and oceanographic logs were maintained. Phase Two immediately followed the one month deployment cruise. R/V OCEANUS and R/V ENDEAVOR returned to the FASINEX area to make oceanographic and meteorological measurements for approximately another month. During this time period, six aircraft including the NRL P3, NASA C-130, NCAR Electra, NASA P3, NOAA P3, and NASA Electra completed 41 flights measuring atmospheric and oceanic conditions. Phase Three, the mooring recovery cruise, KNORR 123, returned to the FASINEX area in early June 1986. The instrumentation that recorded data on station for the six month period was retrieved. Meteorological and oceanographic logs were again maintained. The field program ended with the ship returning to Woods Hole. The Phase Two cruises are summarized in this report. The summary of Phases One and Three is WHOI Report #86-35 (FASINEX Document #13). Figure One shows an artist's concept of the mooring array bracketing a frontal feature and the joint work of the ships and aircraft during the one month of intensive scientific measurements.

The overall goals of the ship and aircraft scientists during FASINEX were:

1. To describe the horizontal and vertical structures of the oceanic and atmospheric boundary layers in the region in and around an oceanic front.
2. To investigate the relation between structures found on each side of the air-sea interface.
3. To study the physical processes associated with air-sea interaction in the vicinity of an oceanic front.

During Phase Two, the ships and aircraft worked jointly to measure with high resolution, over a limited time, the temporal and spatial variability of a frontal feature and investigate the processes acting within the front. The ships primary goal was to observe and characterize the three dimensional

and across frontal features. The meteorological goals were to collect sections (radiosonde and atmospheric sounder) perpendicular and parallel to the front, and to make stress measurements in the vicinity of the moored array; both these efforts were done in conjunction with the aircraft flights. This report will summarize only the shipboard work done during Phase Two.

Scientific goals dictated that the field work during Phase Two focus on an oceanic front, so the area of interest shifted to the position of a nearby front rather than remain at the moorings set during Phase One. The frontal feature studied was the same one that moved northeast from the central mooring array. At the conclusion of Phase Two, a final survey south to the mooring array area showed that another front had moved into the area. The characteristics of this front were very different from the original front located in the same area. (Throughout the six month experiment, frontal features moved through the central array. This is clear from the SST signal seen by the buoy instrumentation.)

A brief description of the instrumentation on both ships and its capabilities will serve as an overview of the oceanographic and meteorological parameters measured during Phase Two. Within this report, participant summaries are included when available.

OCEANUS surveyed the frontal region with an underway Doppler Log. SST and velocity profiles were collected for all but 2 days of the 26 days the ship was in the FASINEX region. Continuous SST was measured by the ship's SAIL (Serial ASCII Interface Loop) system. A thermosalinograph also continuously recorded surface temperature and salinity. Fifteen minute buckets were taken as part of an underway oceanographic watch. Hourly salinity samples were taken. For approximately 17 days of the cruise the SeaSoar gathered temperature, salinity and oxygen data in a range from 30-350 m while the ship steamed at 8 kts. This instrument output a real time display and with software on board a large scale picture of the front was available with 24 hours of the survey. A real time profiler (RTP) section was made across the front. The profiler measured u,v and w components of velocity along with temperature and conductivity. Two forms of drifters were used on OCEANUS. Neutrally buoyant drifting Vertical Current Meters (VCM) which measured pressure, temperature and turns (allowing for a vertical displacement calculation) and Scripps' surface and 50 m drogued drifters which measured surface and nearsurface currents. CTD stations were taken in the vicinity of the moorings as a last task of the cruise before the ship headed back to Woods Hole. Radiosondes were taken as part of Ken Davidson's meteorological program on both ships.

ENDEAVOR gathered oceanographic data with two profilers. A newly designed free fall microprofiler made 39 dives. The instrument measured temperature, conductivity and pressure (using a standard CTD unit), small scale temperature, conductivity and velocity with special microstructure probes, fine scale velocity variations with acoustic current meters and accelerometers. EPSONDE, another small scale profiler operated in a tethered free fall mode, transmitting its measured parameters to the surface using a kelvar multiconductor line. This instrument completed 39 stations, doing multiple profiles at each position. It measured microstructure velocity fluctuations, temperature gradient microstructure and mean temperature,

conductivity and pressure. XBT surveys were run to locate the front. A total of 70 CTD stations were completed, including a section in conjunction with an overpass by GEOSAT. A WOTAN (Wind observation through Ambient Noise) drifting mooring was deployed 12 times. It carried four different transducers to measure acoustic backscatter and a WOTAN measuring bubble clouds. Underway meteorological data was collected using the ship's SAIL system. A Doppler log operated during part of the cruise.

Although this is a cruise/data report for the shipboard work, the timing of the aircraft overflights is included. Most flight days the joint work required the ships' positioning themselves on opposite sides of the front and heading into the wind measuring meteorological data for ground truth. Communication was maintained with VHF radios when the aircraft were in the FASINEX area.

Total Flights: 41

NRL P3	12
NASA C130	11
NCAR Electra	7
NASA P3	5
NOAA P3	4
NASA Electra	2

Feb 10 NRL P3

14	NRL P3
16	NRL P3, NCAR Electra, NOAA P3
17	NRL P3, NCAR Electra, NOAA P3
18	NRL P3, NCAR Electra, NASA C130, NASA P3
20	NCAR Electra, NASA C130, NASA P3, NASA Electra, NOAA P3
21	NCAR Electra, NASA C130, NASA P3, NASA Electra, NOAA P3
22	NASA C130
24	NCAR Electra, NASA C130, NASA P3
25	NRL P3, NCAR Electra
26	NRL P3, NASA C130, NASA P3

Mar 1 NRL P3, NASA C130

3	NRL P3, NASA C130
5	NRL P3, NASA C130
7	NRL P3, NASA C130
8	NASA C130
9	NRL P3

Communication was maintained via two one hour sessions daily on the ATS system. Charlie Eriksen manned the FASINEX office at the Bermuda Biological Station for the month long Phase Two. Aircraft scientists, based in Bermuda at the Naval Airstation, either relayed information through Charlie or coordinated flight plans with the ships during the evening FASINEX hour by stopping by the office to discuss upcoming flights with the ships. This allowed for daily updates of the field work.

The numerous sampling patterns used by the two ships and six aircraft allowed for many different data sets to be gathered under different oceanographic and atmospheric conditions during the field program. Until data sets are shared and intercomparisons made, it will be difficult to draw a conclusion of the overall success of the experiment, but because of the variability of the oceanographic and atmospheric conditions, the successful coordination among the aircraft with their complex joint work and with the ships, and the data return from the instrumentation on the ships, aircraft and buoys, the field program accomplished all the tasks scheduled.

The FASINEX area was designated to be a four by five degree box southwest of Bermuda. The coordinates are 25° to 30° North and 72° to 68° West. Two charts are used in this data report. FASINEX Total Area (Figure 2) includes the East Coast and Bermuda to identify the area of the western Atlantic. Area 1 (Figure 3) is an expanded scale of one section of the Total Area chosen to include all the oceanographic and meteorological sampling done by the ships involved in all three phases of FASINEX. A solid square identifies the central mooring array location at approximately 27° N, 70° W.

The fronts seen in the AVHRR images and the underway oceanographic sampling make up the Figure 3 composite plot. The front locations for January 6-7 and January 21-22 were taken from AVHRR images. Bucket temperature data from the OCEANUS 175 radiator pattern were used for the February 15 front location. The locations for the February 27 and March 4 frontal positions were also taken from the 15 minute bucket temperatures on OCEANUS.

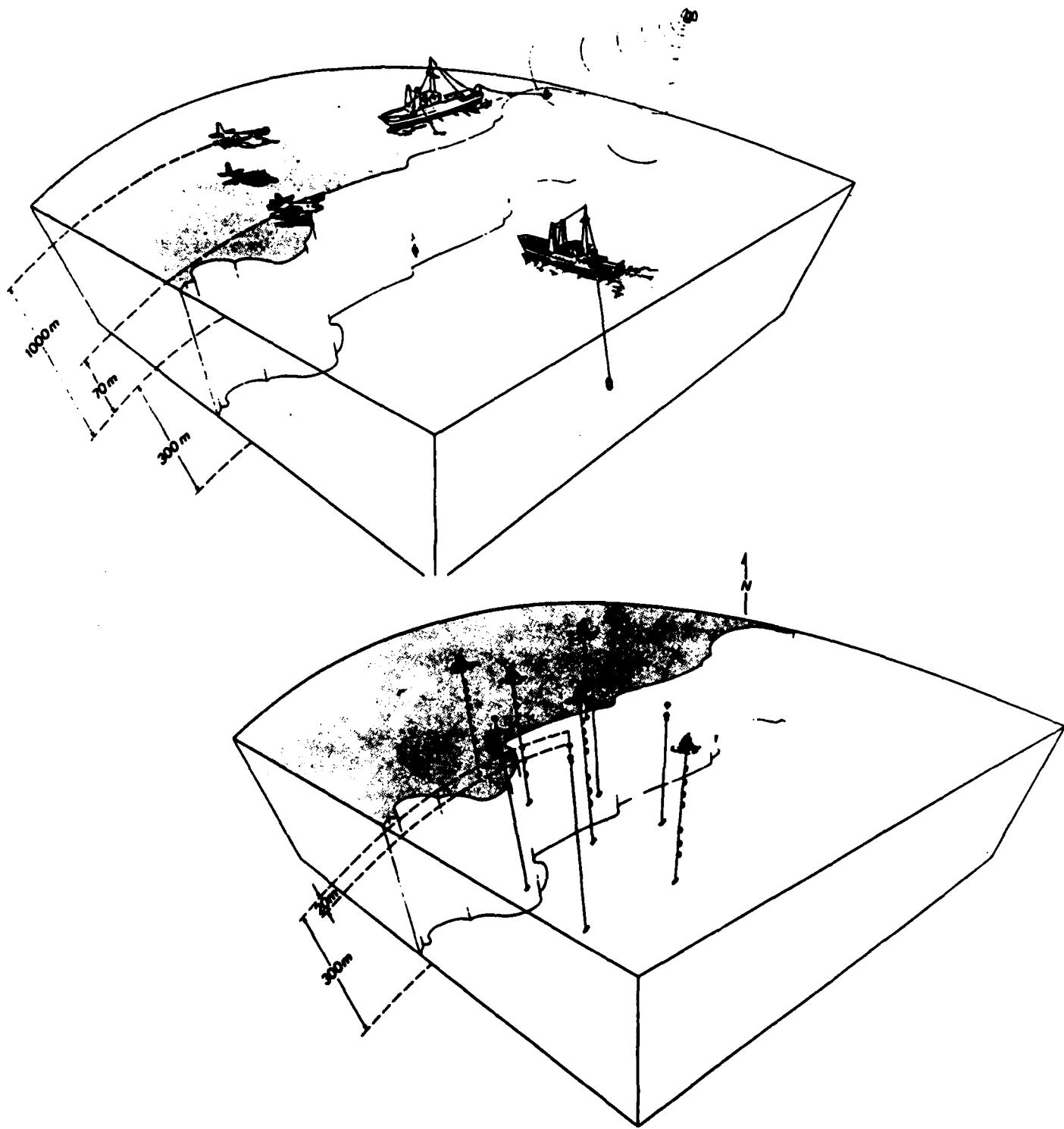
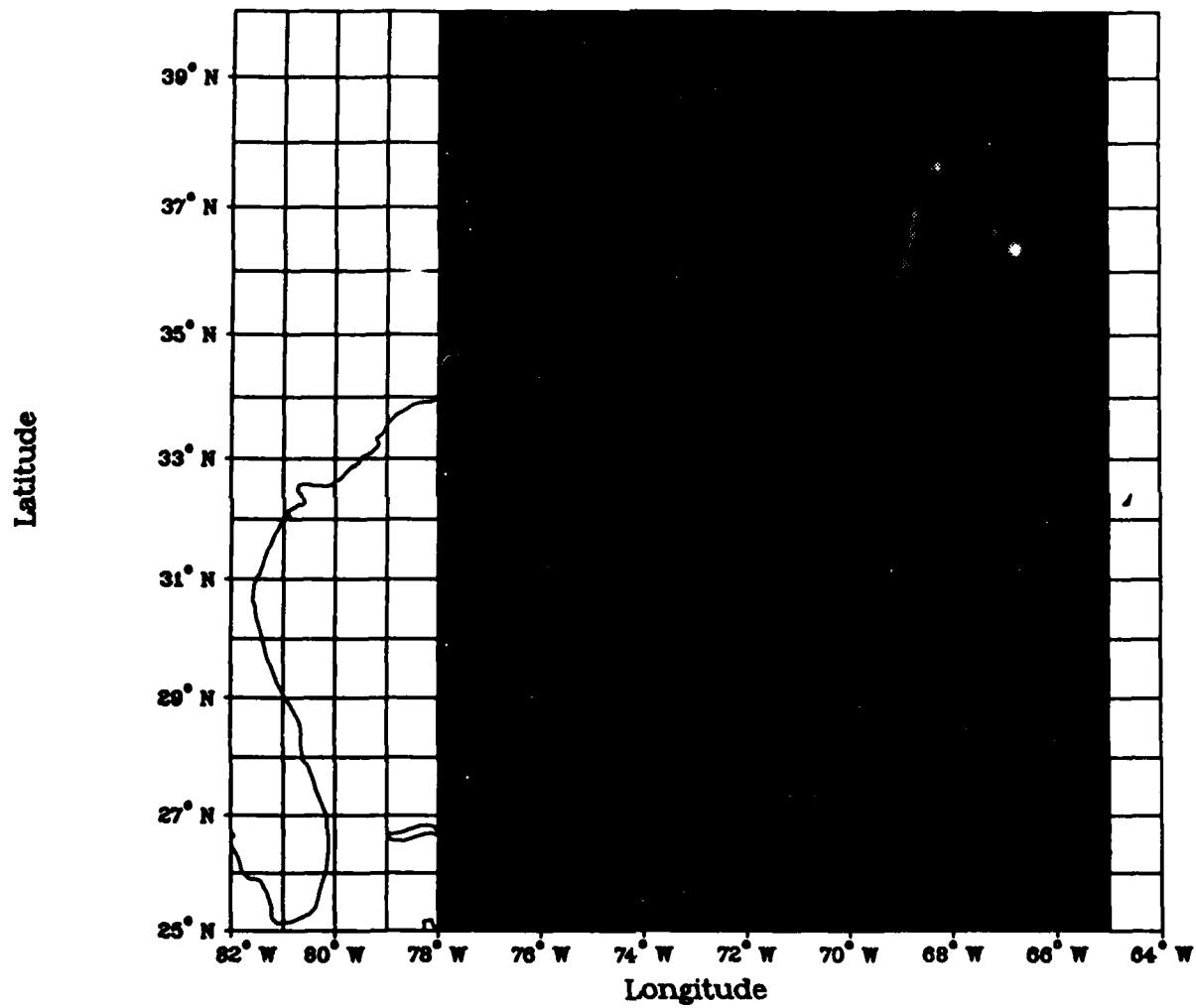


Figure 1. Artist's conception of frontal regions during Phase One, the mooring work (lower), and Phase Two, the intensive scientific period (upper).

FASINEX Total Area**Figure 2**

FASINEX Frontal Positions

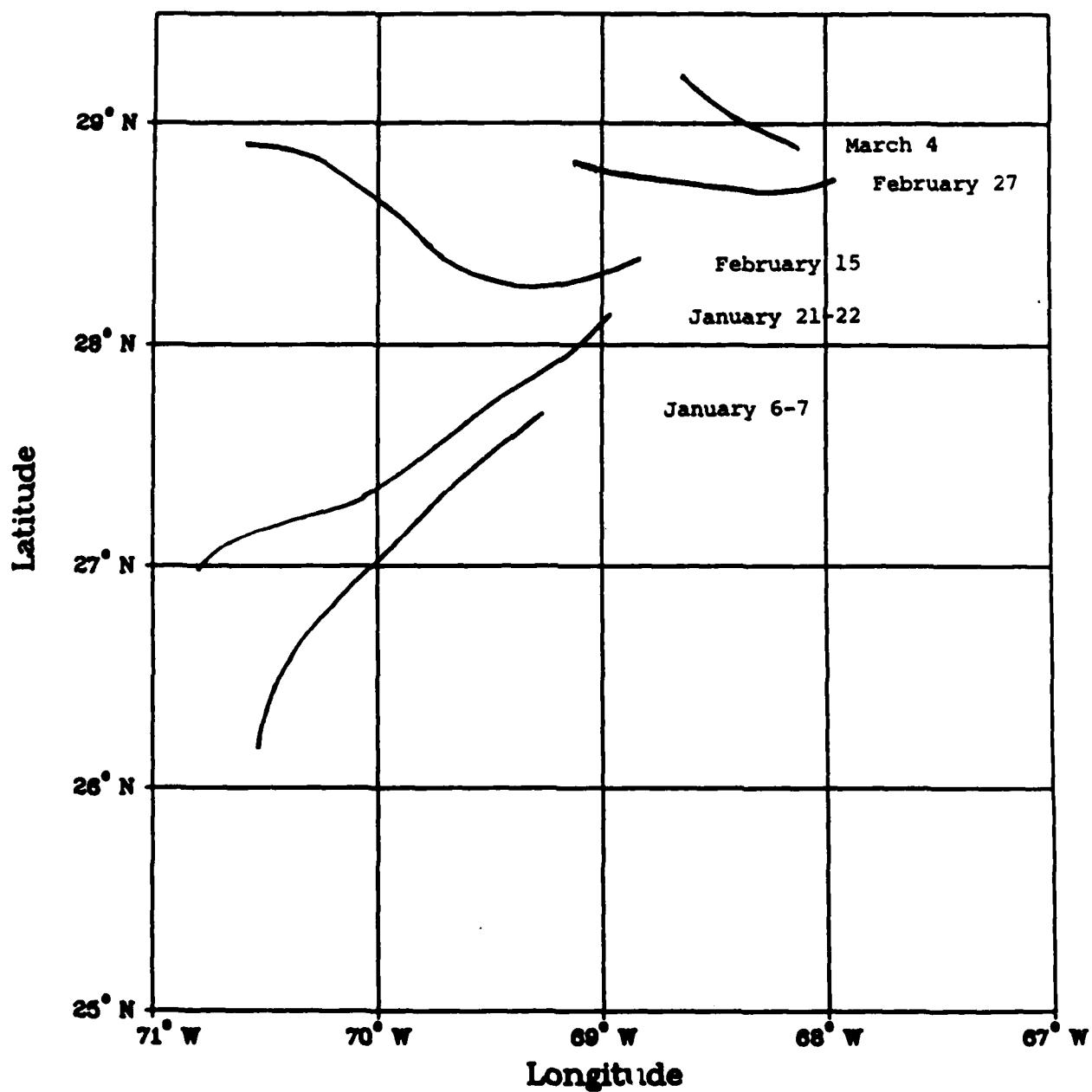


Figure 3: Area 1 showing Frontal Positions.

II. Cruise Narrative - OCEANUS 175

a. Summary

OCEANUS sailed on February 5, 1986 for Bermuda to rendezvous with ENDEAVOR and several members of the KNORR (Phase One) scientific party. Because of steering problems, she returned to Woods Hole and was delayed three days while repairs were completed. She departed again on February 8 and arrived at St Georges, Bermuda on February 11. Scientists on board during the transit set up the main lab and tested instrumentation. When the ship arrived at the dock, the party transferring from KNORR immediately loaded their gear, so the ship was ready to sail early on the February 12. Due to a delay of an air-shipped IC for a computer on ENDEAVOR, the OCEANUS did not sail until 1900.

A watch was started at 1600 on February 13. The oceanographic underway log that was maintained during the cruise included time, LORAN C latitude and longitude, bucket sea surface temperature (SST), SAIL SST, and towed fish SST. During specific times, thermosalinograph SST and SeaSoar mixed layer depth and temperature were recorded. A half hour meteorological log including time, LORAN C latitude and longitude, wind speed and direction, barometric pressure, and dew point (wet and dry bulb temperatures) was maintained throughout the cruise.

The ship arrived in the FASINEX area where ENDEAVOR had located a strong frontal feature late on February 13. This location was approximately 60 miles north of the moored array. Because of rough seas and high winds, the SeaSoar was deployed to run a survey down south to box in the moored array looking for any features that might be present but did not show on the satellite imagery. This survey took 48 hours. During that time the first overpass of the NRL P3 took place. The SeaSoar was hauled just before rendezvousing with ENDEAVOR on February 15 to transfer some XBTs, the computer IC chip and some data.

Balloon launches began on February 13. OCEANUS and ENDEAVOR alternated launching radiosondes. Five to seven balloons were launched each day between the two ships, with additional launches on aircraft days.

On February 16 at 1413, a second SeaSoar survey began while the ENDEAVOR tow-yoed in the front. An eight leg radiator pattern was run to locate the front and measure its scale and orientation. This survey continued until February 20. At that time a bucket survey was started to locate the front for deployment of the SIO drifters and the VCMs. For five days, SIO drifters and VCMs were tracked. Three different deployments of the expendable drifters were made. Each deployment consisted of eight instruments, four surface and four 50 meter drogues. The VCMs were deployed twice. The first 50 hour experiment involved two instruments ballasted to 140 and 90m. The second deployment involved three VCMs ballasted to 150, 95, and 175m. The VCMs were recovered by 2000 on February 25.

During the drifter/VCM tracking, ENDEAVOR and OCEANUS rendezvoused on February 26. Six members of the ENDEAVOR scientific party, came aboard for a meeting to discuss the work completed and plans for the final week and a half.

Joint shipboard work was scheduled for the remainder of the cruises. SeaSoar was again deployed at 2000 on February 26. A diamond shaped pattern enclosing a sharp front was begun, while ENDEAVOR steamed parallel inside the diamond. This survey ran for only six hours, until ENDEAVOR reported that the front had moved farther east. OCEANUS still surveying with the SeaSoar steamed south to box in the mooring array finishing the pattern at 0800 March 1. An RTP section was started, but after three stations was aborted because of rough seas and high winds. Once again the SeaSoar was launched at 1600. During the next 36 hours, the mate reported 15-18 foot seas, and wind gusts to 50 kts with the ship taking 30° rolls while SeaSoar continued an elongated box survey. During this time, ENDEAVOR was hove-to after tow-yoing and microstructure profiling inside the box of OCEANUS' survey.

With the weather improving, an RTP survey was begun on March 4. This survey ran south-southwest to north-northeast. Fourteen stations were completed crossing the front. XBTs were done in conjunction with the RTP survey.

The buoys set during Phase One in the vicinity of 27°N, 70°W telemetered position and meteorological data. One of the buoys F10 had an intermittent problem and infrequently updated its position. Because of the length of time the buoys were to remain on station, this position information was very important for monitoring purposes. The decision was made to borrow a spare ARGOS transmitter from ENDEAVOR, to use on Buoy D in the mooring array. (A third and final rendezvous took place to pass the transmitter over.) On March 6, the OCEANUS returned to the central array to install this duplicate transmitter. While down south in the mooring area, all the buoys were visually checked. SeaSoar was deployed the final time to survey a box around the moorings on March 6. A frontal feature with unique salinity characteristics was mapped. Six CTD stations were taken in the area of the moorings before the ship headed back to Woods Hole. OCEANUS left the FASINEX area on March 9 ending FASINEX Phase Two. The ship returned to Woods Hole on March 12.

b. Schedule Overview

5 February 1986	Depart for Bermuda/ Return to Woods Hole with steering problems
8 February	Depart for Bermuda
11 February	Arrive Bermuda
12 February	Depart St. Georges Bermuda
13 February	Arrive FASINEX area
8 March	Depart FASINEX area
12 March	Arrive Woods Hole

Science Party - Woods Hole to Bermuda

1. Pollard, Raymond, Co-Chief Scientist, IOS
2. Regier, Lloyd, Co-Chief Scientist, SIO
3. Smithers, John, Scientific Officer, IOS
4. Jackson, Christopher, Computer Specialist, NERC
5. Lewis, Derek, Computer Engineer, NERC
6. Potter, Kay, Computer Programmer, NERC
7. Lind, Richard, Research Meteorologist, UW
8. Vaucher, Chris, Technician, NPGS
9. Spencer, Eric, Safety Officer, WHOI

Science Party - FASINEX Phase Two

1. Waller, Robert, Chief Scientist, WHOI
2. Pollard, Raymond, Scientist, IOS
3. Regier, Lloyd, Scientist, SIO
4. Davidson, Ken, Scientist, NPGS
5. Payne, Richard, Research Associate, WHOI
6. Dean, Jerome, Research Specialist, WHOI
7. Pennington, Nancy, Sr. Research Assistant, WHOI
8. Light, Christina, Research Assistant, WHOI
9. Guest, Brian, Research Assistant, WHOI
10. Smithers, John, Scientific officer, IOS
11. Lewis, Derek, Computer Engineer, NERC
12. Dufor, James, Development Engineer, SIO

WHOI	Woods Hole Oceanographic Institution
IOS	Institute of Oceanographic Sciences, England
SIO	Scripps Institution of Oceanography
NPGS	Naval Postgraduate School
UW	University of Washington
NERC	Natural Environment Research Council, England

c. Chronological Log for OCEANUS 175

Feb 05 Depart Woods Hole/Return with Steering Problems

08 Depart Woods Hole for Bermuda

11 Arrive St. Georges, Bermuda

12 Depart St. George's, Bermuda for FASINEX Area

13 1600 Launch SeaSoar

14

15 Transfer equipment to ENDEAVOR
Meteorological calibration between ships

16

17

18 Recover SeaSoar 1200
Deploy SeaSoar 1600

19

20 Recover SeaSoar 0400
Deploy SCRIPPS Drifters Deploy VCMs
Tracking

21

22 Recover/Deploy VCMs

23 ENDEAVOR Party aboard

24

25 Deploy SeaSoar 1600 Recover VCMs

26

27

28

Mar 01 Recover SeaSoar 0400

cont.

- Mar 01 RTP #1-#3
 Deploy SeaSoar 1300

02 Recover SeaSoar 2130
 Deploy SeaSoar 2330

03
04 Recover SeaSoar 0900
 RTP #4-#7

05 RTP #8-#14
 ENDEAVOR rendezvous for transmitter
06 Check Buoys D, B, C
 Install Buoy D transmitter
 Deploy SeaSoar

07
08 Recover SeaSoar 0900
 CTD Stations #1-#5
09 CTD Station #6
 Woods Hole transit
10
11
12 Arrive Woods Hole

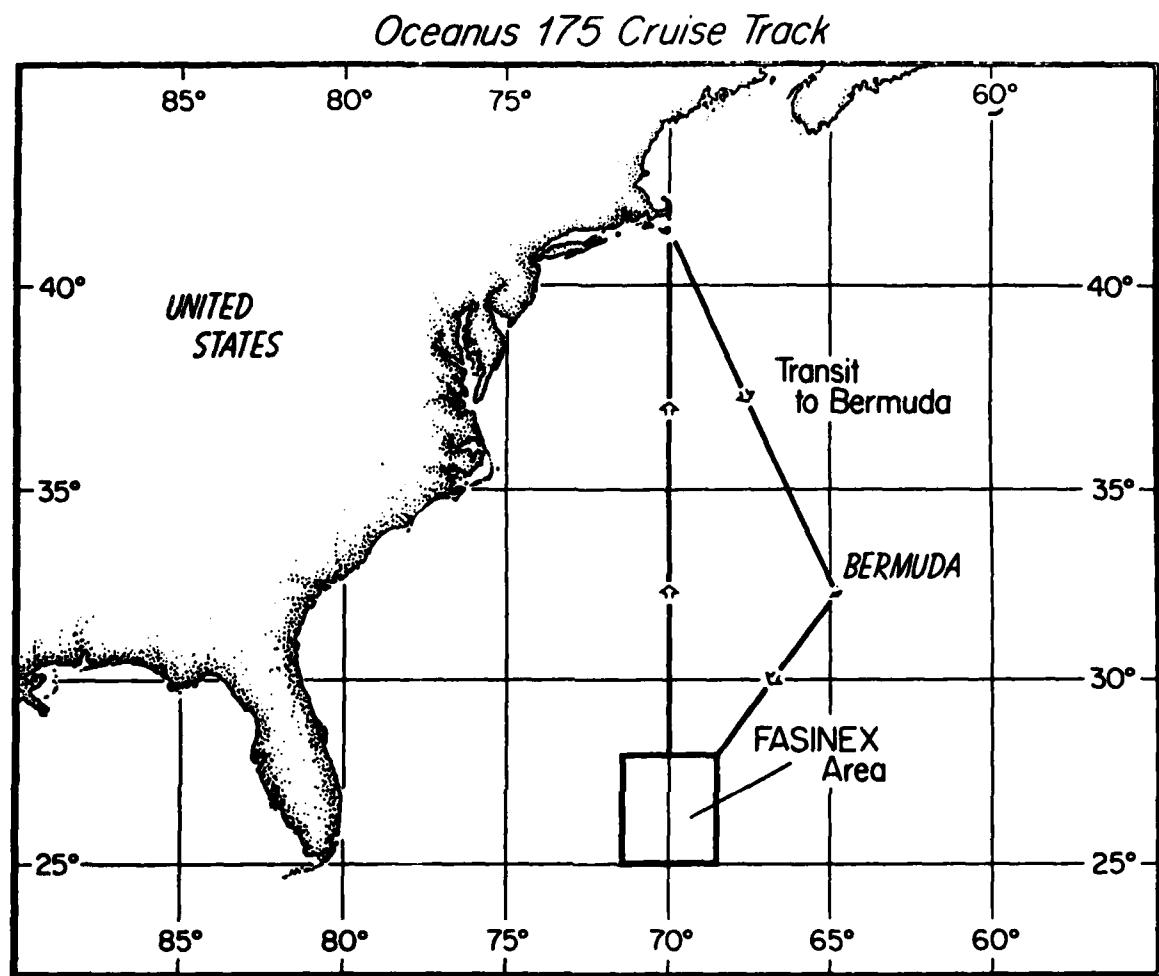


Figure II-1: Cruise track.

III. FASINEX Moored Array

The oceanic front is a three-dimensional feature with temporal as well as spatial variability. In contrast to the aircraft and ship operations, which provided high resolution views over a limited time, the moored array used self-contained surface and subsurface instruments to obtain a longer running view from a small number of fixed locations. Over the 6-month period the fronts moved through the center of the moored array so that moored instruments returned observations from a variety of environments (in the front, out of the front; under various meteorological conditions) as well as during the transition from winter, when the SST jump is large, to summer, when the SST signal associated with the front fades.

The 6-month array was composed of surface moorings and PCM moorings. The longer duration moorings set by Brink in October 1984 were subsurface moorings.

Phases One and Three of FASINEX consisted mainly of mooring work, with some additional survey work. A summary of the mooring cruises, KNORR 119, the deployment cruise and KNORR 123, the recovery cruise is available in another data report, WHOI Technical Report 86-35 (FASINEX Report #13).

The data from the moored array will be presented in a later data report.

Figure III-1

FASINEX Mooring Schematics

Figure III-2

Anchor Positions of Moorings

Table III-1

GPS/LORAN C Positions of Anchors

Figure III-3

Phase Two Time Period Wind Data from F6

(Davidson 3-day expanded scale plots)

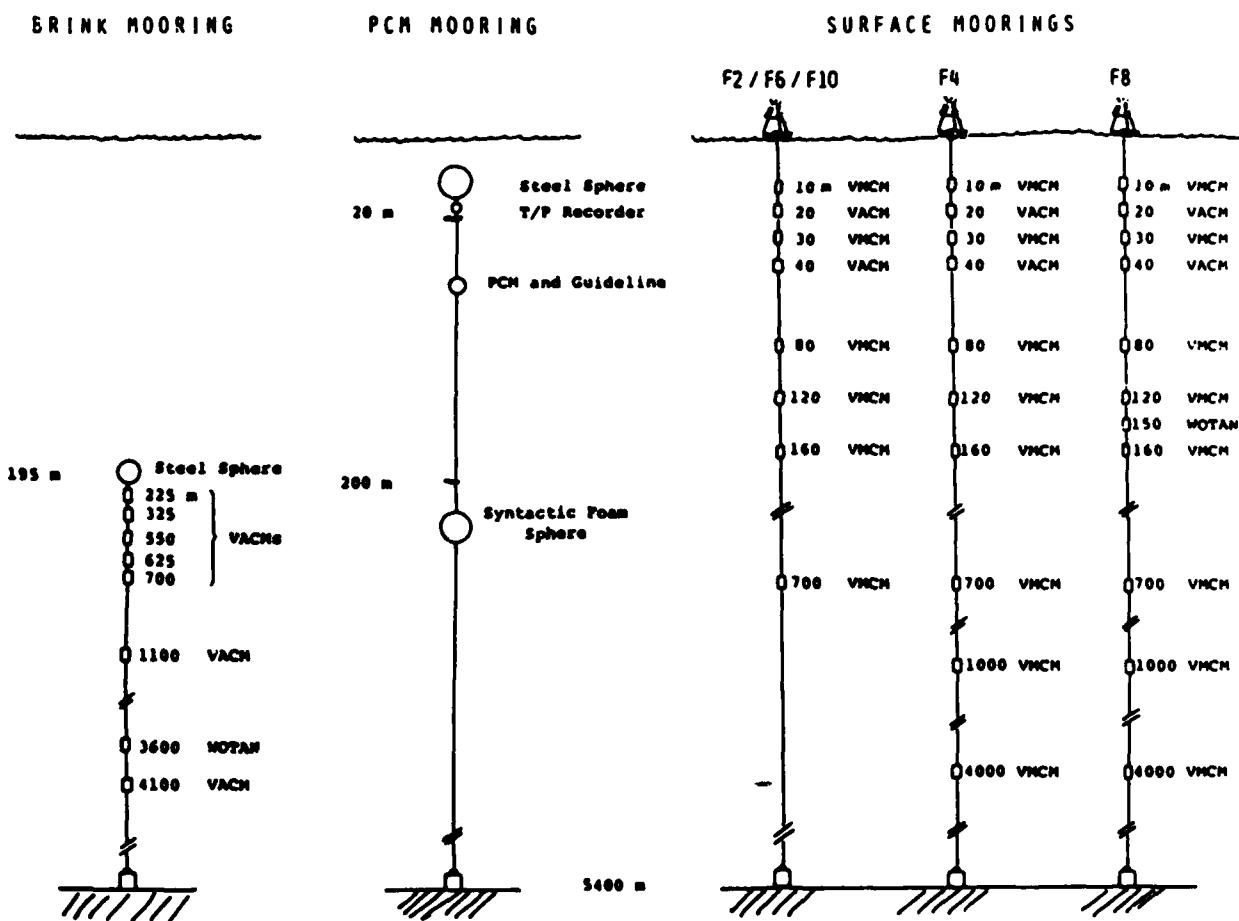
FASINEX

Figure III-1: FASINEX Mooring Schematics.

FASINEX Mooring Anchor Positions

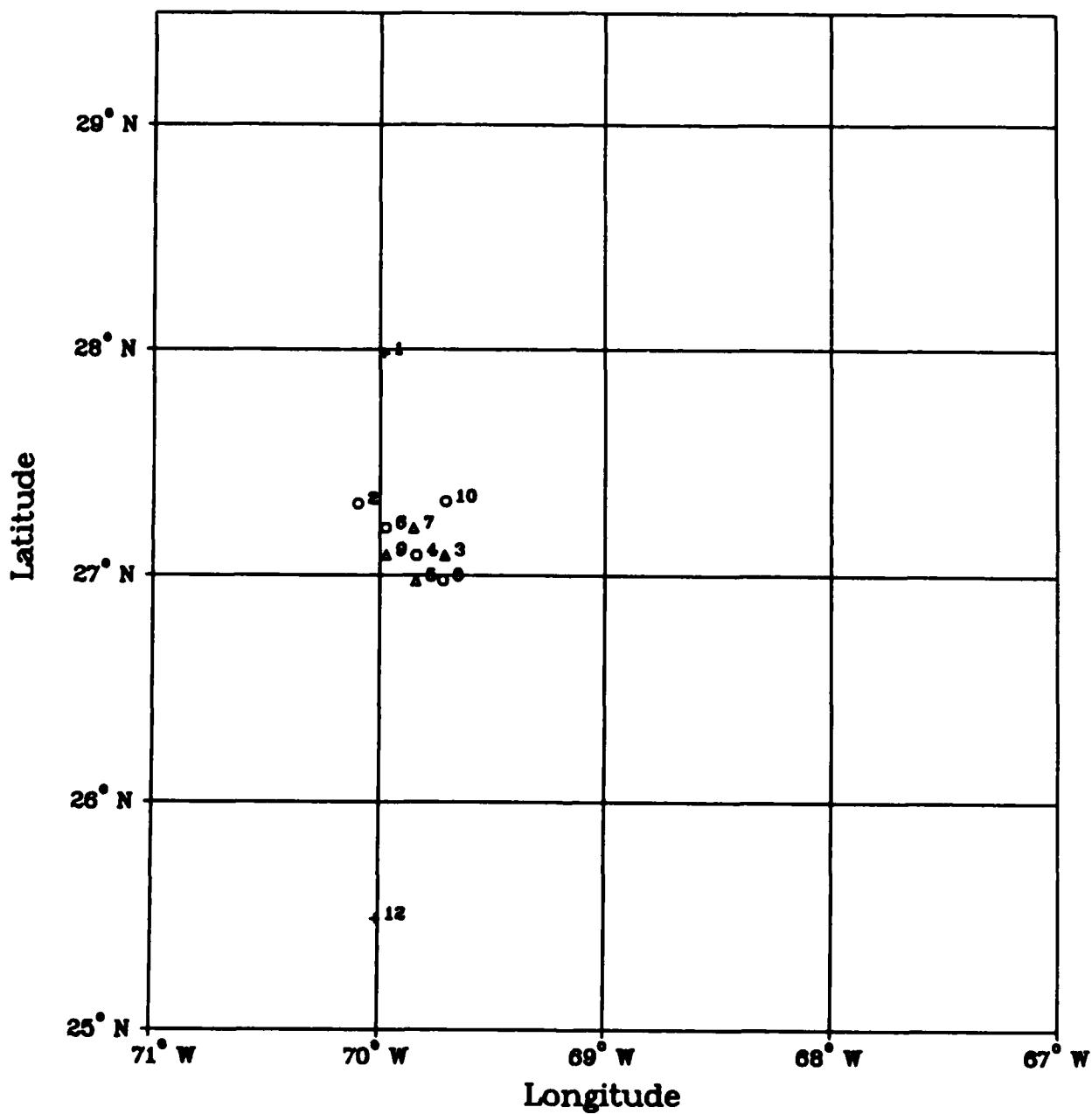


Figure III-2: Anchor Positions of Moorings.

GPS ANCHOR POSITIONS

FASINEX Designation	Visible Identifier	Lat/Lon	WHOI Mooring #
F2	A	27°18.95'N 70°05.86'W	845
F3		27°05.34'N 69°42.75'W	PCM-1
F4	C	27°05.35'N 69°50.30'W	846
F5		26°58.58'N 69°50.40'W	PCM-2
F6	B	27°12.59'N 69°58.48'W	847
F7		27°12.53'N 69°51.03'W	PCM-3
F8	E	26°58.66'N 69°43.19'W	848
F9		27°05.45'N 69°58.33'W	PCM-4
F10	D	27°19.63'N 69°42.52'W	849

Ken Brink's two year subsurface moorings (LORAN C positions)

F1	27°58.90'N 69°58.80'W	829
F12	25°29.10'N 70°00.70'W	830

Table III-1: GPS/LORAN C Positions of Anchors.

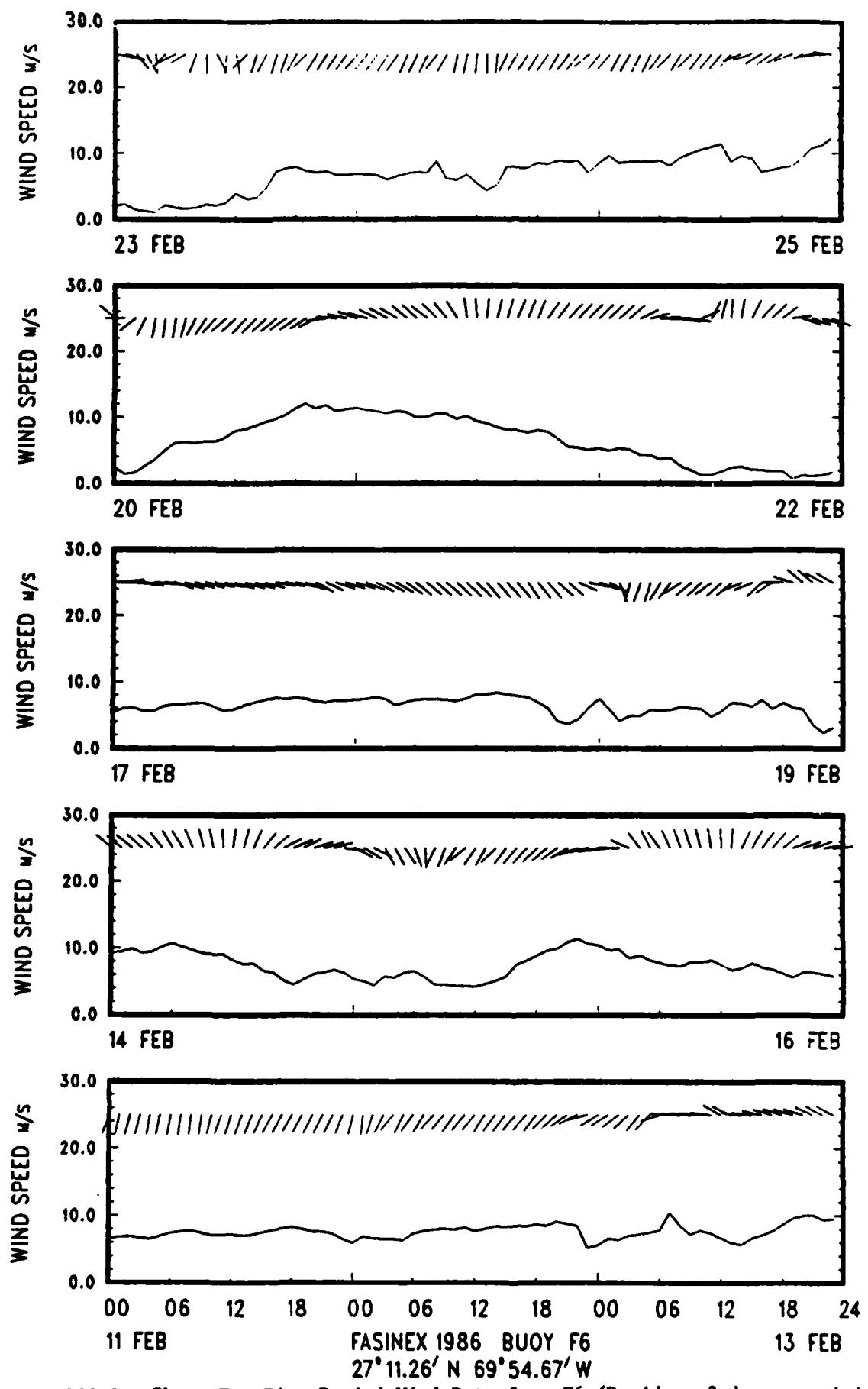


Figure III-3: Phase Two Time Period Wind Data from F6 (Davidson 3-day expanded scale plots).

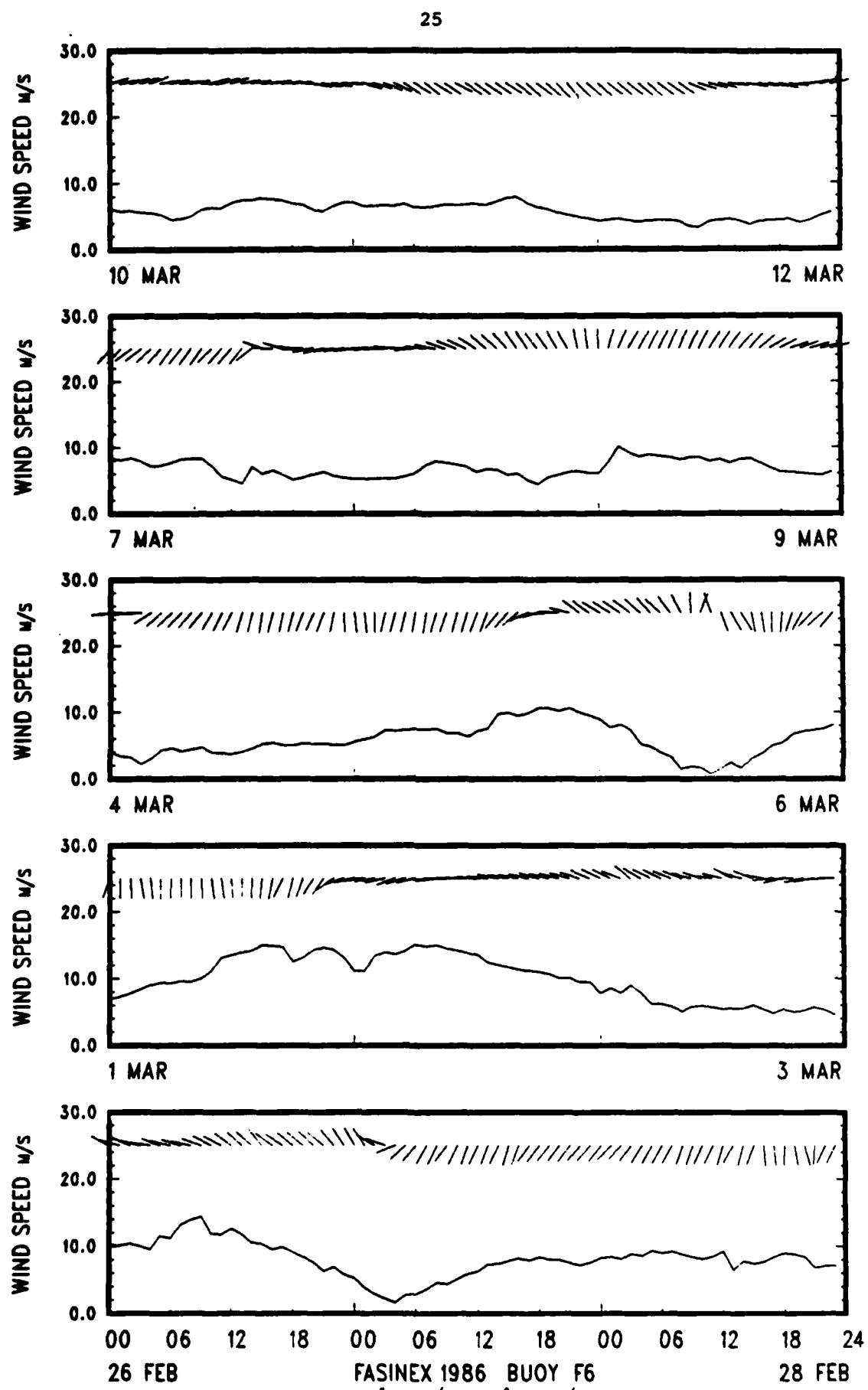


Figure III-3 (Continued)

IV. FASINEX XBT Data

During Phase Two, one XBT section was completed on OCEANUS. The survey was taken in conjunction with the RTP stations which ran from the south to the north crossing the front at approximately $29^{\circ} 04.09'N$ $67^{\circ}53.49'W$ on March 4-5.

The data were plotted on a strip chart recorder, but due to a malfunction only several profiles were written to a Bathysystem Recorder cassette.

Figure IV-1 Total XBT Pattern
Table IV-1 XBT Time and Position

(See RTP temperature section - XBT/RTP used for data set.)

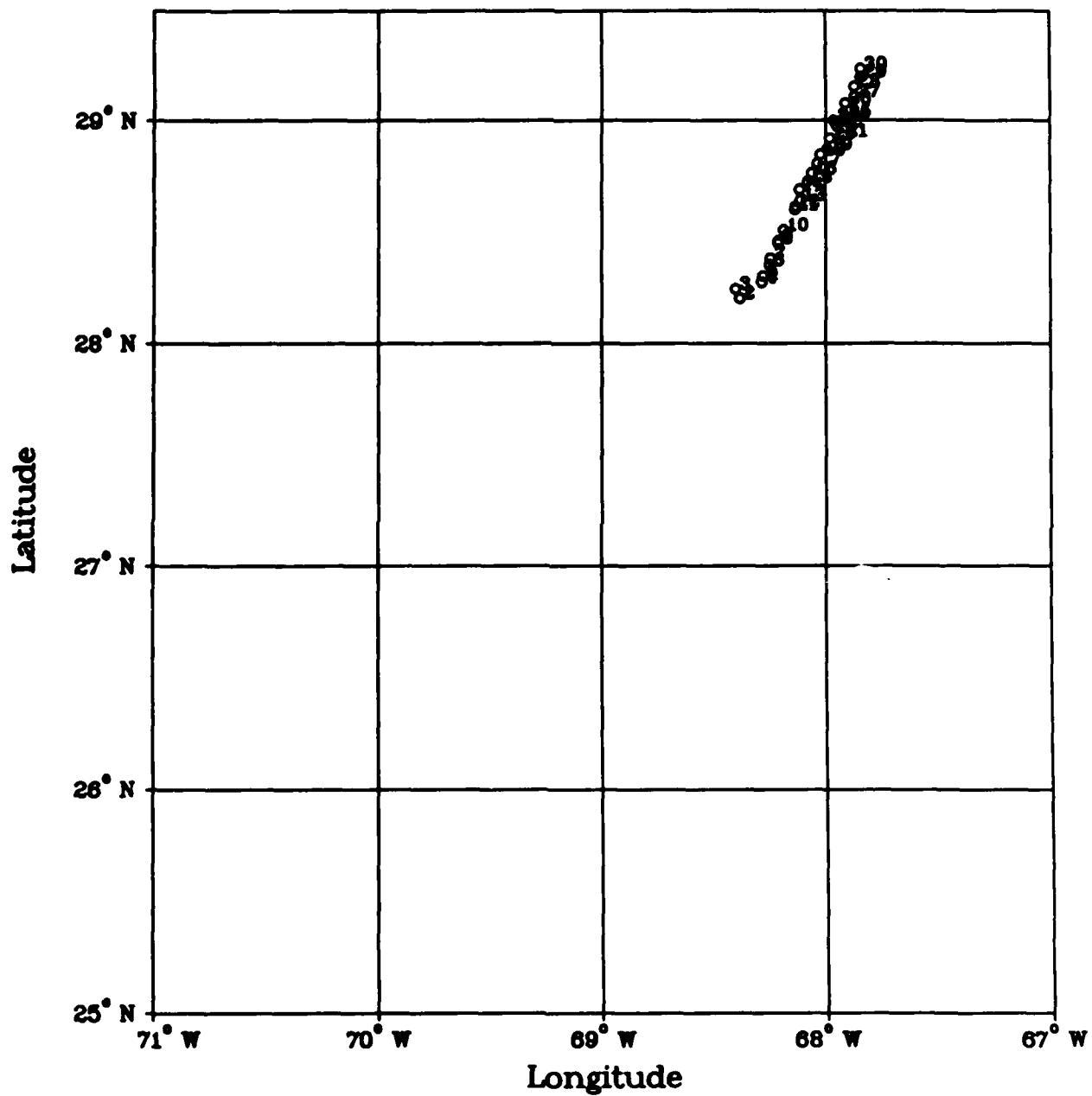
FASINEX Oceanus 175 XBT Section

Figure IV-1: Total XBT Pattern.

OCEANUS 175 XBT STATIONS

XBT#	TIME	DAY/MONTH	LATITUDE	LONGITUDE
1	1337	1 Mar	28°12.10	68°23.10
2	1435	1 Mar	28°12.17	68°22.96
3	1508	1 Mar	28°14.68	68°24.15
4	1627	4 Mar	28°16.43	68°17.16
5	1641	4 Mar	28°18.17	68°16.77
6	1825	4 Mar	28°21.19	68°15.00
7	1839	4 Mar	28°22.93	68°14.78
8	2024	4 Mar	28°27.01	68°12.81
9	2030	4 Mar	28°27.63	68°12.78
10	2145	4 Mar	28°30.59	68°11.28
11	0009	5 Mar	28°36.05	68°08.20
12	0015	5 Mar	28°36.89	68°08.06
13	0222	5 Mar	28°38.66	68°06.75
14	0244	5 Mar	28°41.48	68°06.93
15	0440	5 Mar	28°43.52	68°04.85
16	0458	5 Mar	28°45.88	68°03.70
17	0635	5 Mar	28°48.51	68°02.15
18	0651	5 Mar	28°50.84	68°01.39
19	0834	5 Mar	28°52.30	67°59.45
20	0855	5 Mar	28°55.23	67°58.83
21	1114	5 Mar	28°55.83	67°55.29
22	1132	5 Mar	28°58.55	67°57.04
23	1144	5 Mar	29°00.08	67°57.85
24	1333	5 Mar	29°00.18	67°54.77
25	1339	5 Mar	29°00.96	67°54.86
26	1533	5 Mar	29°04.68	67°54.80
27	1700	5 Mar	29°06.56	67°52.28
28	1720	5 Mar	29°09.29	67°52.36
29	1906	5 Mar	29°11.87	67°50.65
30	1922	5 Mar	29°14.11	67°50.56

Table IV-1: XBT Time and Positions.

V. FASINEX Underway Sampling

a. Oceanographic Log

An oceanographic log was recorded at 15 minute intervals on OCEANUS 175 for the 25 days the ship worked in the frontal area. The variables logged were time, LORAN C latitude and longitude, sea surface temperature from buckets (SST), SAIL SST, and towed fish SST. Thermosalinograph temperature was logger along with SeaSoar mixed layer temperature for specific time periods. The LORAN C data were stored to an IBM AT using floppy disks. The SAIL and towed fish data were stored every minute on Apple IIe floppy disks. The underway towed sensor was a modified XBT probe.

- | | |
|-------------|---|
| Figure Va-1 | Contoured Bucket Temperatures Across the Front |
| Figure Va-2 | Contoured Salinity Across the Front |
| Figure Va-3 | Bucket, Towed Fish and SAIL Temperature Comparative Plots |
| Table Va-1 | Example of 15 Minute Oceanographic Log |

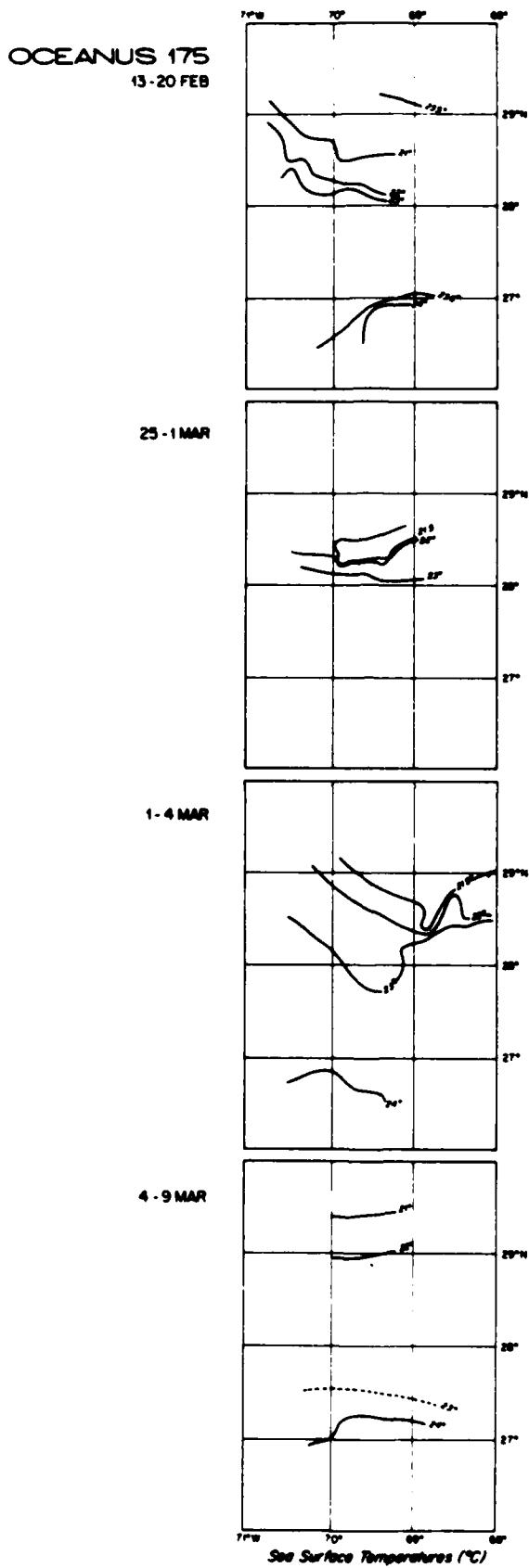


Figure Va-1. Temperature Contours from Bucket Samples.

OCEANUS 175
13-20 FEB

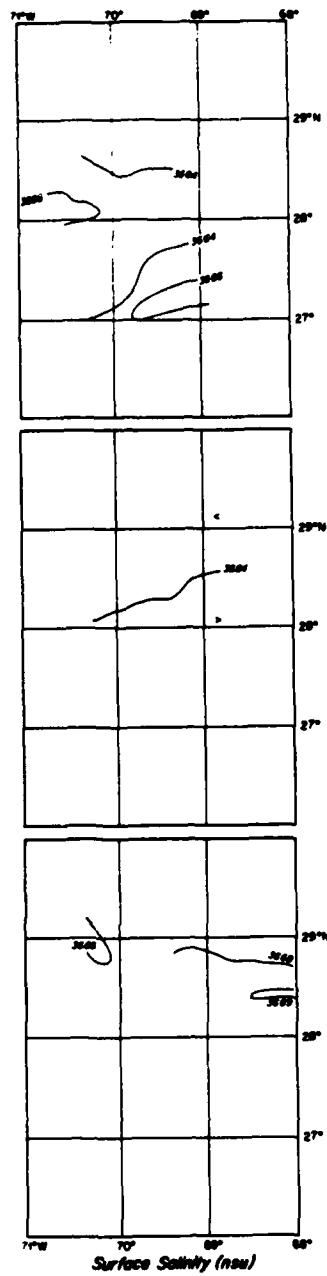


Figure Va-2. Salinity Contours from Bucket Samples

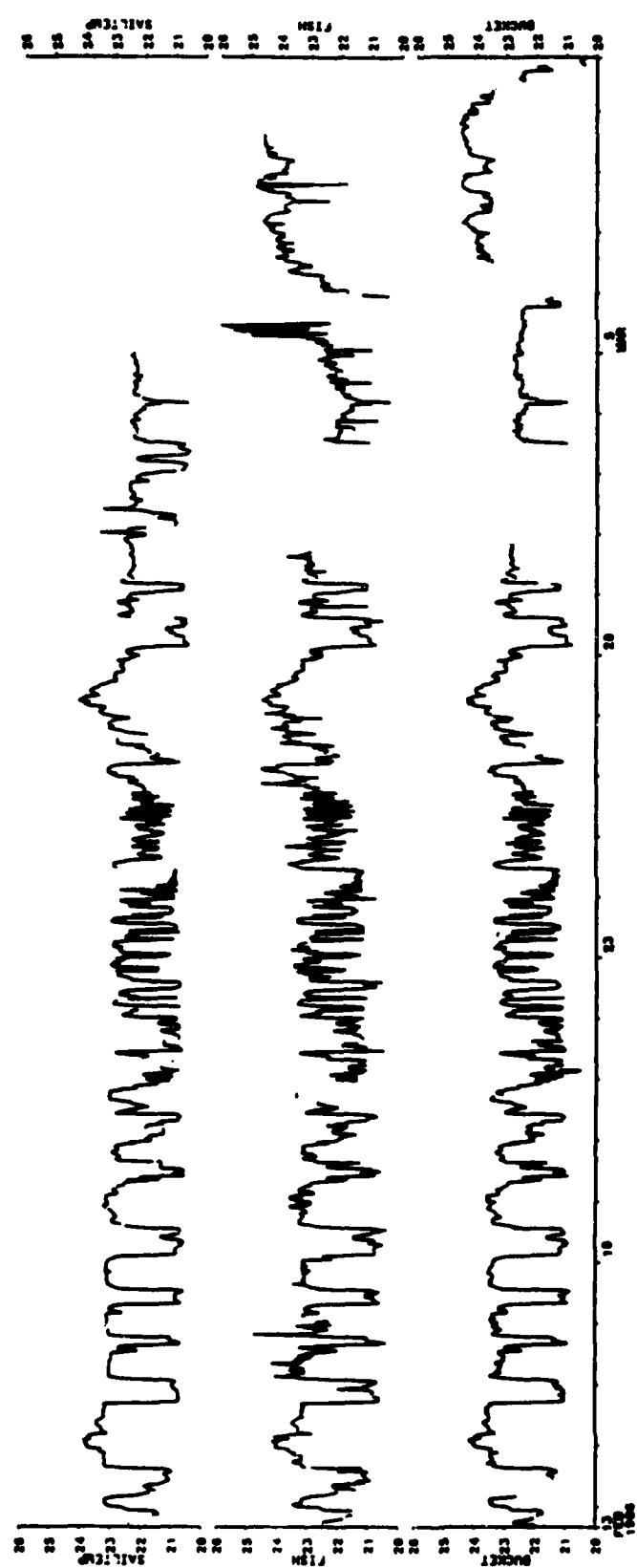


Figure Va-3: Bucket, Towed Fish and SAIL Temperature Comparative Plots.

OCEANUS 175 UNDERWAY LOG

Date	Time	Latitude	Longitude	Fish	Bucket	SAIL	T/S	Mixed Layer Temp	Mixed Layer Time
2/13	1600	30°07.94	67°43.24	-	21.6	26.40			
2/13	1615	30°06.55	67°45.14	-	21.7	26.44			
2/13	1630	30°04.76	67°47.74	-	22.0	26.72			
2/13	1645	30°02.95	67°50.54	-	22.0	26.43			
2/13	1700	30°01.06	67°53.03	22.5	22.0	26.91			
2/13	1715	29°59.11	67°55.79	-	22.0	27.1			
2/13	1730	29°57.24	67°58.53	-	22.5	27.29			
2/13	1745	29°55.37	68°01.07	-	22.6	22.4			
2/13	1800	29°53.58	68°03.84	22.5	22.7	27.6			
2/13	1815	29°51.79	68°06.50	22.5	22.7	27.6			
2/13	1830	29°50.00	68°09.03	22.4	22.6	27.58			
2/13	1845	29°48.20	68°11.91	22.2	22.4	27.29			
2/13	1900	29°46.43	68°14.45	22.1	22.3	27.20			
2/13	1915	29°44.64	68°17.16	22.0	22.2	27.14			
2/13	1930	29°42.78	68°19.89	21.8	22.0	27.04			
2/13	1945	29°40.93	68°22.52	21.9	22.1	27.07			
2/13	2000								
2/13	2015								
2/13	2030	29°35.60	68°30.15	21.7	21.9	26.75			
2/13	2045	29°33.67	68°32.86	21.5	21.9	26.72			
2/13	2100	29°31.80	68°35.34	21.6	21.9	21.65			
2/13	2115	29°30.07	68°37.79	-	21.7	21.43			
2/13	2130	29°28.11	68°40.42	-	21.7	21.46			
2/13	2145	29°26.30	68°42.88	-	21.8	21.46			
2/13	2200	29°24.47	68°45.40	-	21.8	21.56			
2/13	2215	29°22.87	68°48.09	-	21.75	21.53			
2/13	2230	29°21.15	68°50.94	21.5	21.8	21.53			
2/13	2245	29°19.58	68°53.45	21.6	21.9	21.69			
2/13	2300	29°17.88	68°55.87	22.4	22.8	22.41			
2/13	2315	29°17.97	68°56.88	22.5	22.8	22.59			
2/13	2330	29°18.40	68°58.08	22.5	22.8	22.59			
2/13	2345	29°18.87	68°59.22	22.6	22.8	22.66			
2/14	0000	29°18.06	69°00.33	22.6	22.9	22.63			
2/14	0015	29°16.91	69°01.66	23.2	23.0	22.97			
2/14	0030	29°15.78	69°03.04	23.4	23.3	23.12			
2/14	0045	29°14.77	69°04.42	23.4	23.4	23.15			
2/14	0100	29°13.73	69°06.04	23.5	23.4	23.19			
2/14	0115	29°12.63	69°07.71	23.5	23.5	23.22			
2/14	0130	29°11.55	69°09.43	23.2	23.4	23.25			
2/14	0145	29°10.50	69°11.13	23.2	23.4	23.22			
2/14	0200	29°09.43	69°12.81	23.2	23.4	23.25			
2/14	0215	29°08.40	69°14.58	23.2	23.5	23.25			
2/14	0230	29°07.40	69°16.36	23.2	23.5	23.25			
2/14	0245	29°06.34	69°18.00	23.2	23.5	23.25			
2/14	0300	29°05.33	69°19.76	23.2	23.5	23.25			
2/14	0315	29°04.31	69°21.76	23.2	23.4	23.22			
2/14	0345	29°04.57	69°23.99	23.1	23.2	23.09			

Table Va-1: Example of 15 Minute Oceanographic Log.

V. FASINEX Underway Sampling

b. Meteorological Log

Ken Davidson coordinated a met program on both OCEANUS and ENDEAVOR during FASINEX Phase Two. Using met sensors mounted on a bow mast, data were gathered and logged to floppies. Manual observations were also taken every half hour. Radiosondes were launched from both ships alternating on a four hour schedule, with several additional radiosondes launched on aircraft overflight days. SODAR data was also collected on the two ships. The plots included in this section are for both ships. Each three-day data section shows synoptic weather maps with wind arrow, OCEANUS variables, ENDEAVOR variables, joint radiosonde locations and radiosonde data.

Davidson Description of Measurements

1. Due to system failure/performance the following measurements were not made, except for short periods at the beginning, on the ENDEAVOR

Aerosol

Humidity variance (Lyman- α)

SODAR

2. Temperature and humidity on the OCEANUS will only be available from point measurements every 1/2 hour. The SAIL system was judged to be in error for both of these.

3. OCEANUS relative wind direction at 5 minute intervals will be available from the SAIL System when the relative wind was from 300 clockwise to 060. Otherwise, relative wind direction will be obtained from point measurements every 1/2 hour.

4. The OCEANUS SODAR operated throughout except for 36 hours due to enclosure damage. However, its range did not extend to the inversion that was above 1 km. Hence the OCEANUS SODAR will not yield much information of continuous evaluation of inversion.

Dick Payne was in charge of an hourly meteorological log on OCEANUS 175. The variables logged were time, LORAN C latitude and longitude, wind speed and direction, wet and dry bulb temperatures, barometric pressure, wave height and direction, cloud cover and type.

Figure Vb-1

Davidson 3-Day Expanded Meteorological Plots
from Payne's Data to Match KNORR Data Set
(see WHOI report 86-35, FASINEX report #13)

Table Vb-1

Shipboard Meteorological Measurements

Figure Vb-2

Radiosonde Launch Positions

Table Vb-2

Radiosonde Launch Times and Locations

Figure Vb-3

Payne's Meteorological Plot for OCEANUS 175

Table Vb-3

Hourly Meteorological Log

Participant Summary:**K. B. Katsaros and R. J. Lind ,
University of Washington Field Program Summary**

Our objective was to measure surface radiation fluxes from R/V ENDEAVOR and R/V OCEANUS during Phase Two of FASINEX. It is hoped that these data will allow analysis of the radiation balance and associated feedback mechanisms at work across the oceanic front.

Identical sensors were deployed on ENDEAVOR and OCEANUS. These included: an Eppley Precision Spectral Pyranometer (model PSP) measuring shortwave irradiance in the frequency band from 0.28 to 2.8 micrometers, an Eppley (model PSP) pyranometer measuring shortwave irradiance in the frequency band from 0.7 to 2.8 micrometers and an Eppley Precision Infrared Radiometer (model PIR) measuring longwave irradiance in the frequency band from 3.0 to 50 micrometers.

Sensors on ENDEAVOR were gimbal mounted on top of a WHOI cargo container located on the port side between midship and the stern. Exposure was excellent with only the ship's mast obstructing the skyward hemisphere at a distance of 15 meters. Continuous monitoring by NPS personnel assured proper cleaning and reported that the sensors were maintained at, or very near horizontal in all sea conditions. Data recording of sensor output was continuous during Phase Two of FASINEX.

Sensors on OCEANUS were fix mounted on top of a bow mast. Exposure was excellent except for the close proximity of a wind sensor also mounted on top of the mast. Our intent was to gimbal mount the sensors, but the accelerations at the tip of the mast were too large to use our simple gravity system. Sensors were cleaned whenever the mast was lowered. A set of four photocells with different diffusers and filters were deployed to compare with the Eppley PSP measuring shortwave irradiance in the 0.7 to 2.8 micrometer wavelength band. Work is beginning on development of an algorithm to remotely determine cloud liquid water content from the combined measurements of shortwave irradiance and photocells (DeVault and Katsaros, 1983). The recording system experienced some data losses during the cruise. Data gaps appear on Feb. 11,12,13,14,16,23,26, and Mar. 1,2,3. Where required, data from models (verified on data from the rest of FASINEX) will make the data set from OCEANUS complete.

Our data from FASINEX is now being processed and results, except for model interpolation, should be ready in August. Data will be in the form of hourly and daily averages. These data will include measured shortwave and longwave irradiance and calculations of shortwave exitance (by method outlined in Payne, 1972) and longwave exitance (from measurements of sea surface temperature).

The investigators wish to thank all of the participants for their cooperation and accommodation during the field phase of FASINEX.

References:

- DeVault, J.E. and K. B. Katsaros, 1983: Remote determination of cloud liquid water path from bandwidth limited shortwave measurements. *J. Atmos. Sci.*, 40, 655-685.
- Lind, R.J. and K. B. Katsaros, 1982: A model of longwave irradiance for use with surface observations. *J. Appl. Met.*, 21, 1015-1023.
- Payne, R. E., 1972: Albedo of the sea surface. *J. Atmos. Sci.*, 29, 959-970.

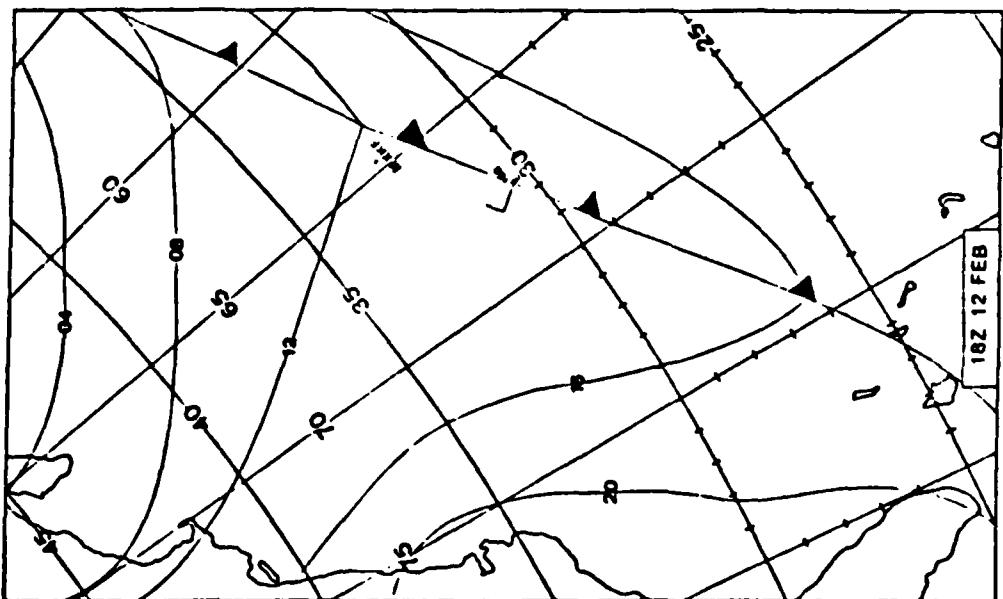
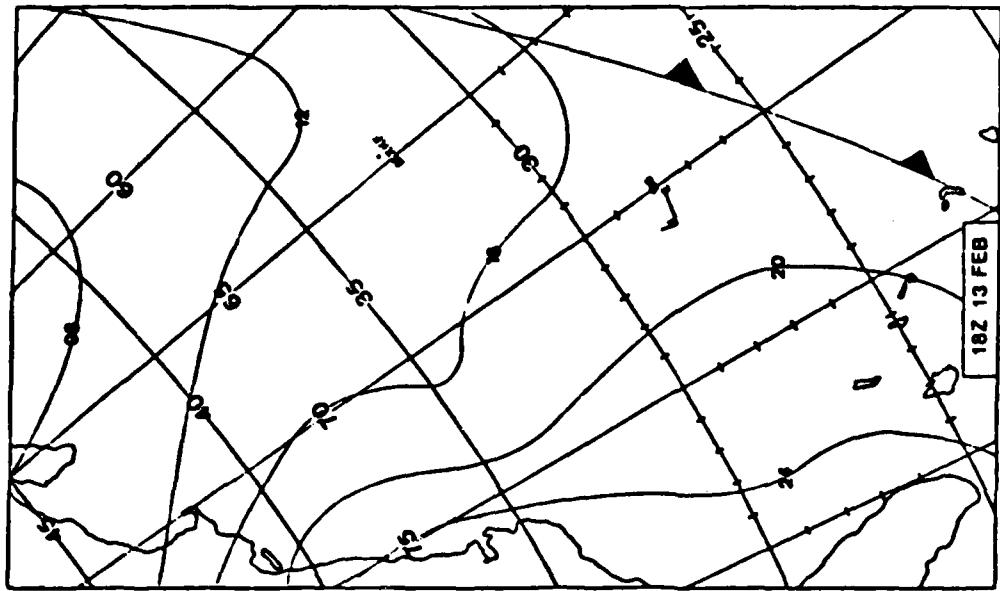


Figure Vb-1: Davidson 3-Day Expanded Meteorological Plots from Payne's Data to Match KNORR Data Set (see WHOI Report 86-35, FASINEX Report #13).

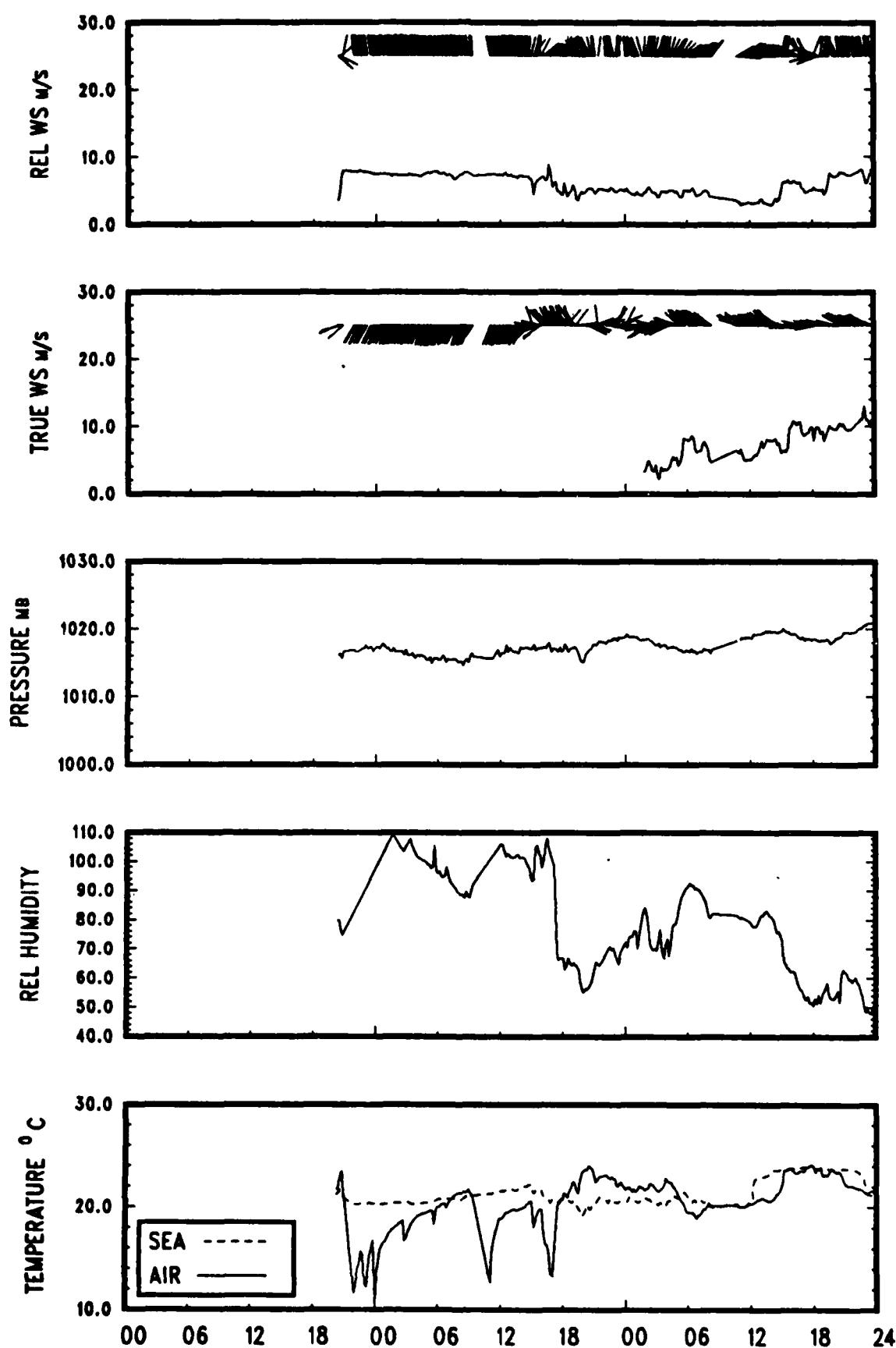


Fig. Vb-1 (Cont)

11 FEB FASINEX 1986 ENDEAVOR

13 FEB

FASINEX RADIOSONDES

13 FEB

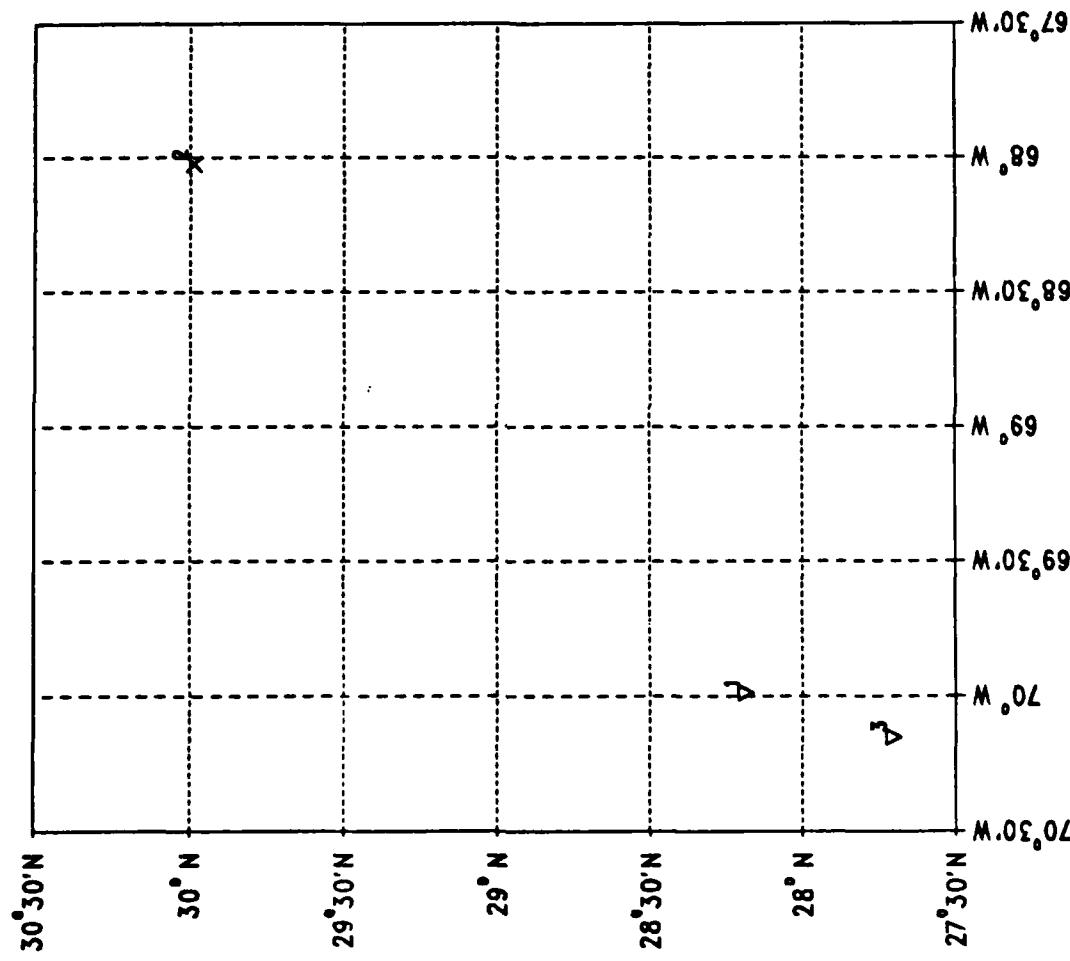


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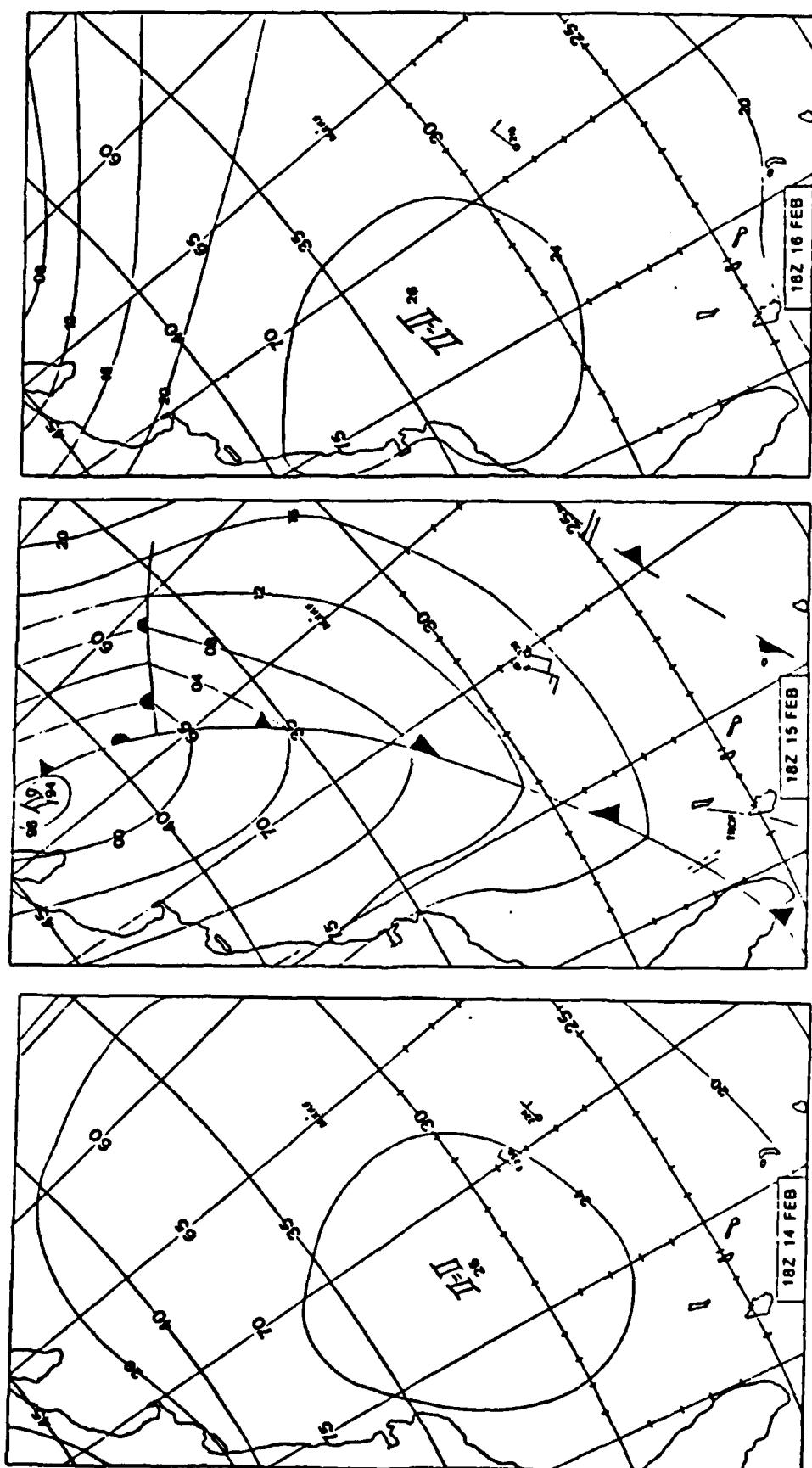
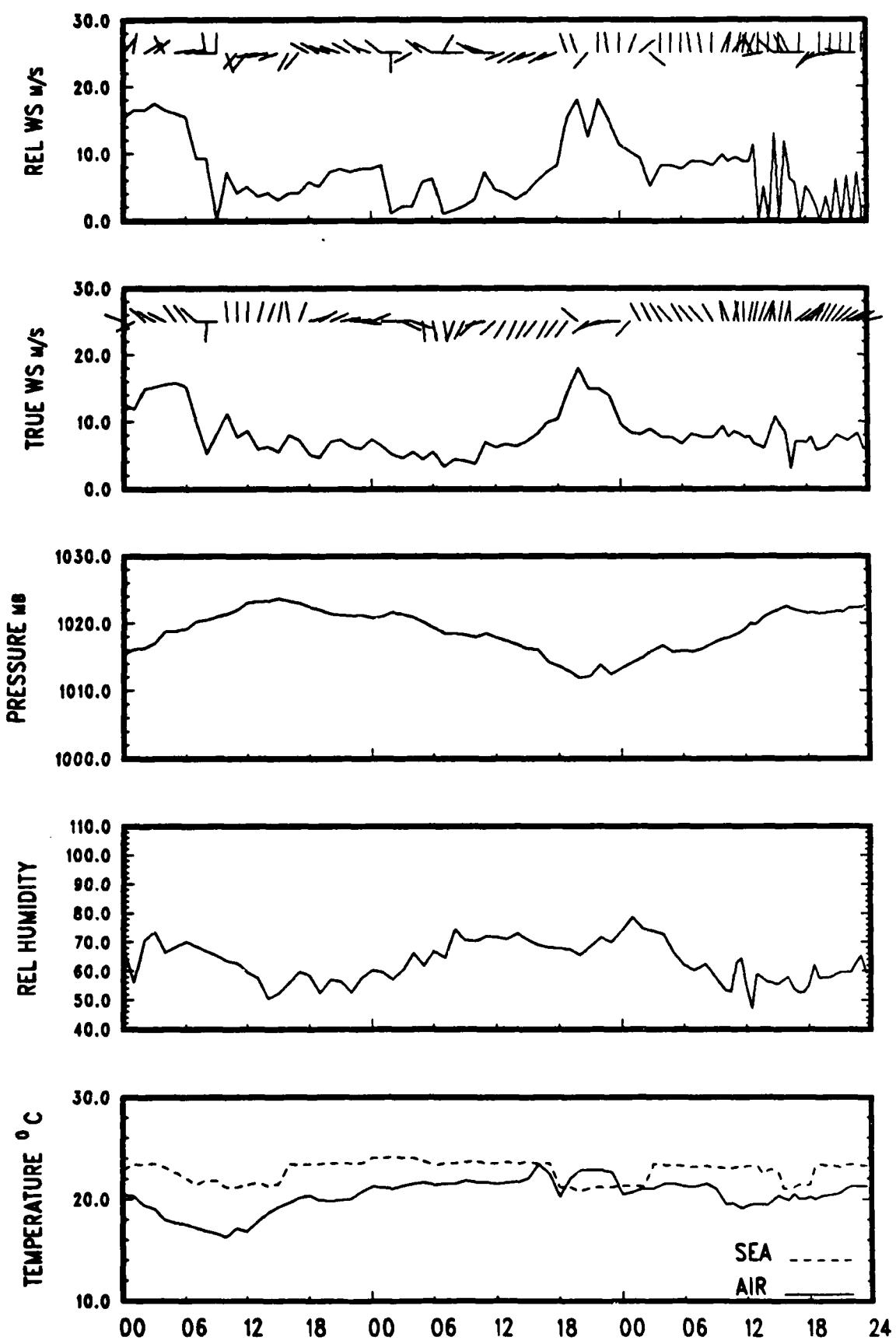


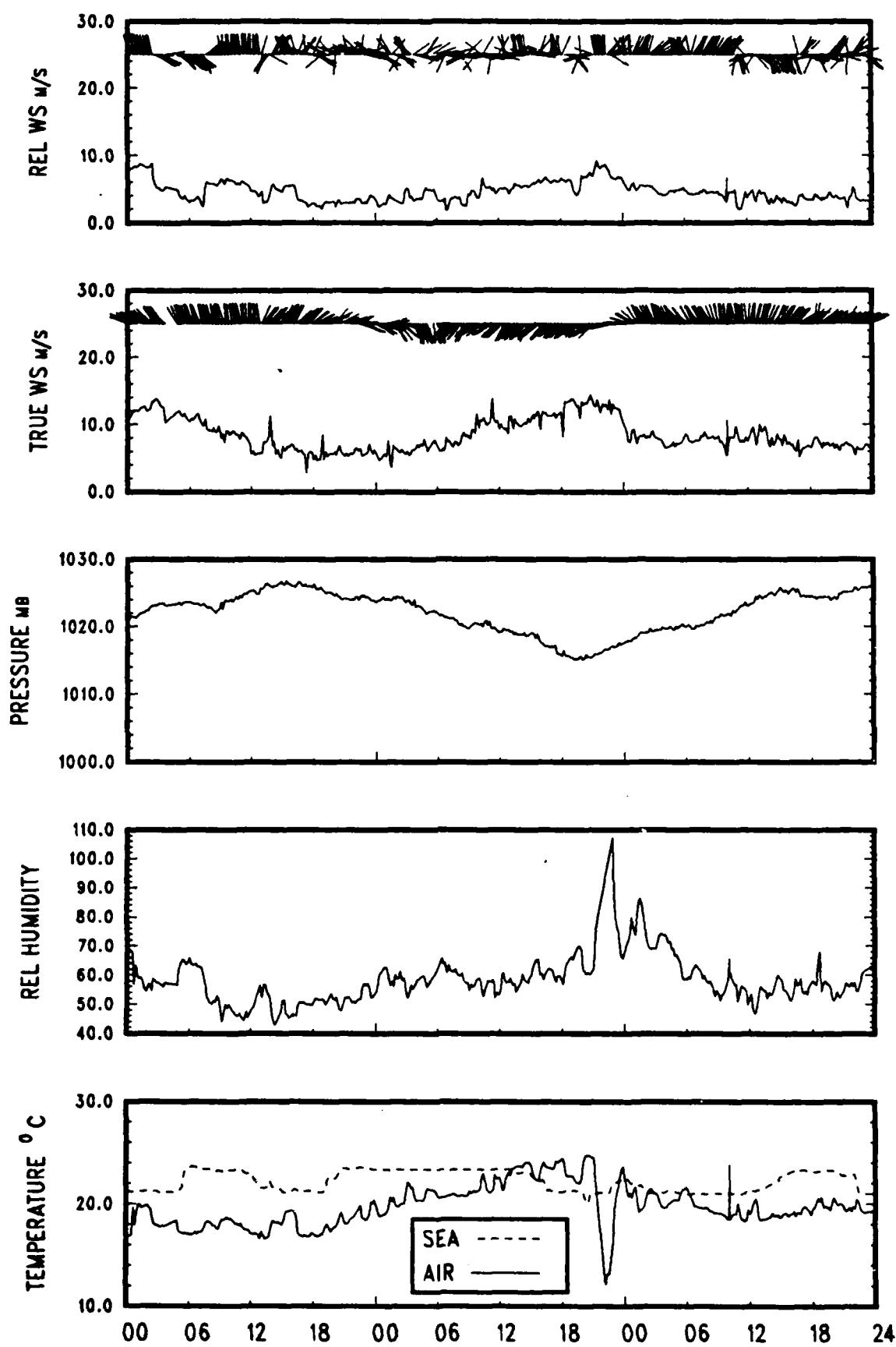
Fig Vb-1 (Cont)



14 FEB
Fig Vb-1 (Cont)

FASINEX 1986 OCEANUS

16 FEB



14 FEB
Fig Vb-1 (Cont)

FASINEX 1986 ENDEAVOR

16 FEB

FASINEX RADIOSONDES

14 FEB - 16 FEB

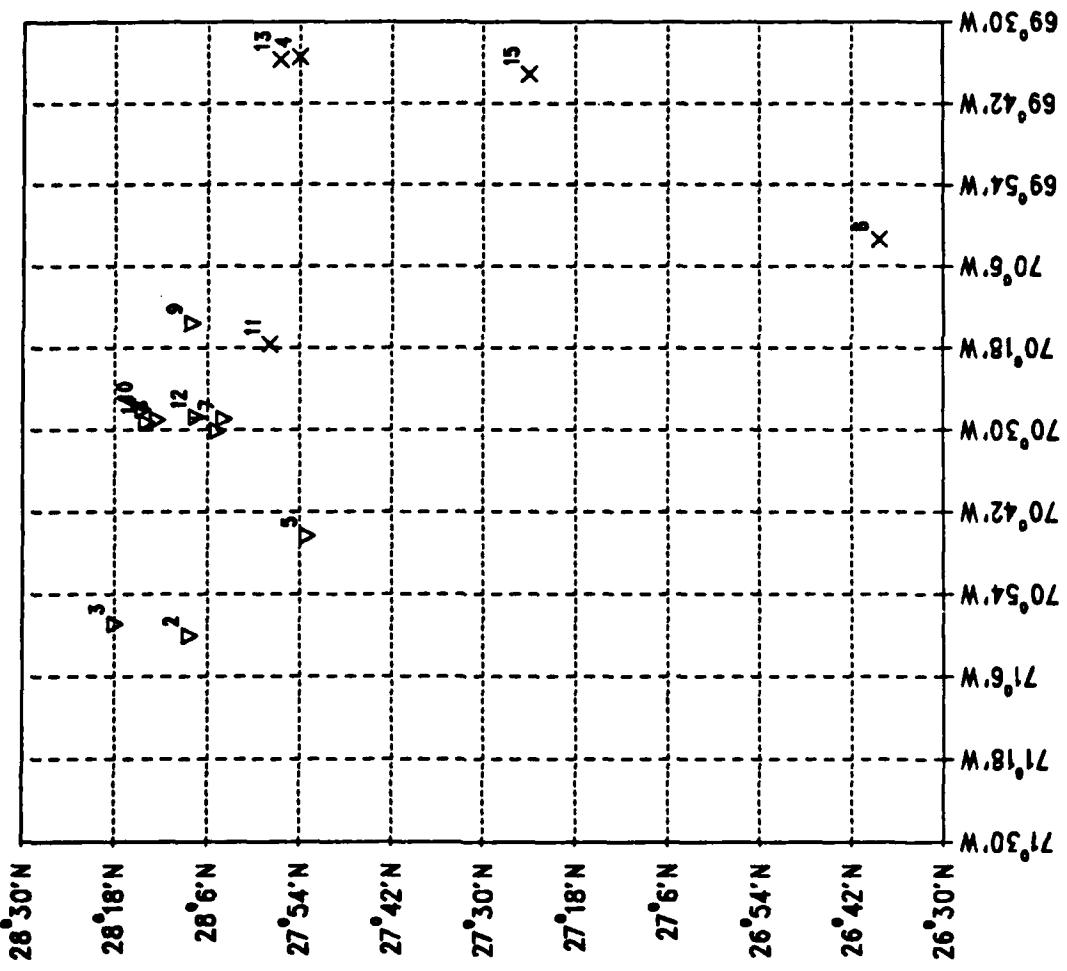


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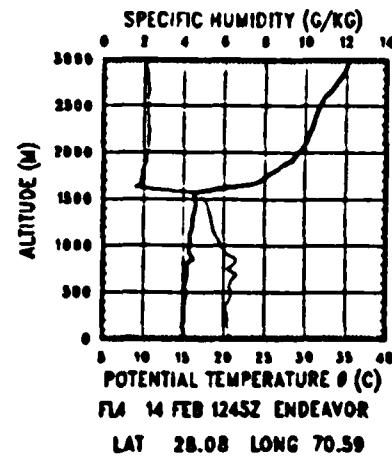
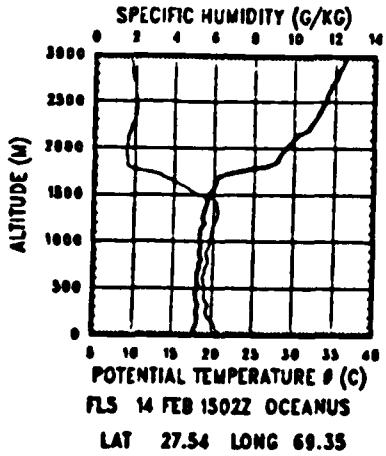
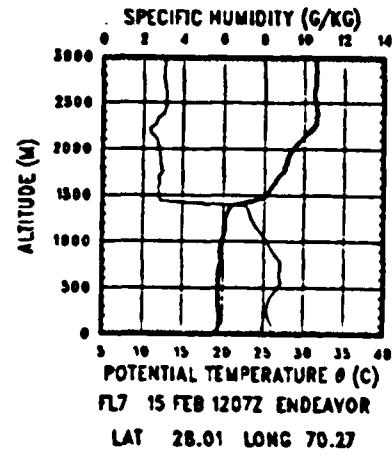
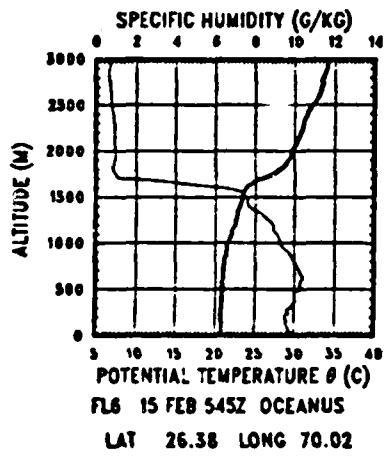
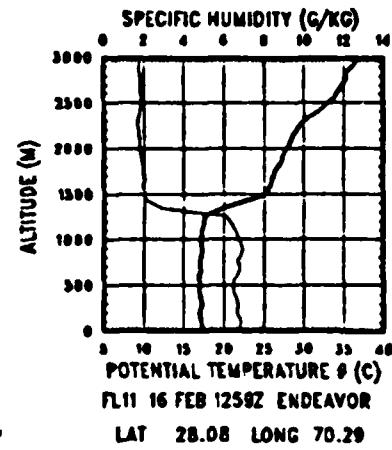
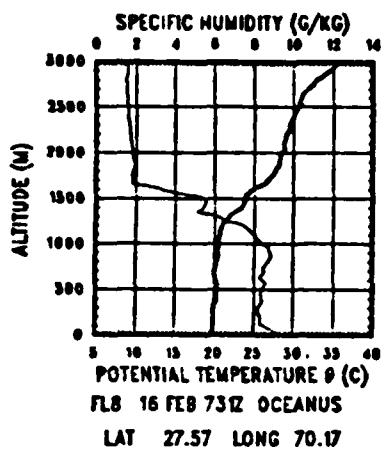


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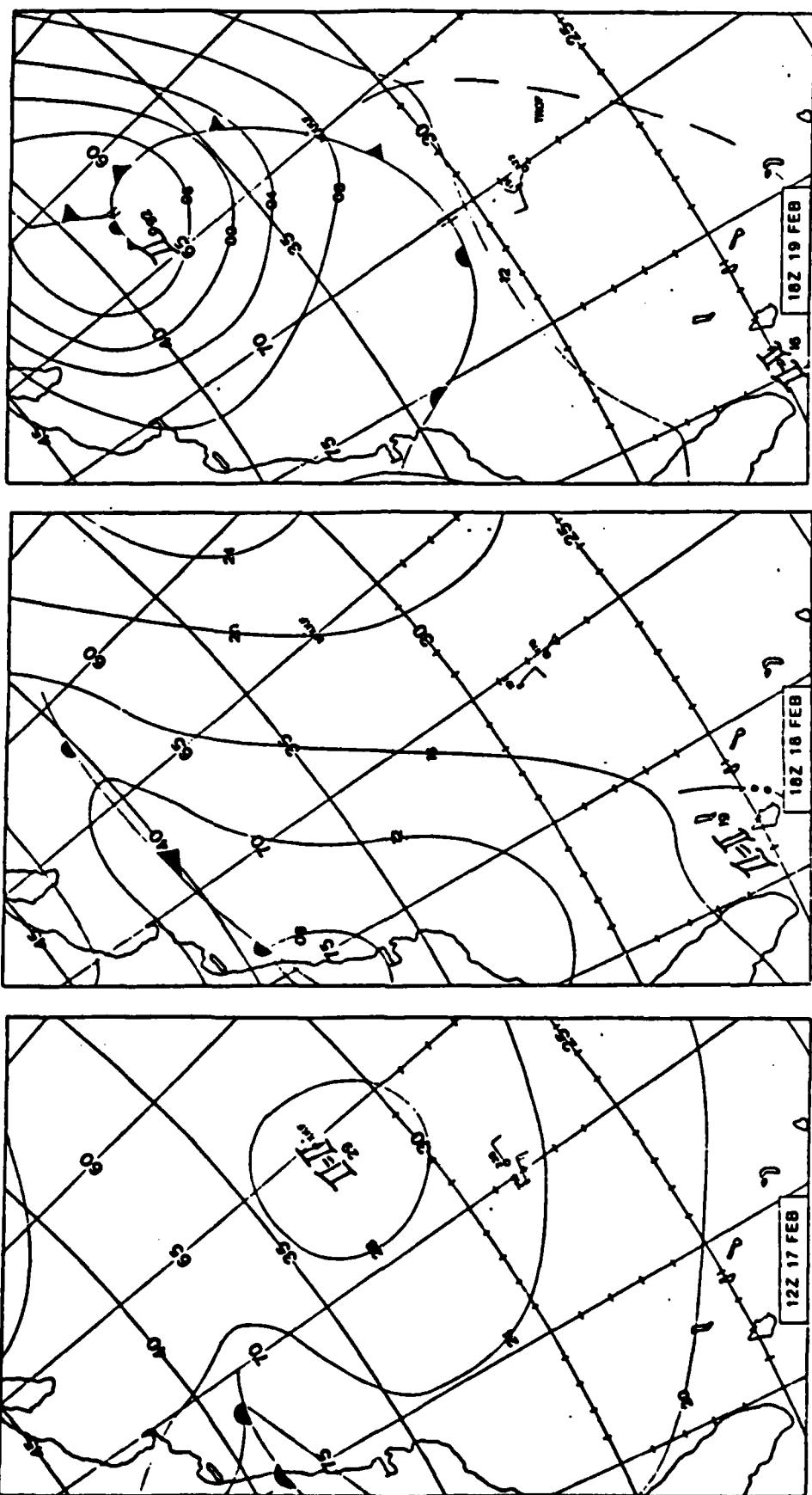


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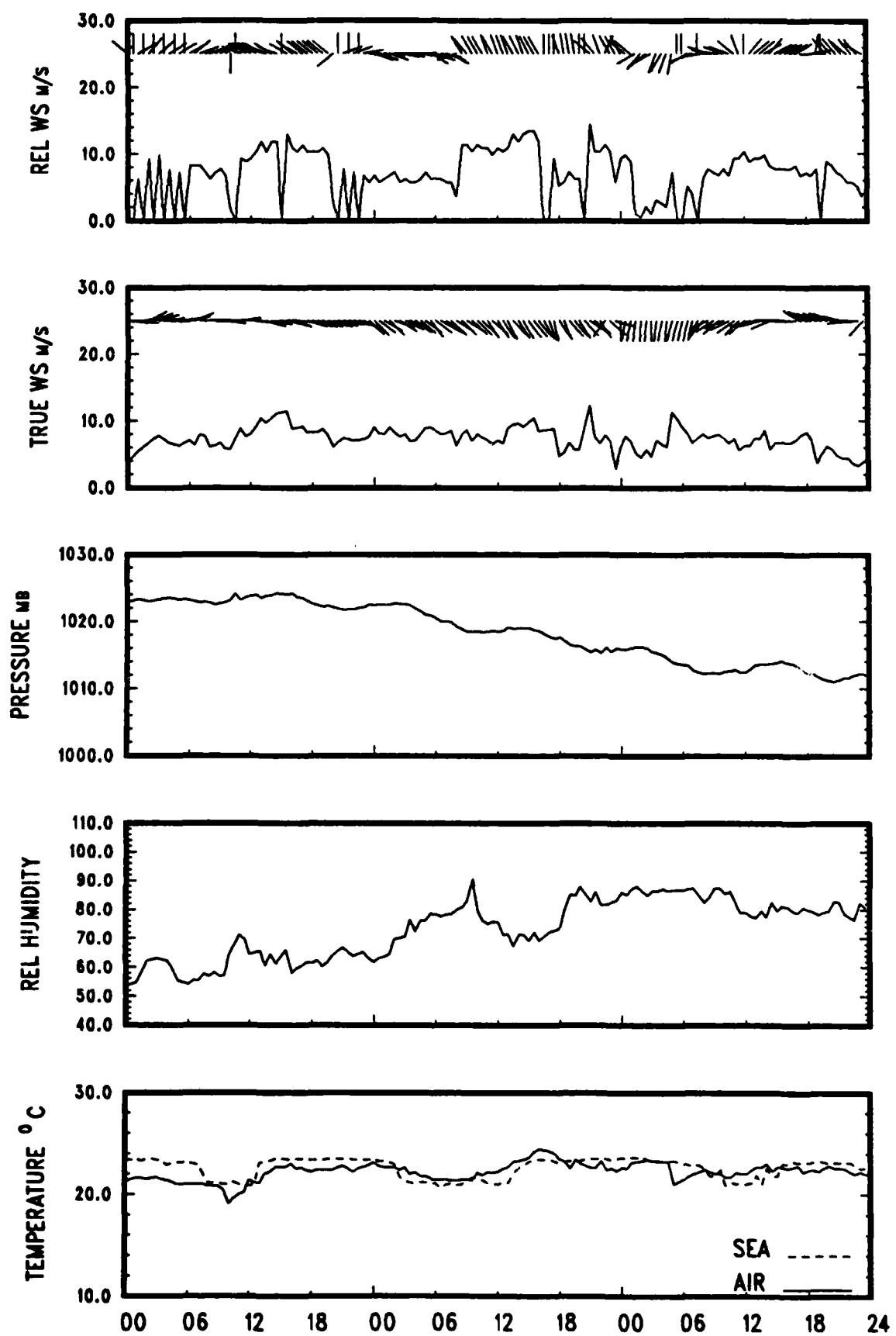


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FASINEX 1986 OCEANUS

19 FEB

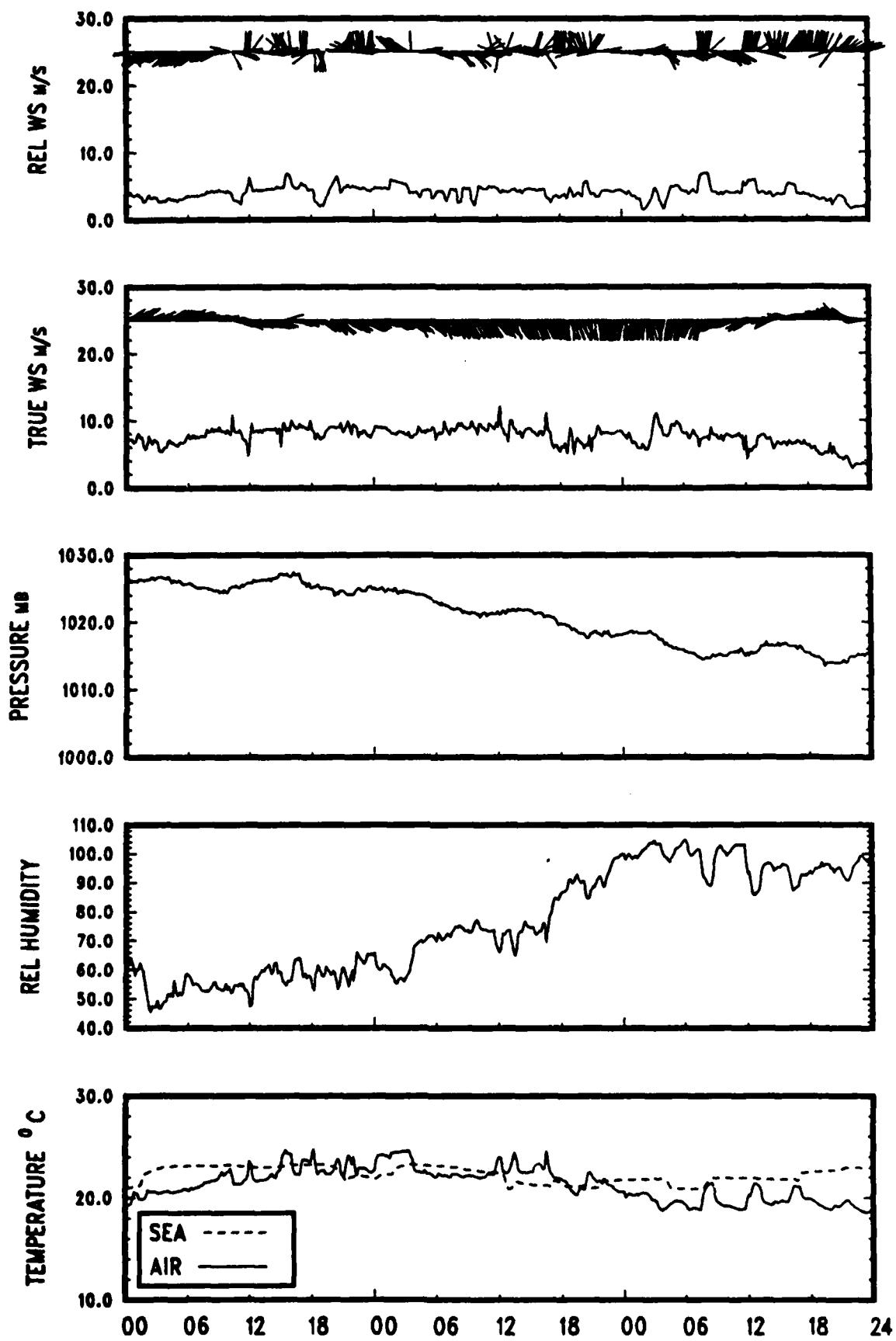


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17 FEB

FASINEX 1986 ENDEAVOR

19 FEB

FASINEX RADIOSONDES

17 FEB - 19 FEB

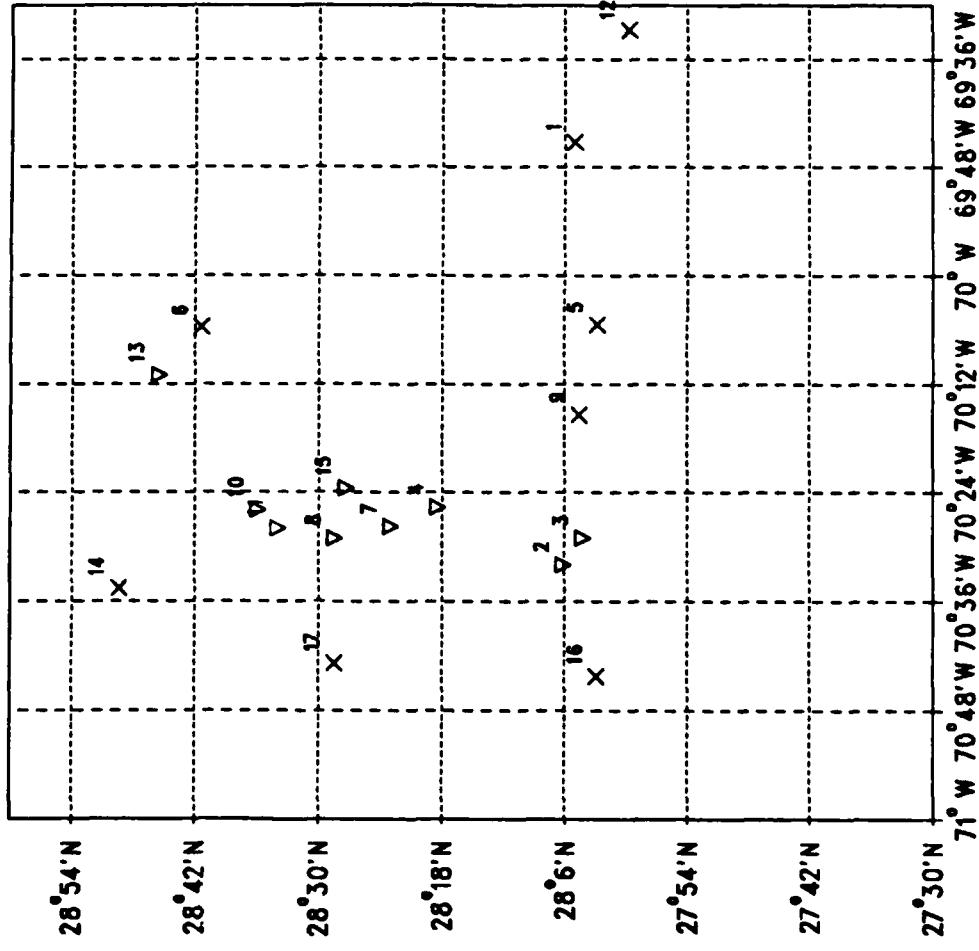


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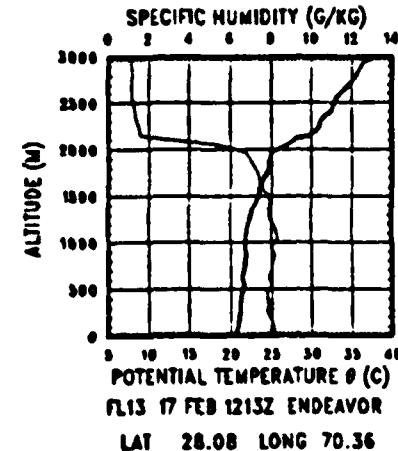
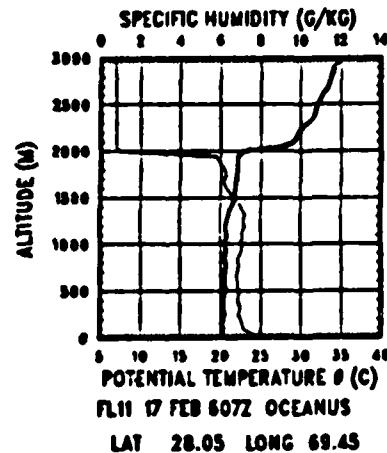
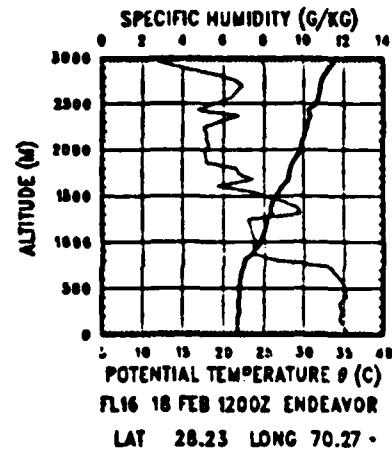
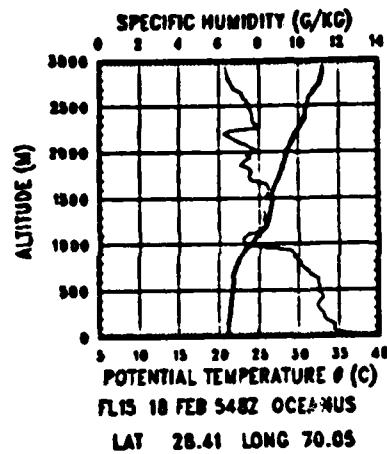
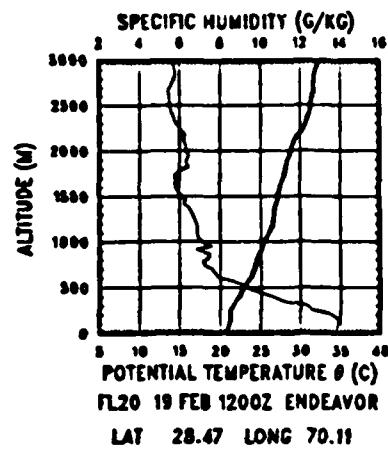
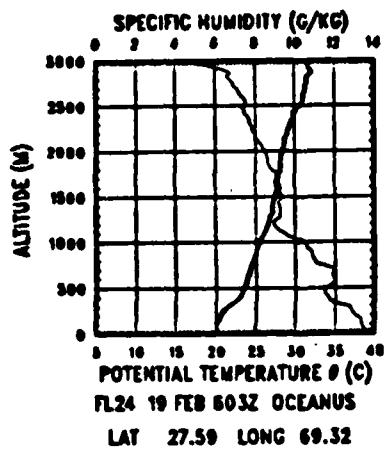


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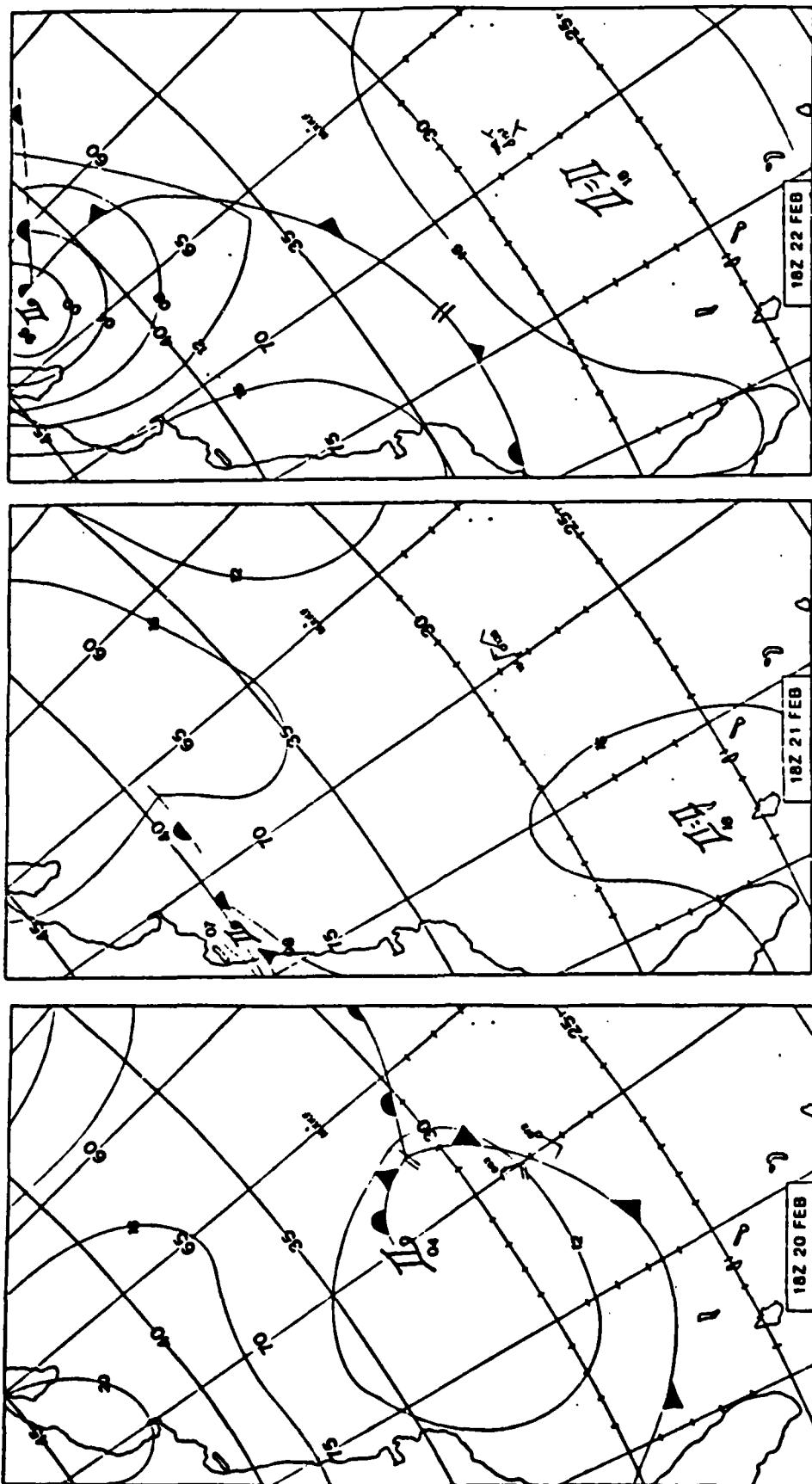
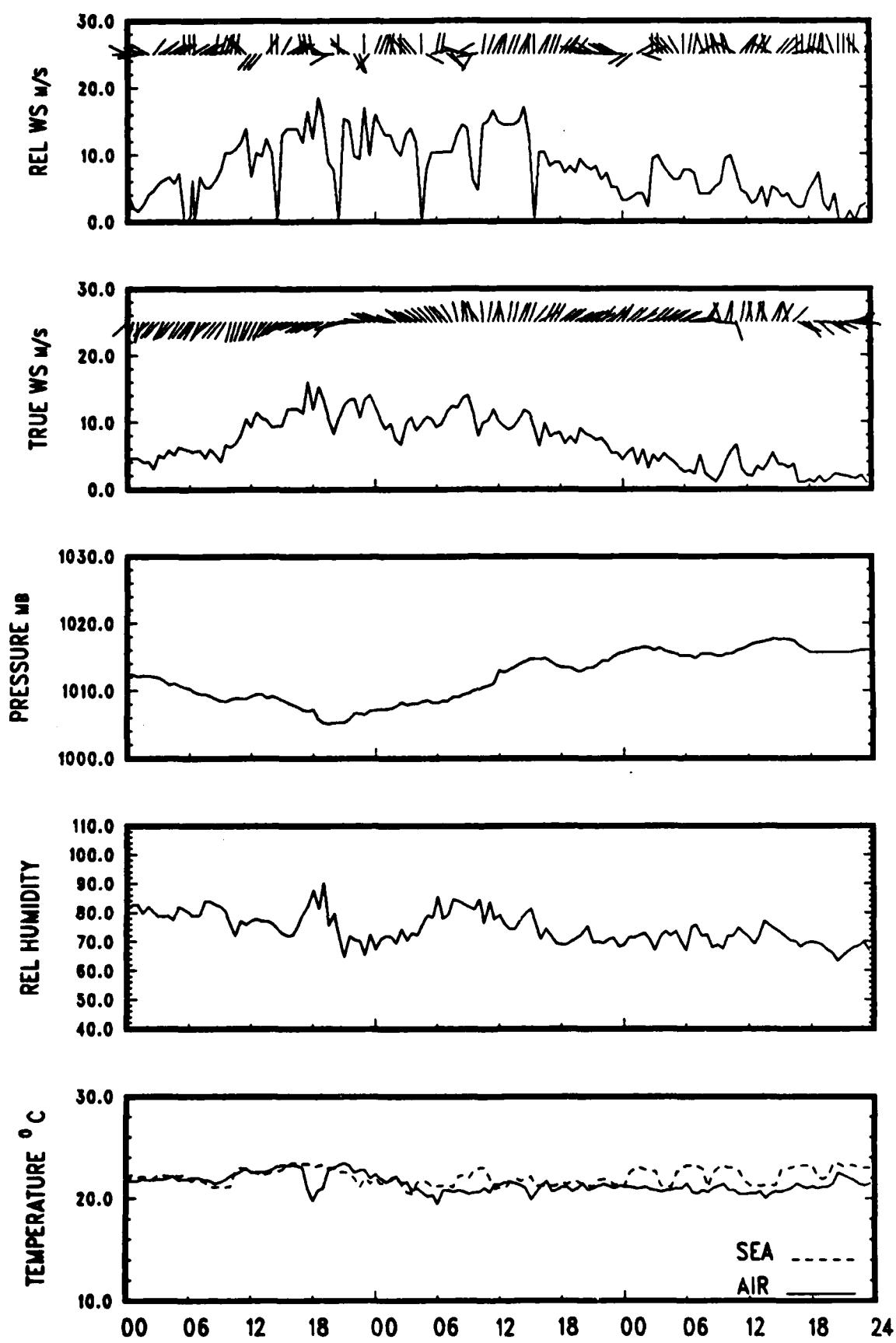


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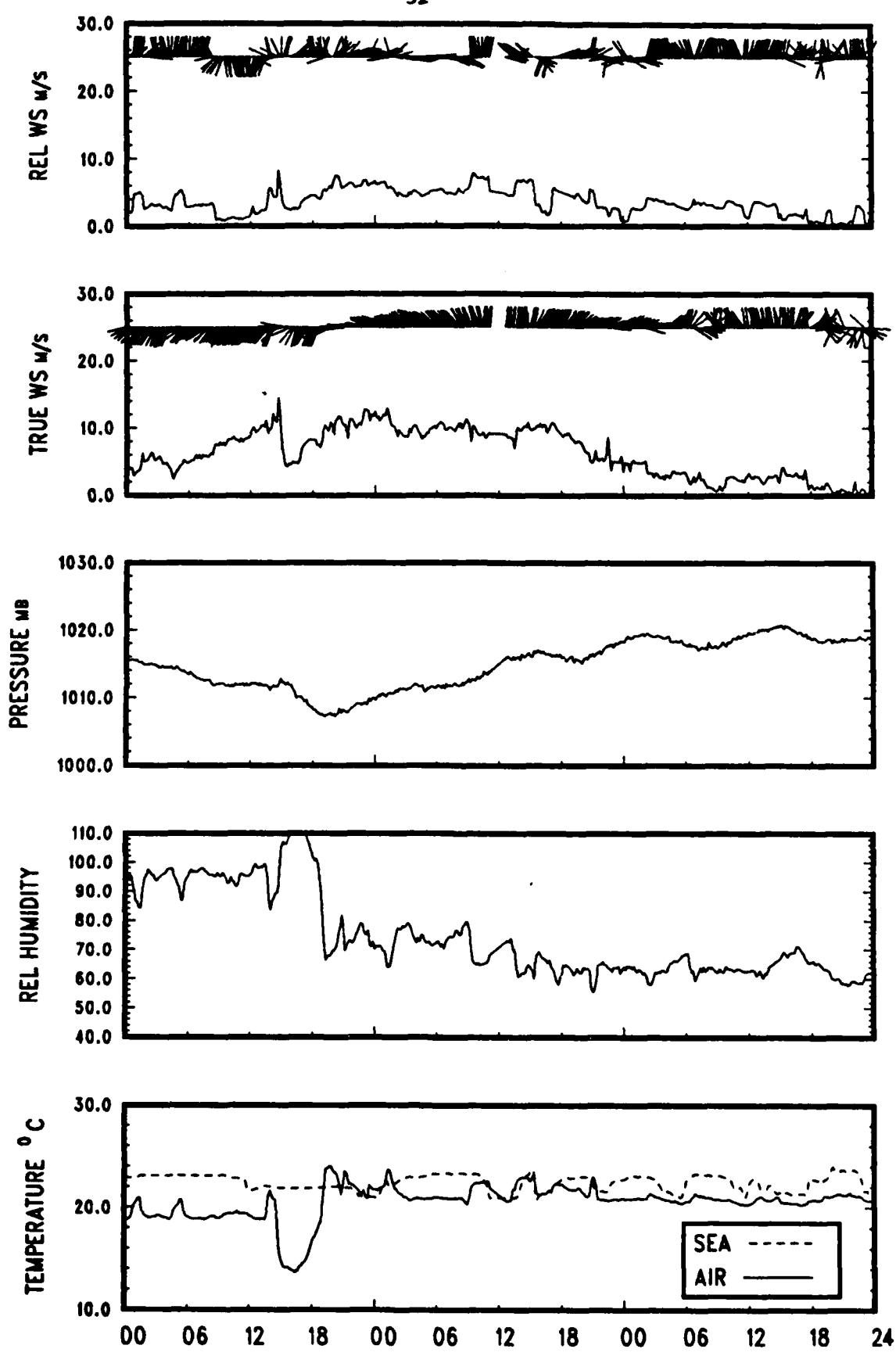
20 FEB

FASINEX 1986 OCEANUS

22 FEB

Fig Vb-1 (Cont)

52



20 FEB

FASINEX 1986 ENDEAVOR

22 FEB

Fig Vb-1 (Cont)

FASINEX RADIOSONDES

20 FEB - 22 FEB

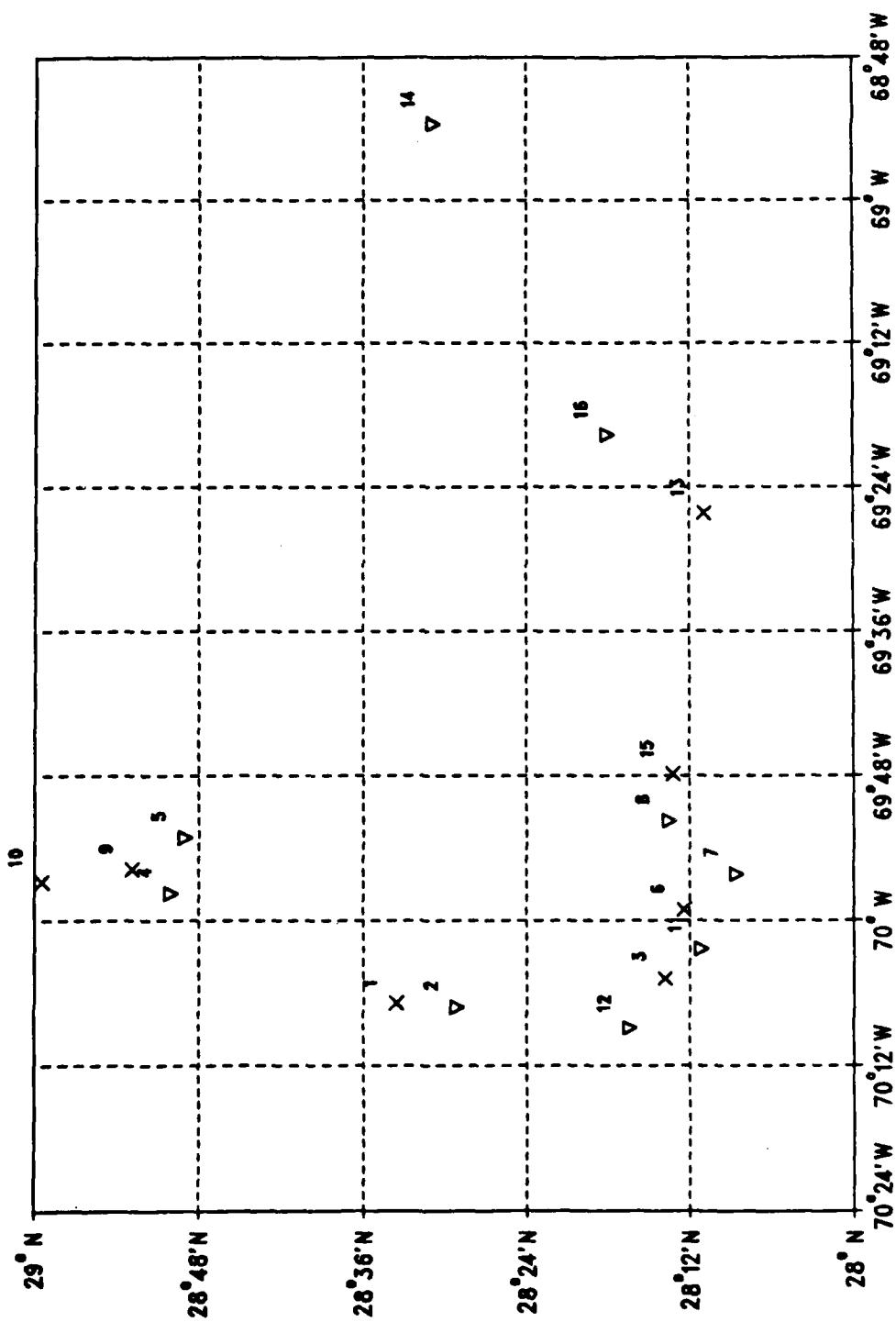


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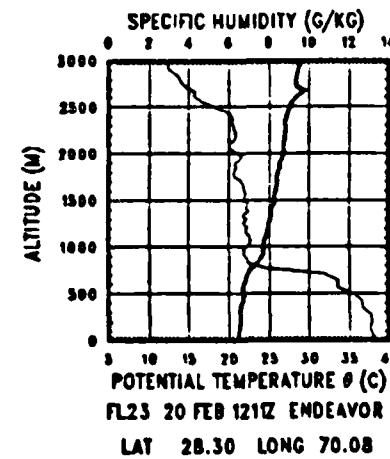
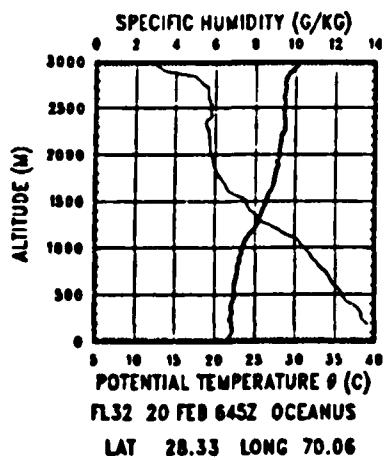
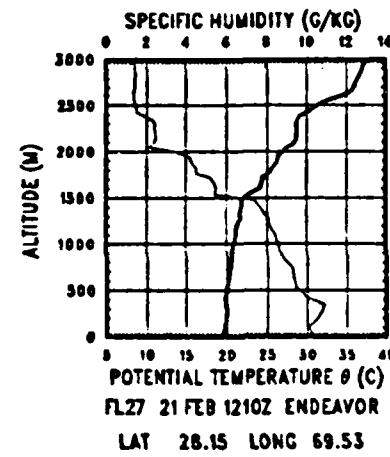
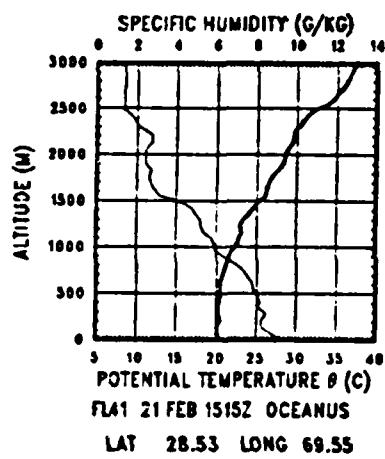
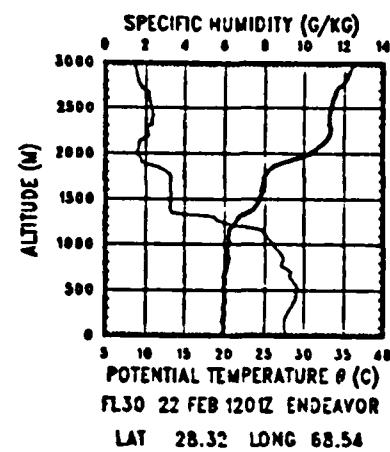
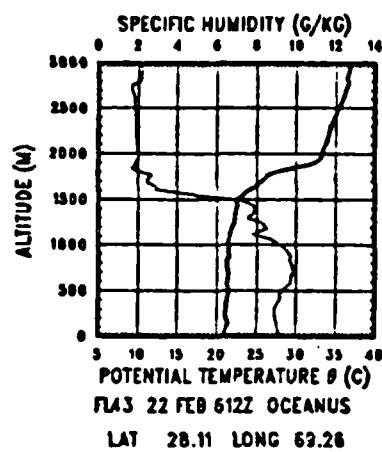


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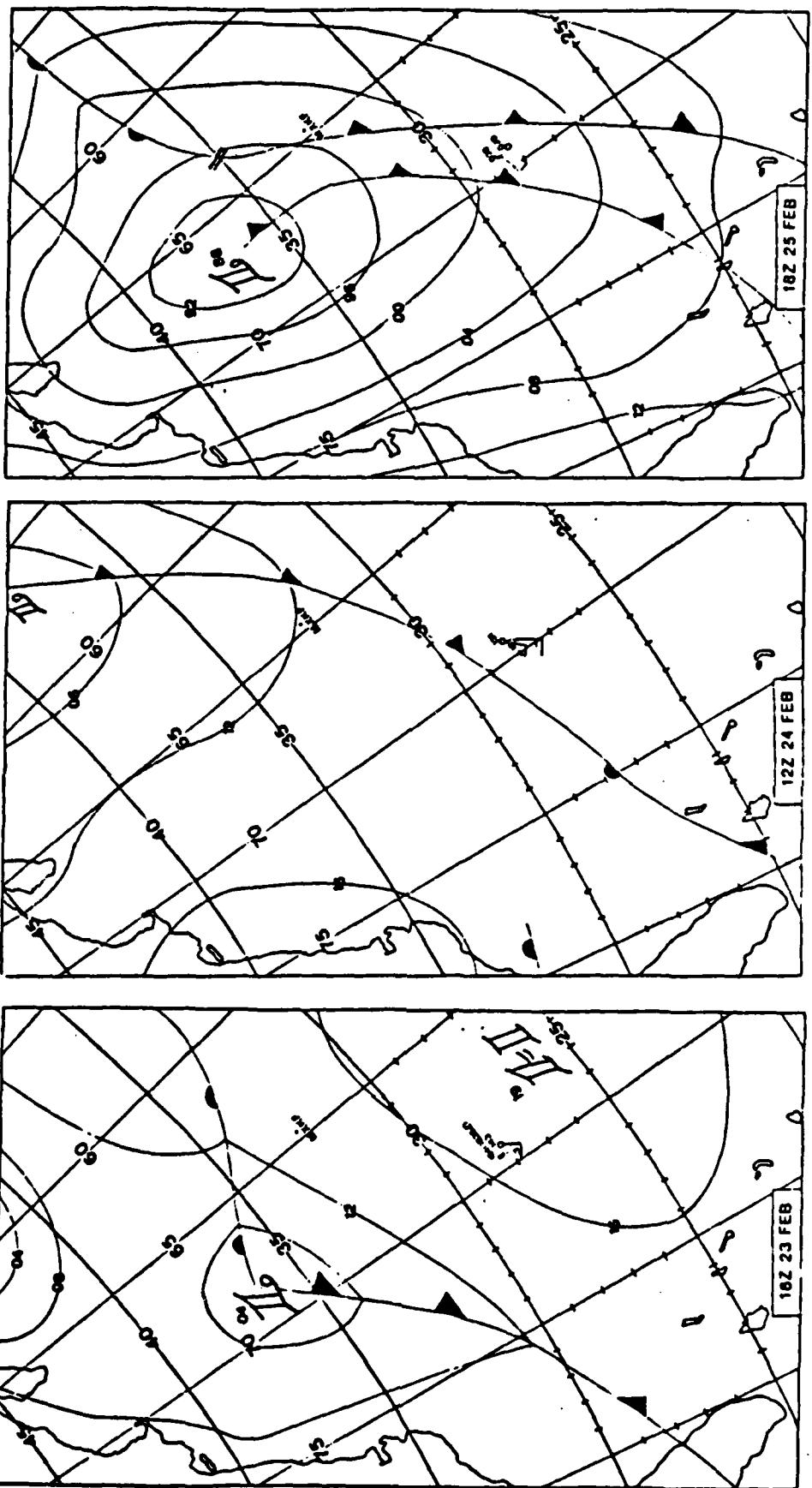


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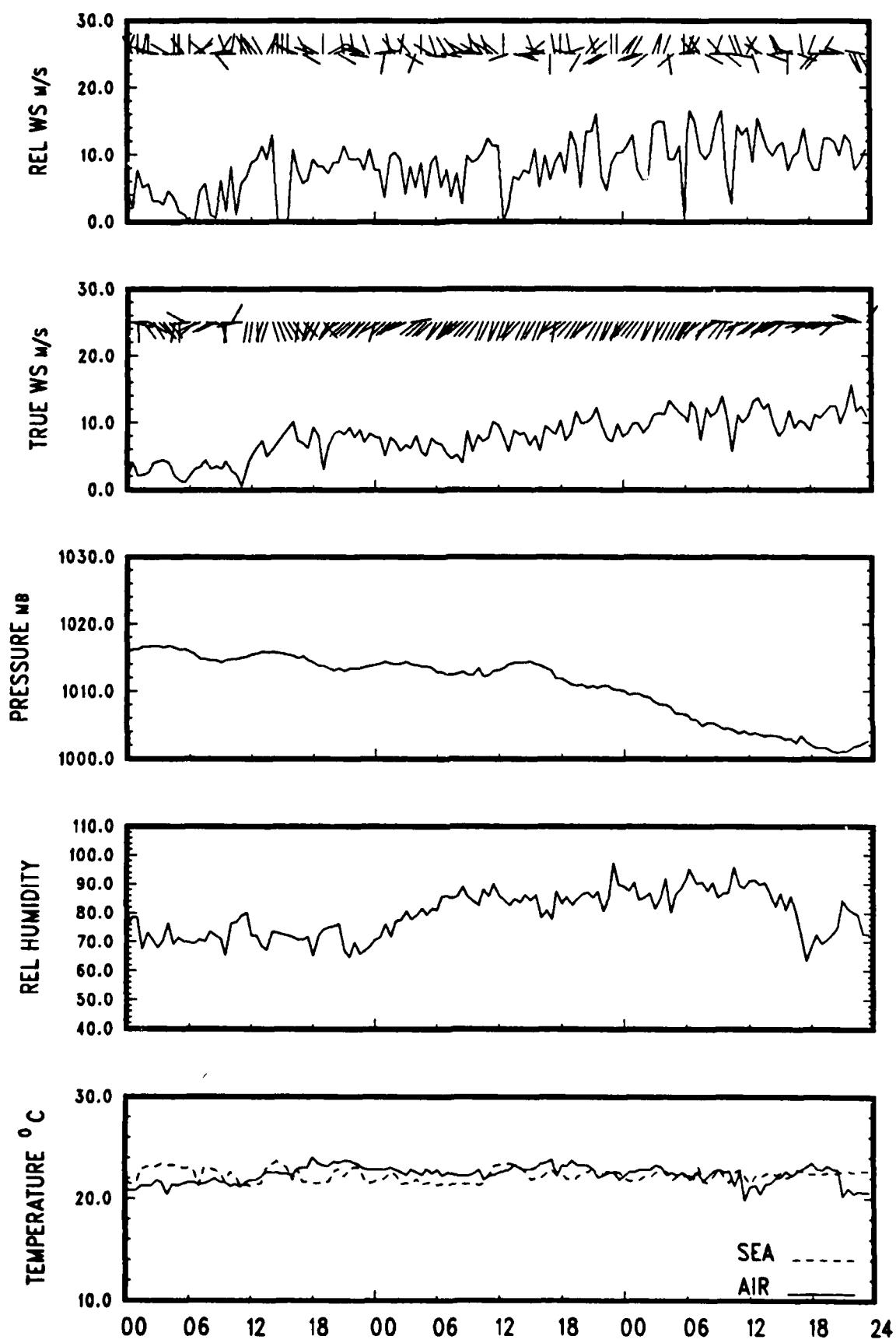
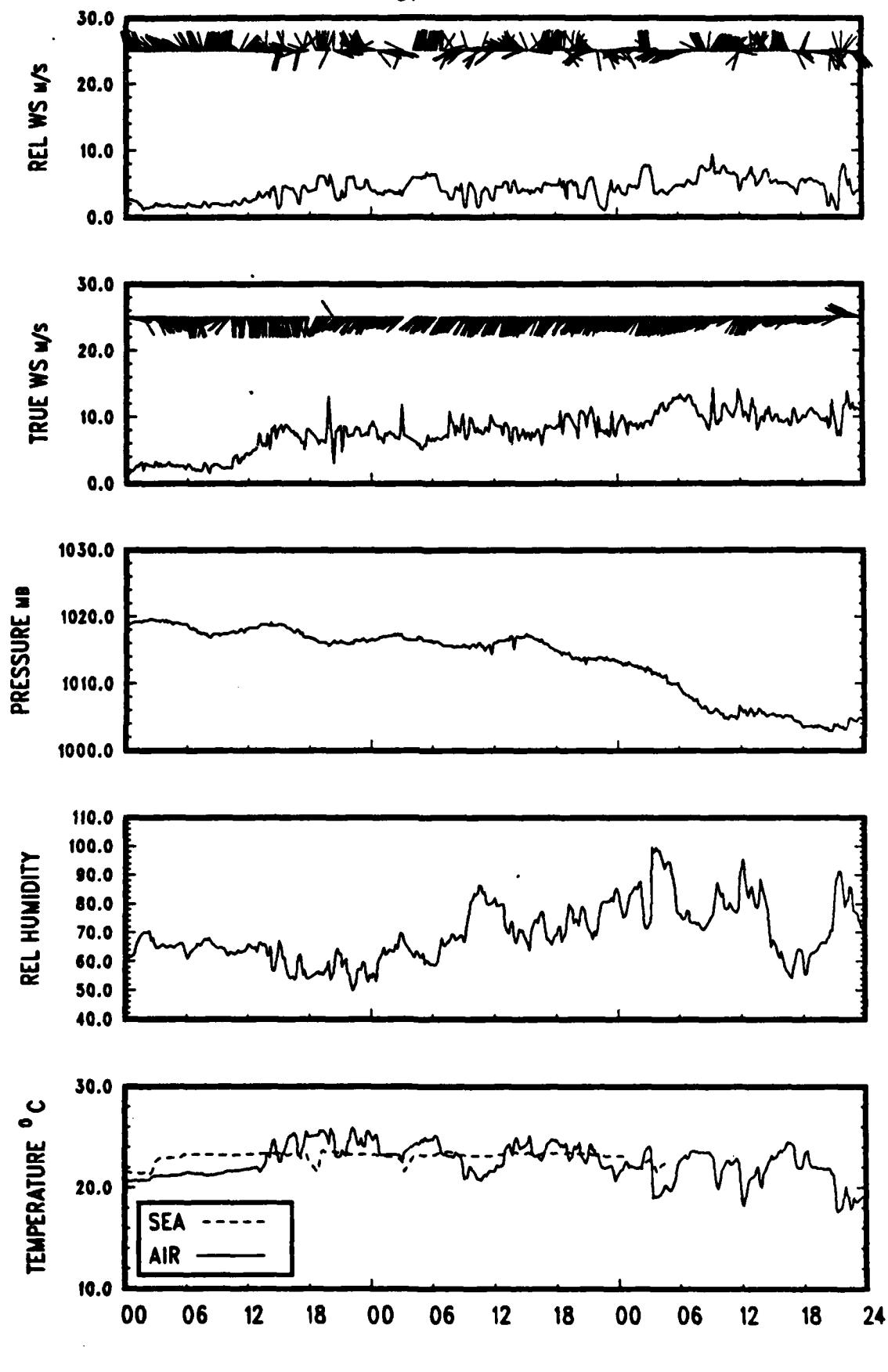


Fig Vb-1 (Cont) 23 FEB

FASINEX 1986 OCEANUS

25 FEB



23 FEB

FASINEX 1986 ENDEAVOR

25 FEB

Fig Vb-1 (Cont)

FASINEX RADIOSONDES

23 FEB - 25 FEB

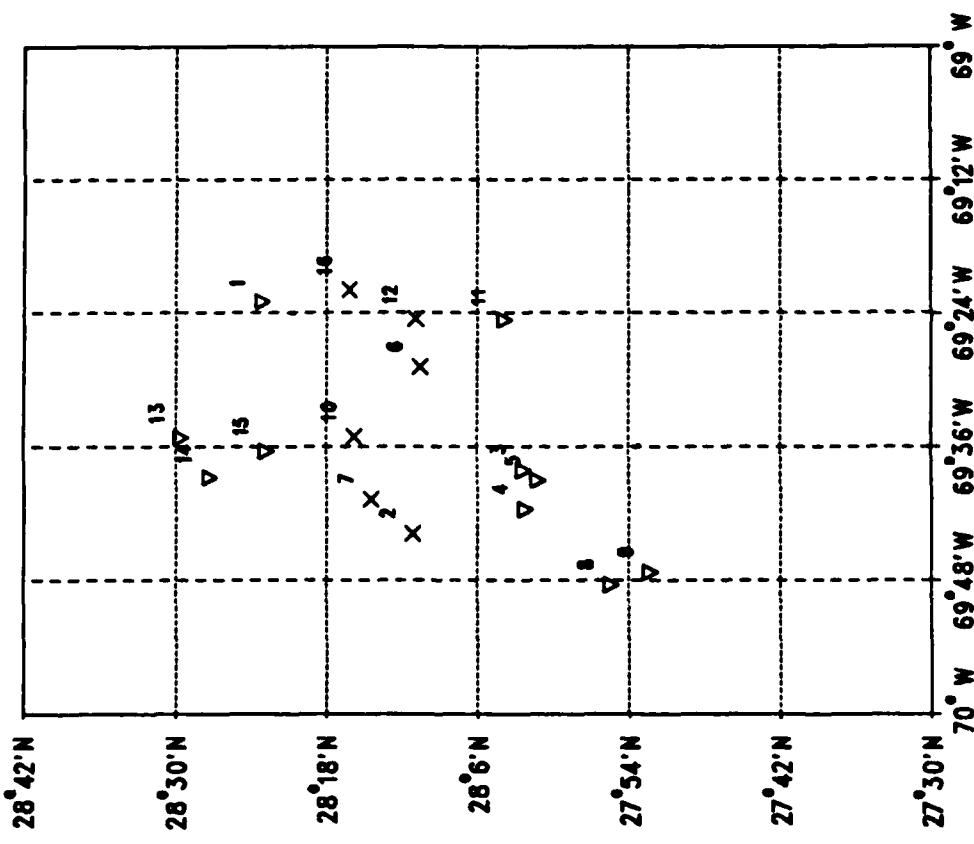


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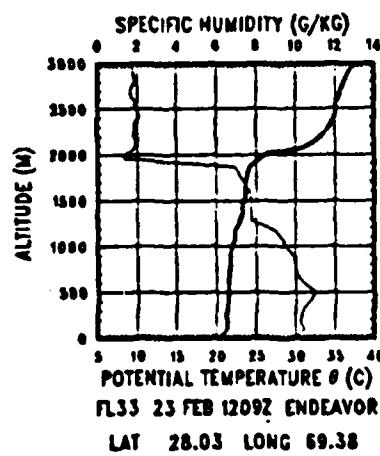
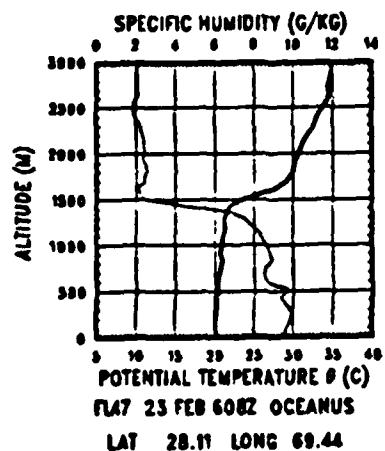
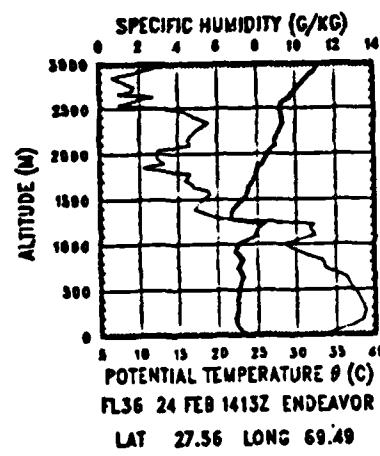
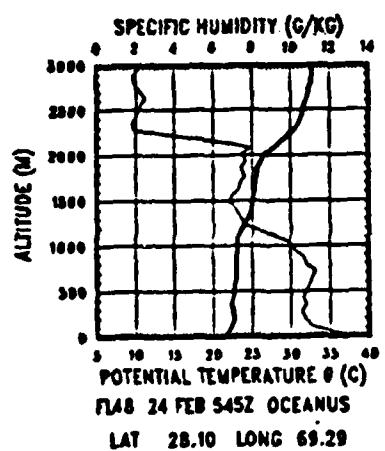
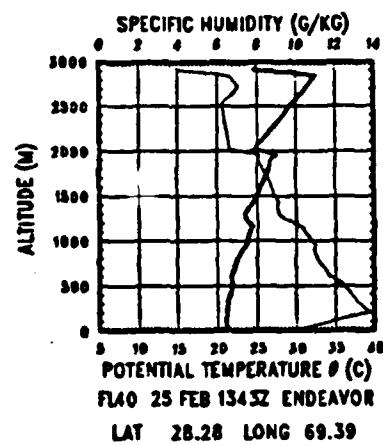
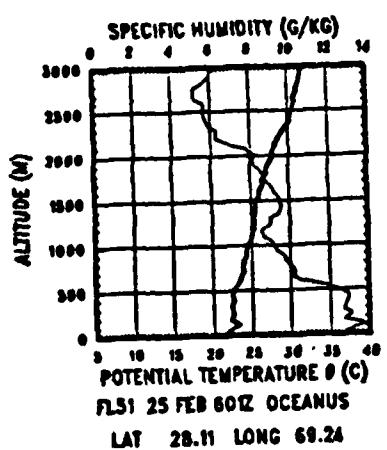


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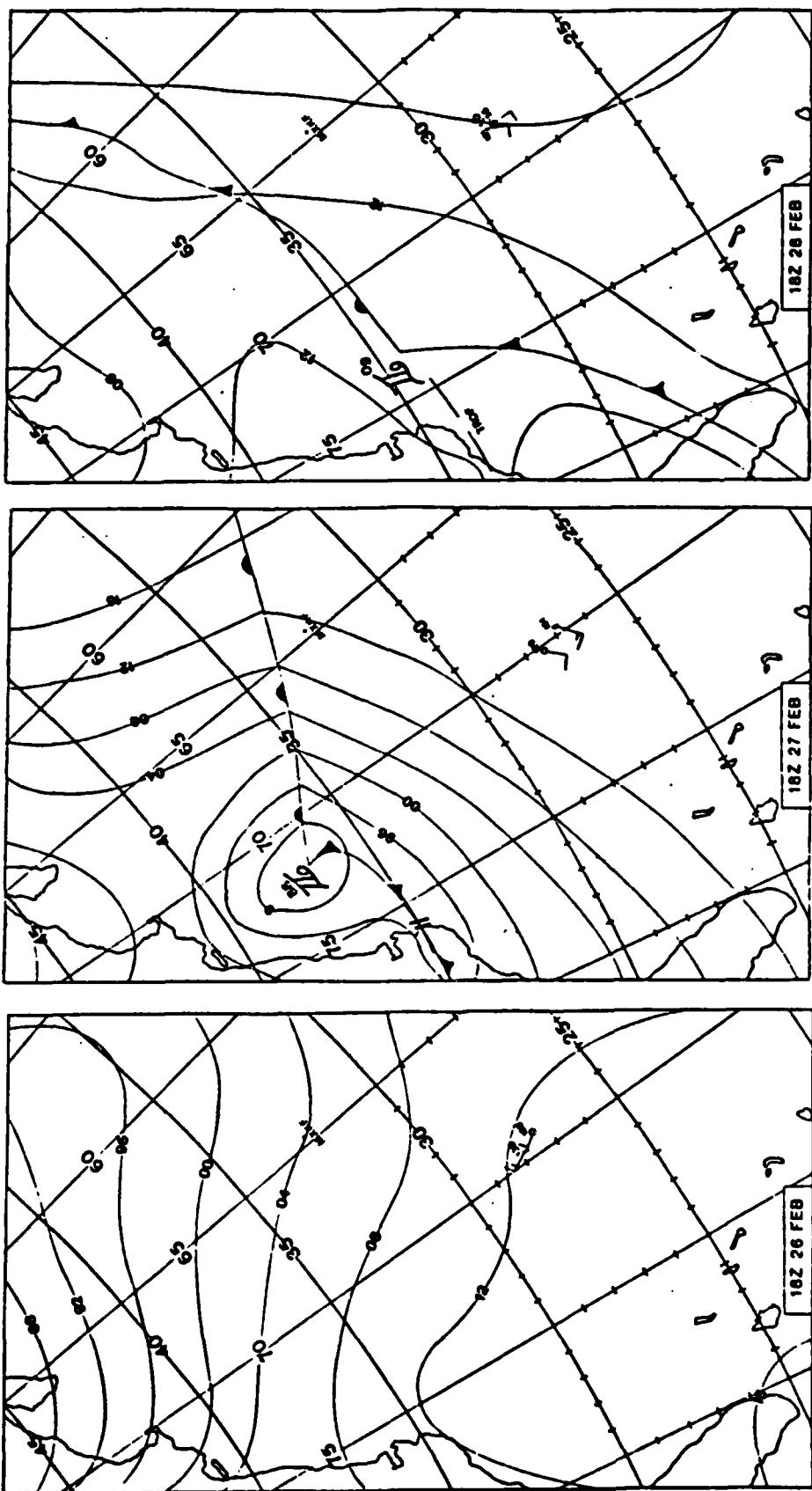


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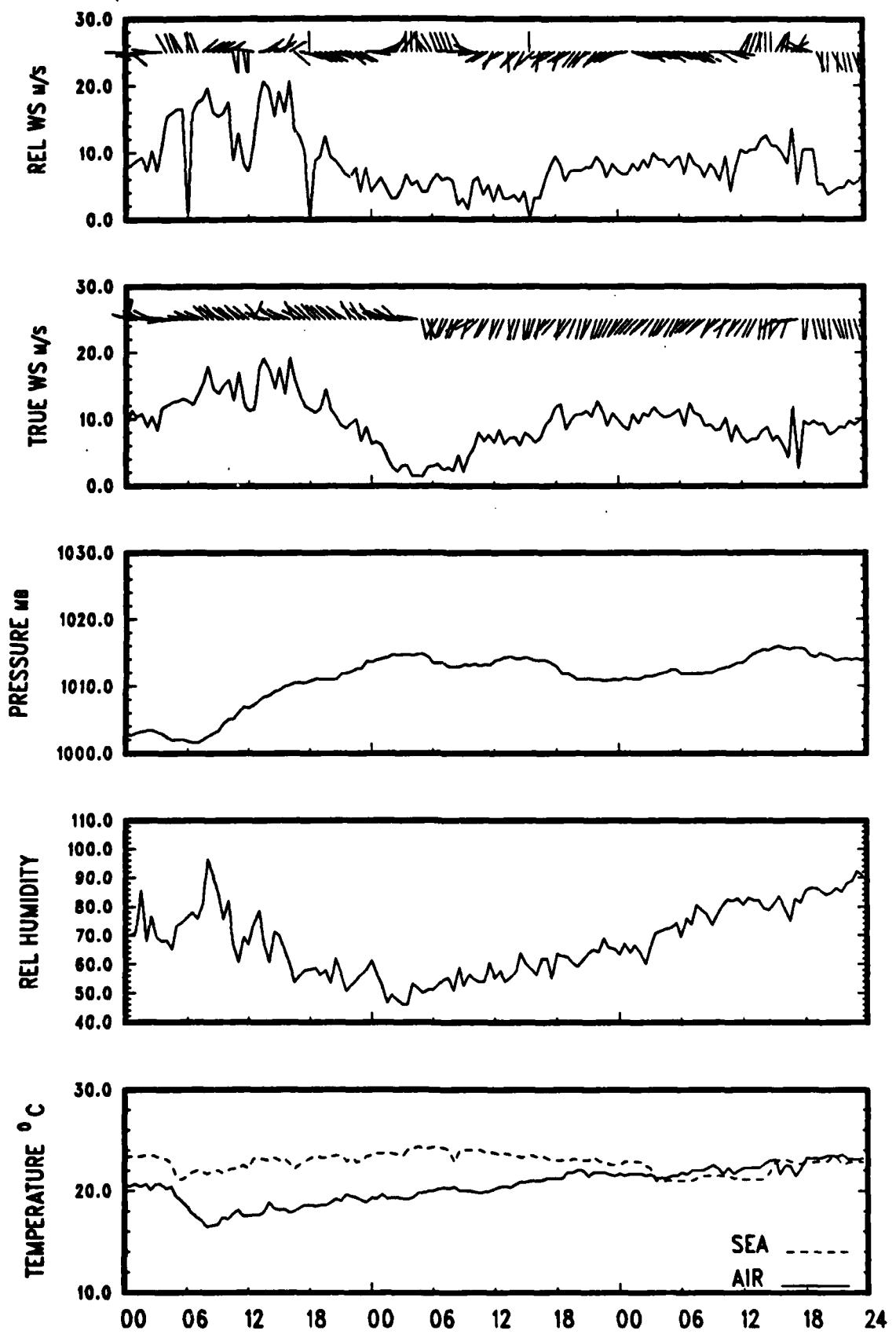
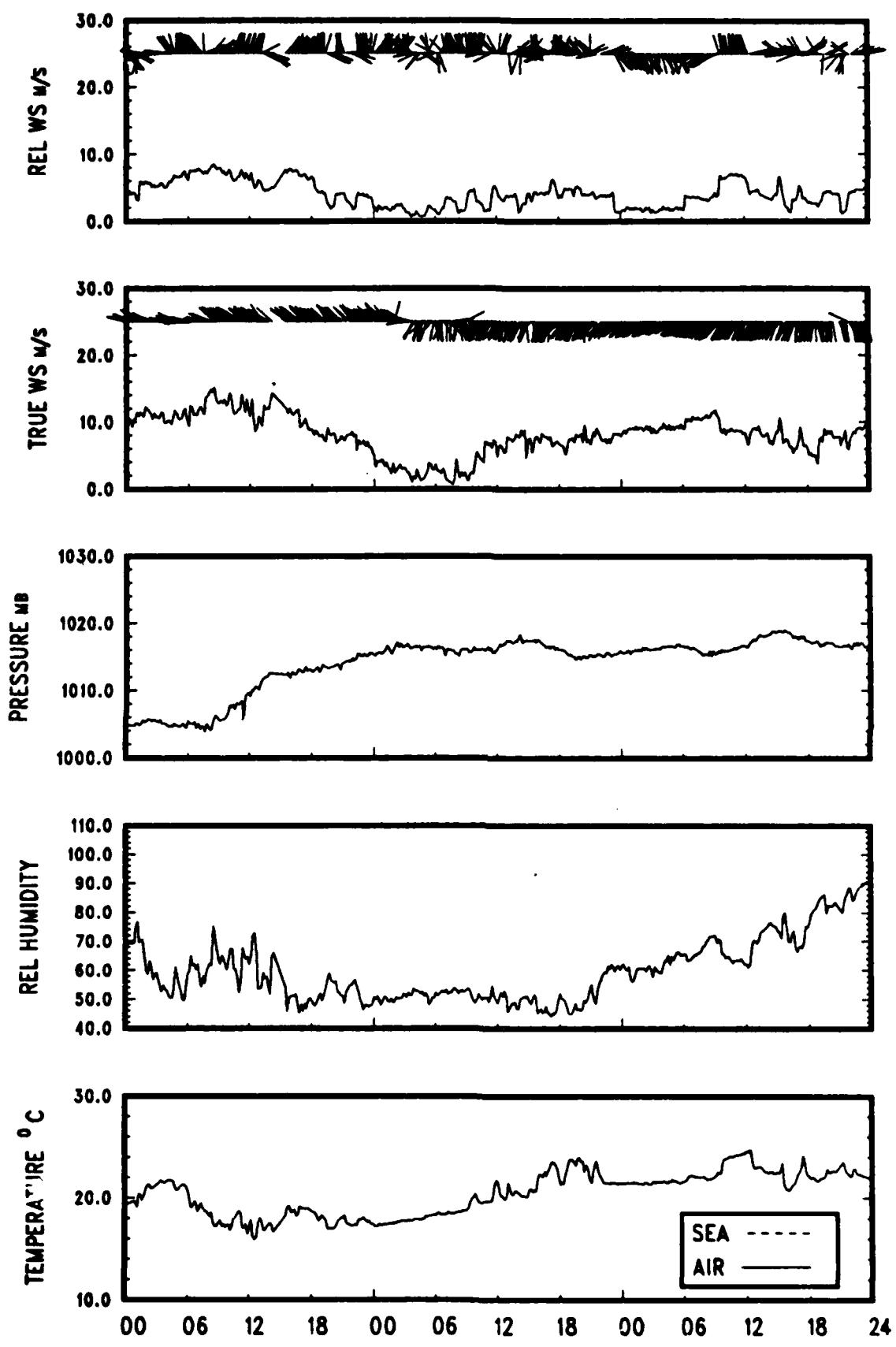


Fig Vb-1 (Cont) 26 FEB

FASINEX 1986 OCEANUS

28 FEB



26 FEB

FASINEX 1986 ENDEAVOR

28 FEB

Fig Vb-1 (Cont)

FASINEX RADIOSONDES

26 FEB - 28 FEB

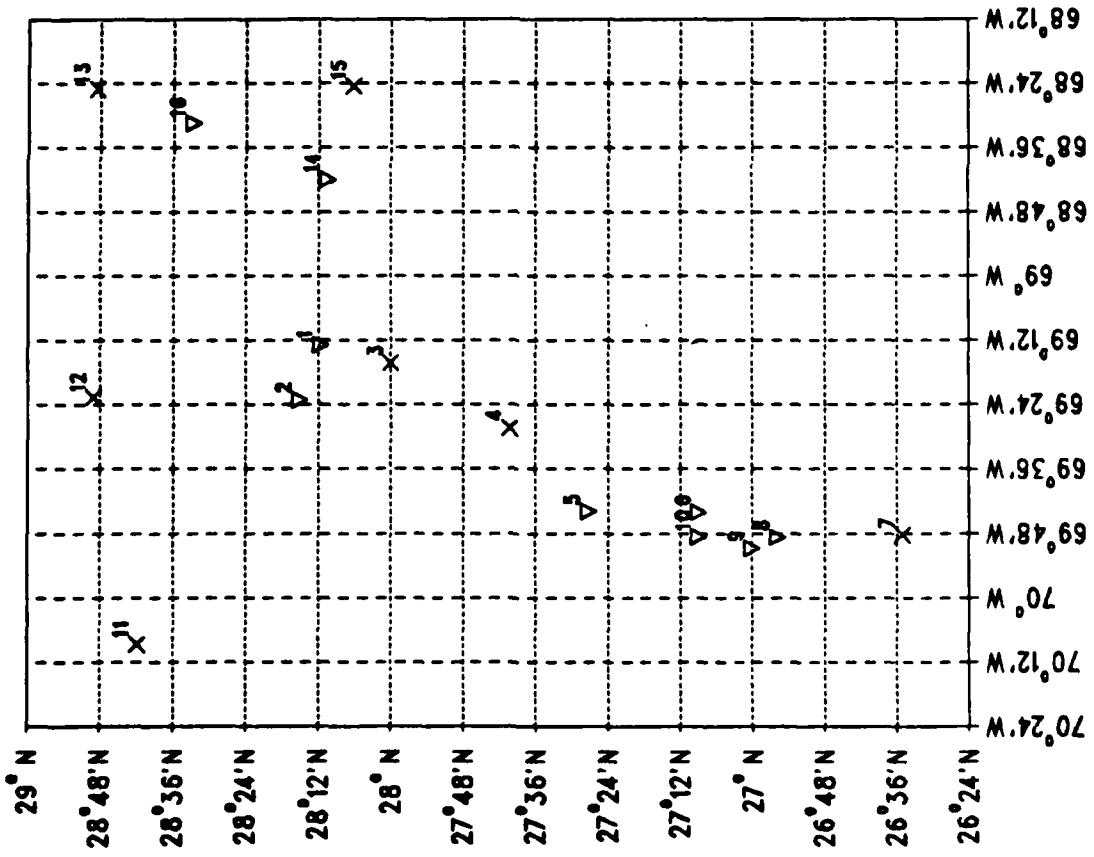


Fig Vb-1 (Cont)

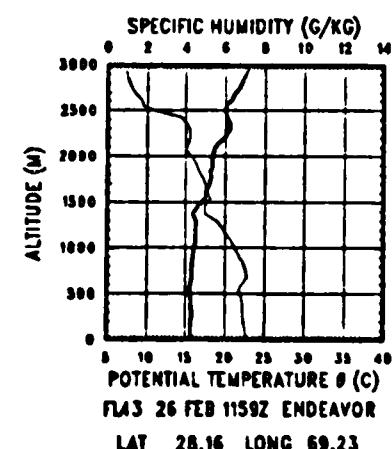
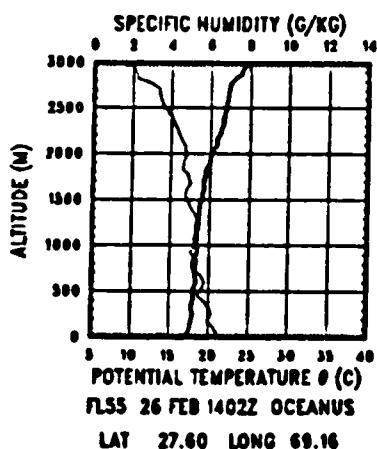
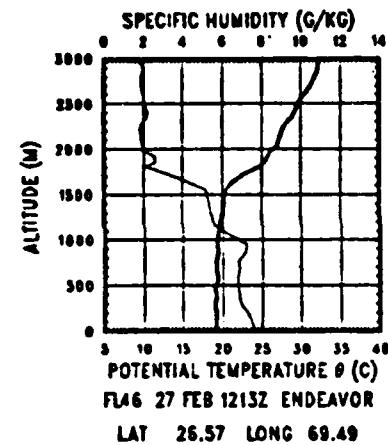
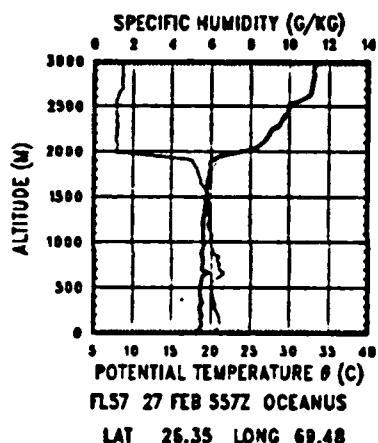
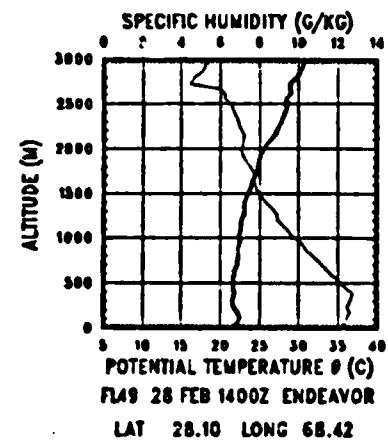
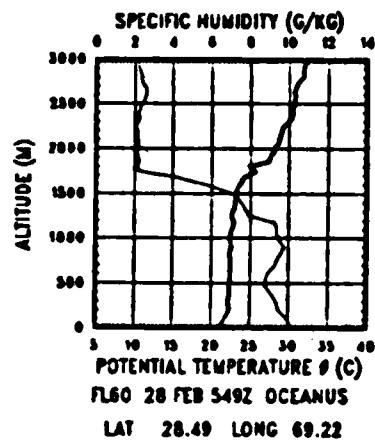


Fig Vb-1 (Cont)

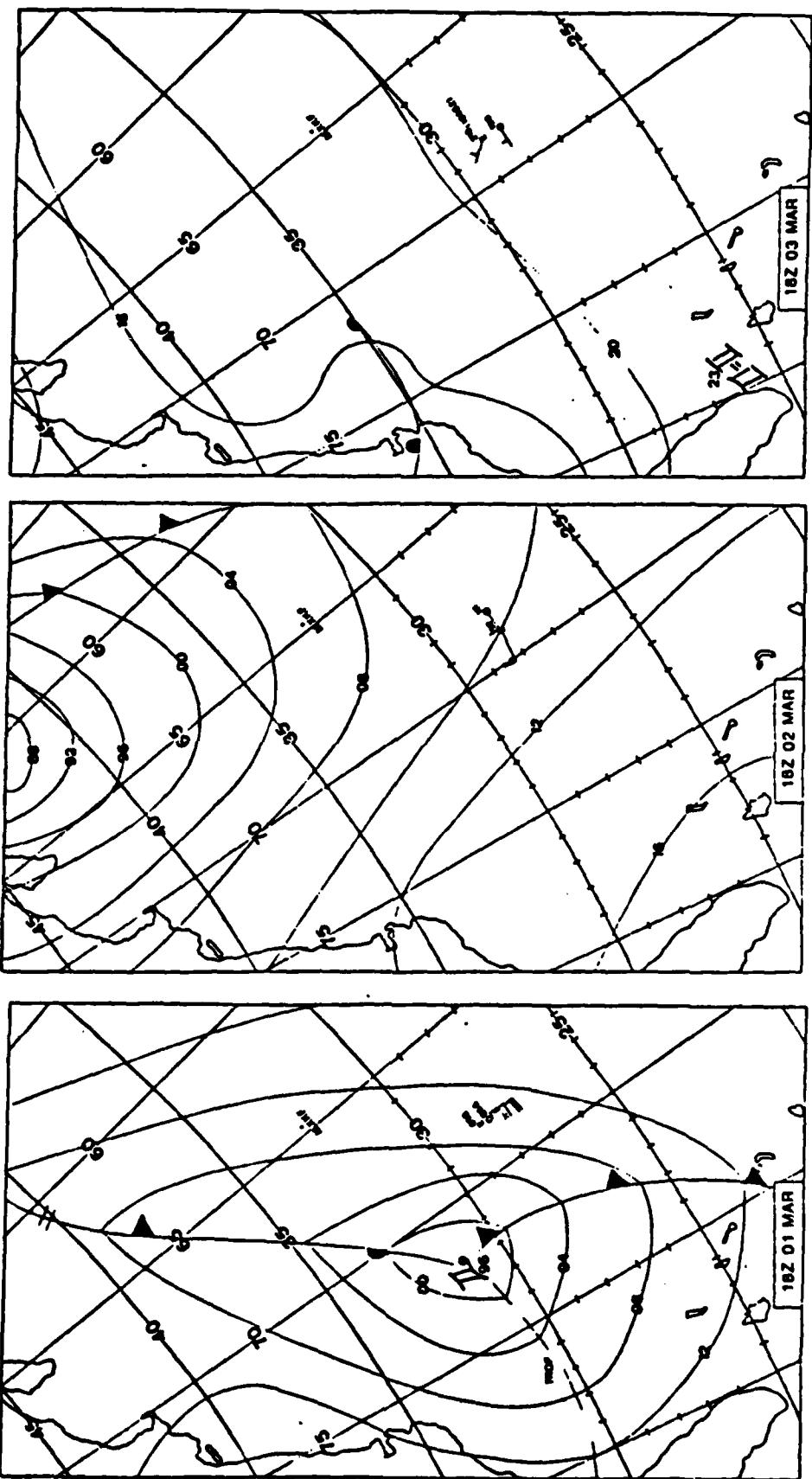


Fig Vb-1 (Cont)

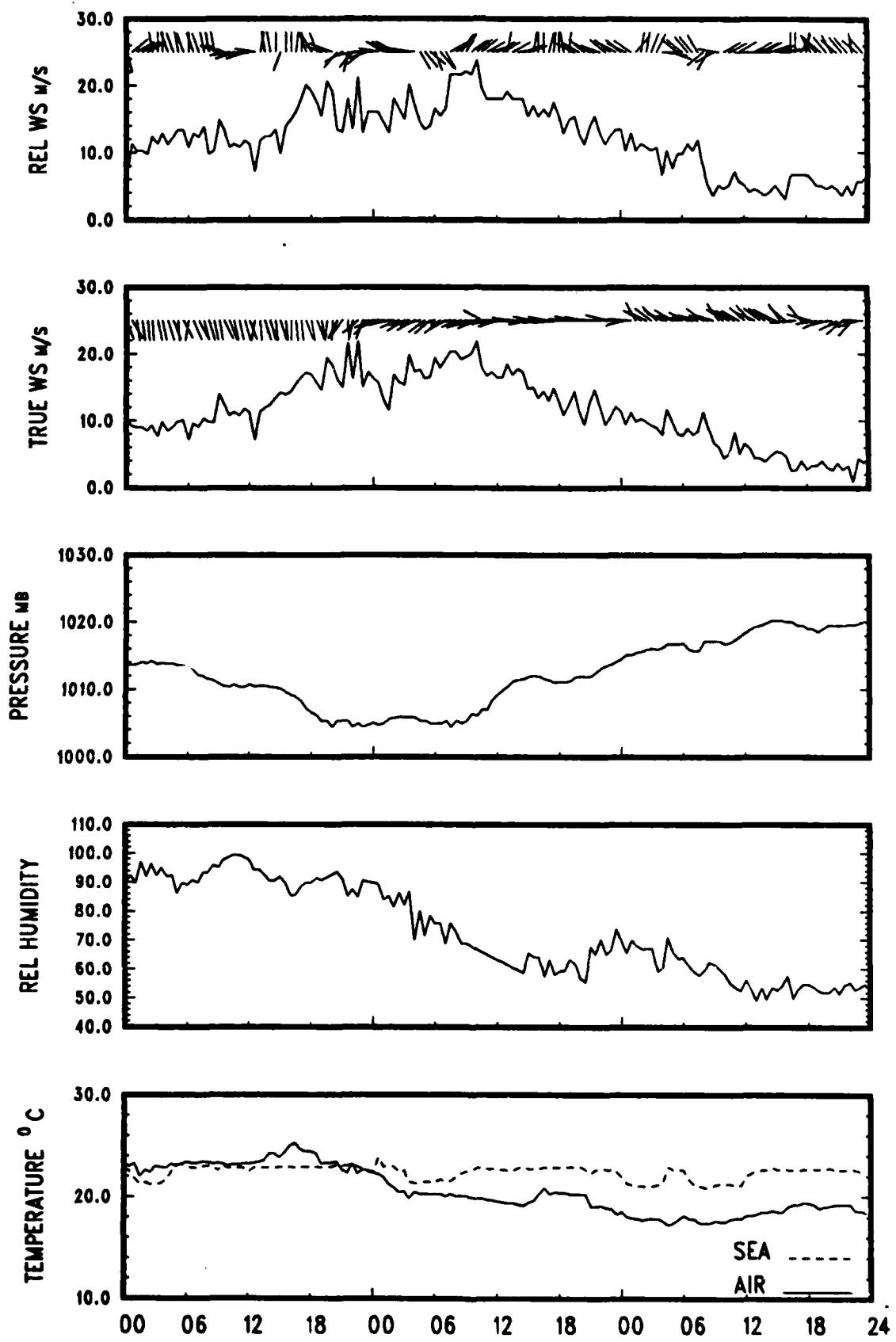
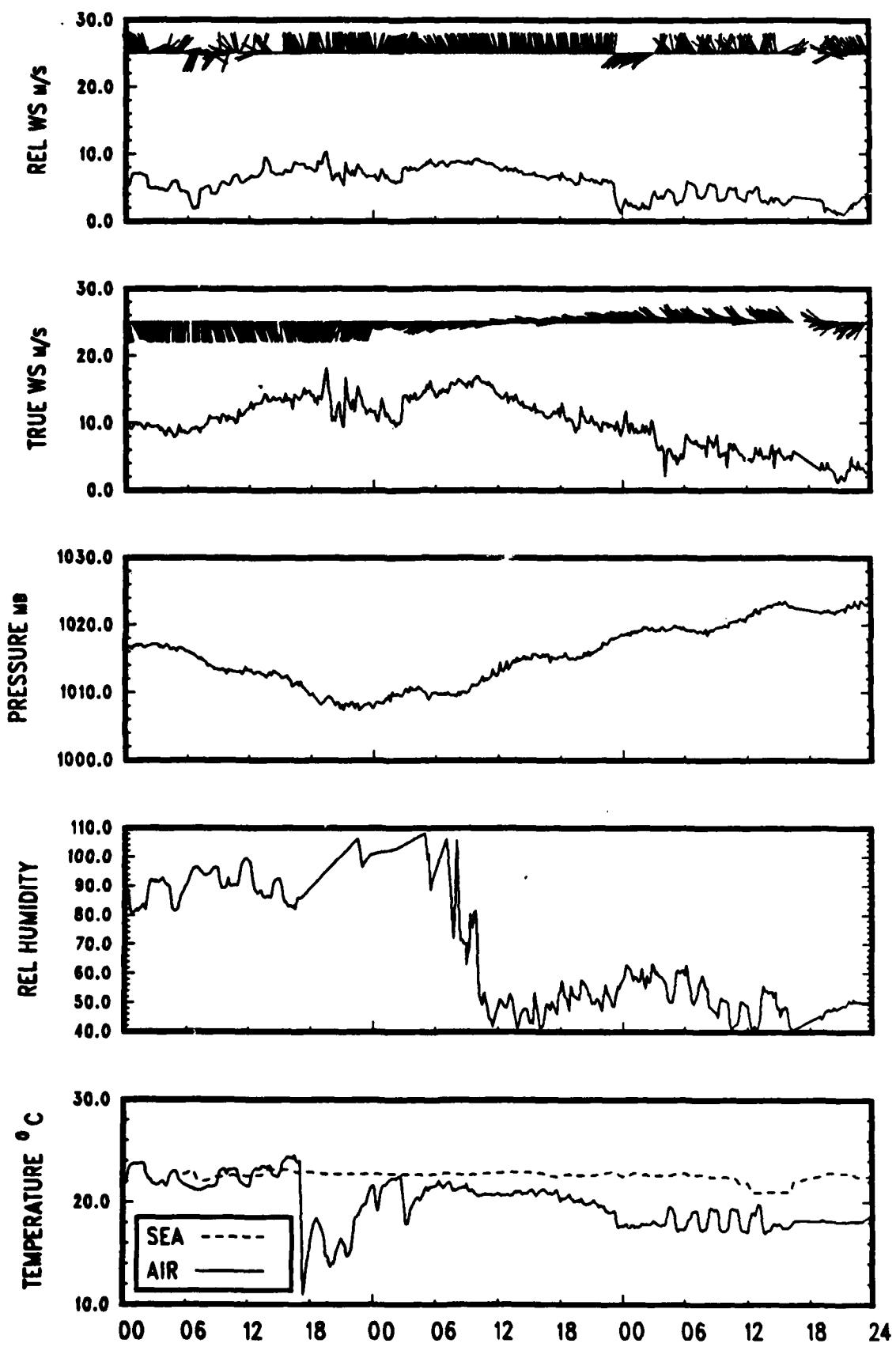


Fig Vb-1 (Cont)

FASINEX 1986 OCEANUS

03 MAR



01 MAR
Fig Vb-1 (Cont)

FASINEX 1986 ENDEAVOR

03 MAR

FASINEX RADIOSONDES
01 MAR - 03 MAR

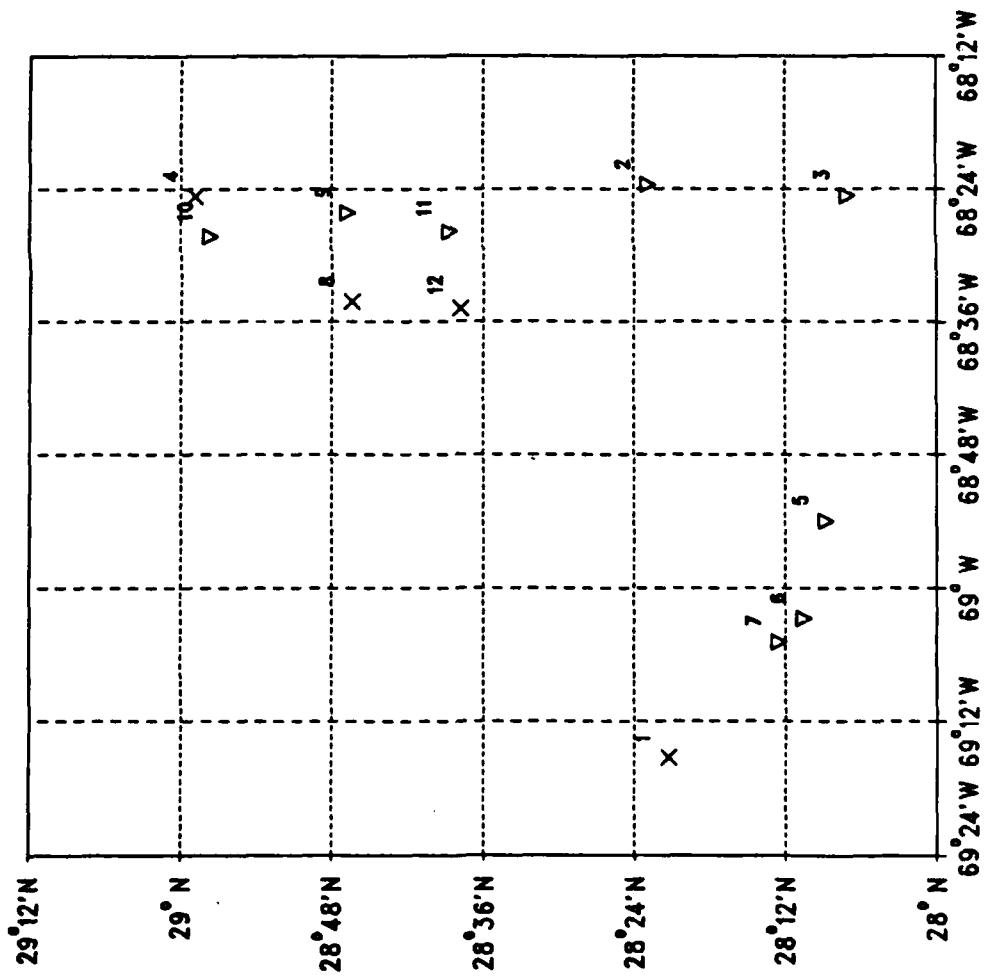


Fig Vb-1 (Cont)

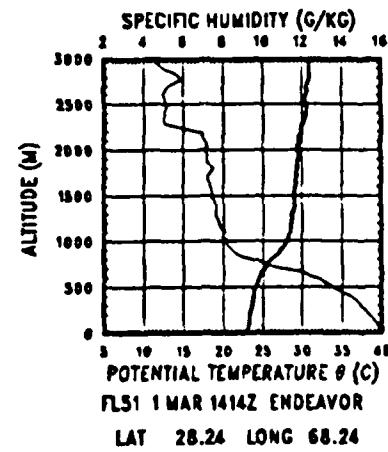
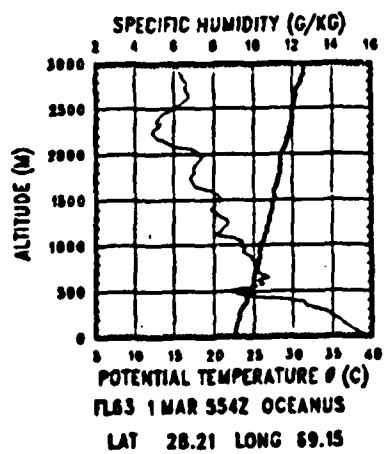
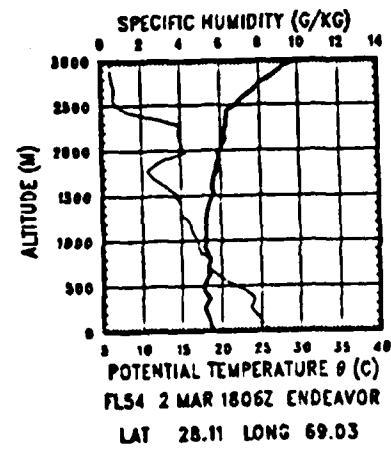
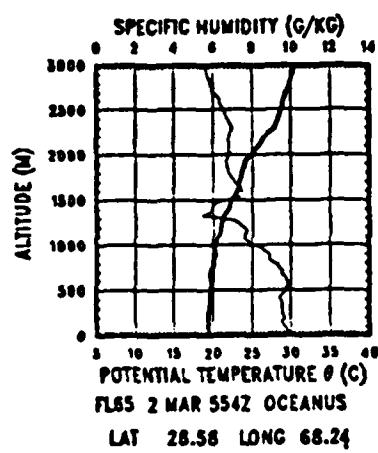
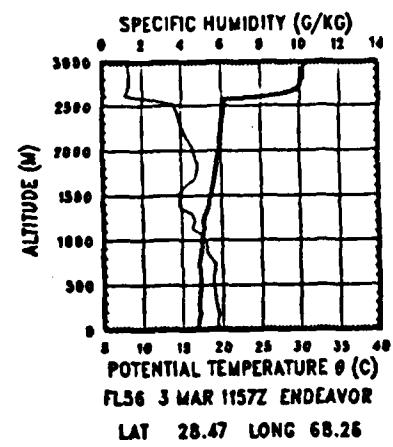
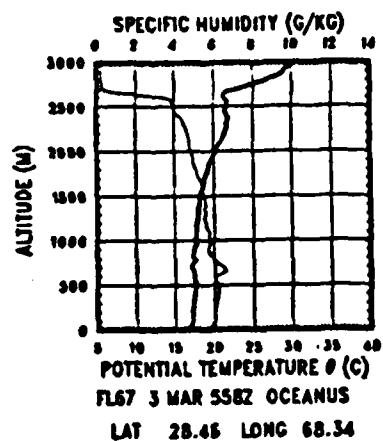


Fig Vb-1 (Cont)

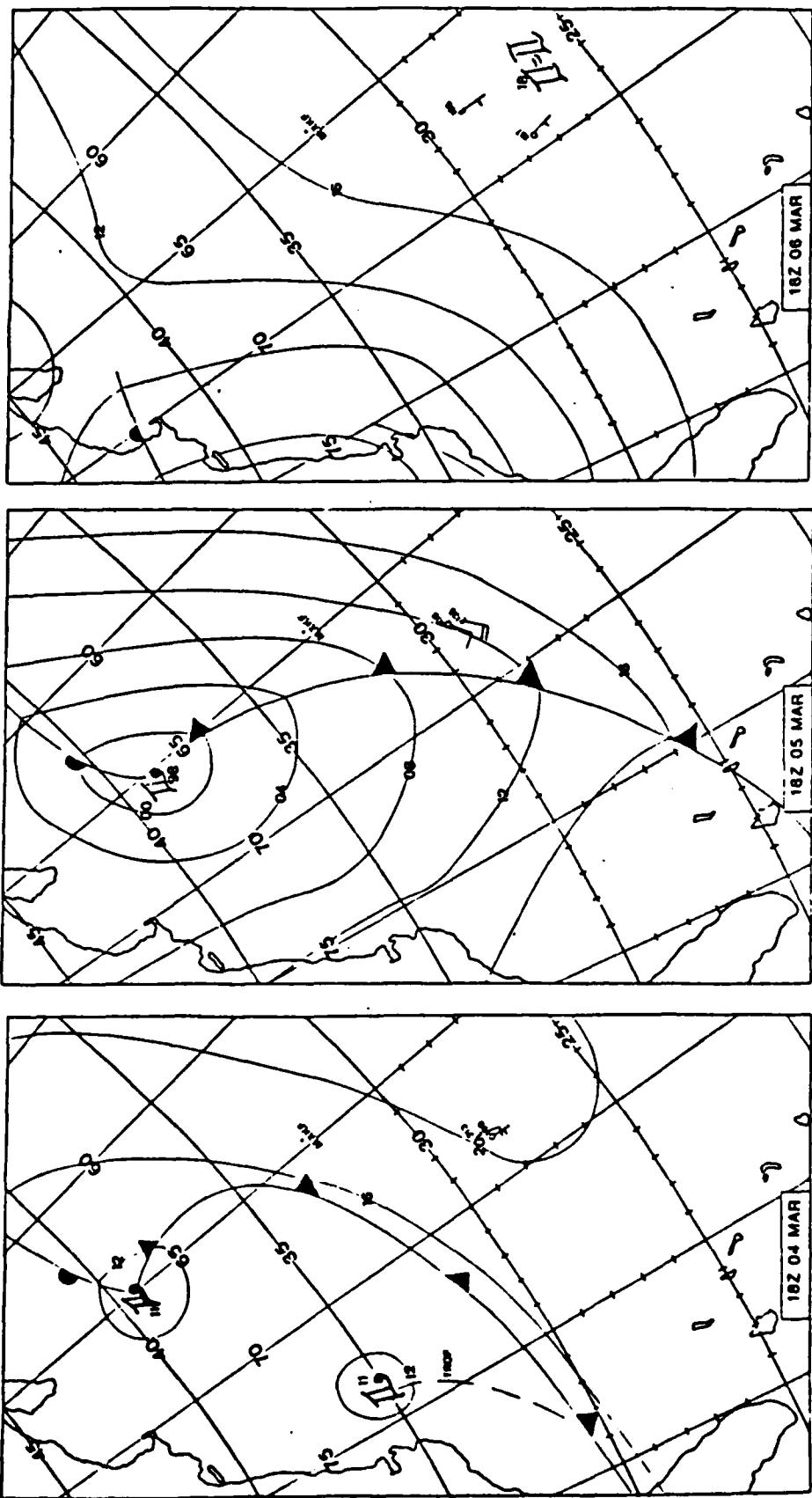


Fig Vb-1 (Cont)

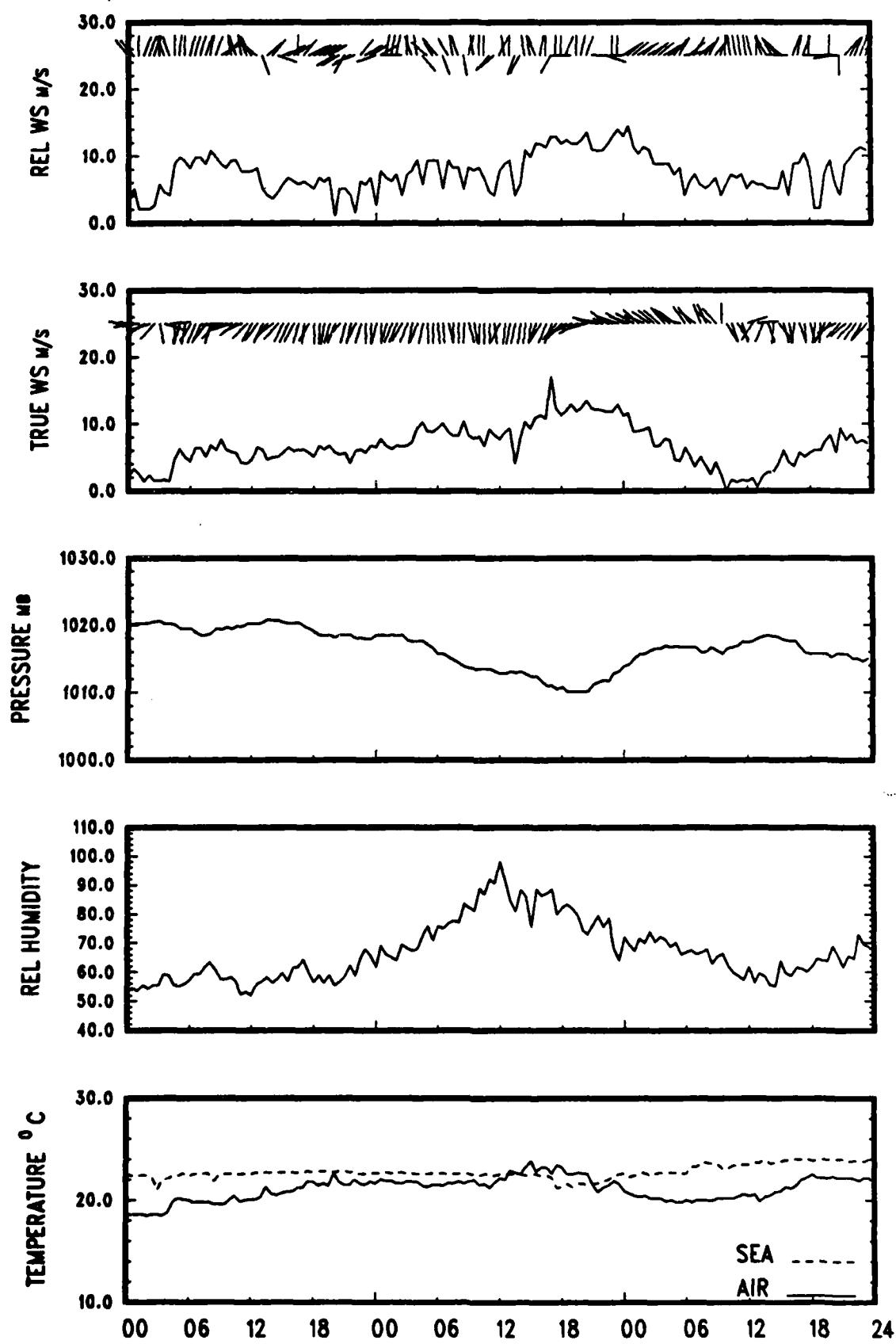


Fig Vb-1 (Cont) 04 MAR

FASINEX 1986 OCEANUS

06 MAR

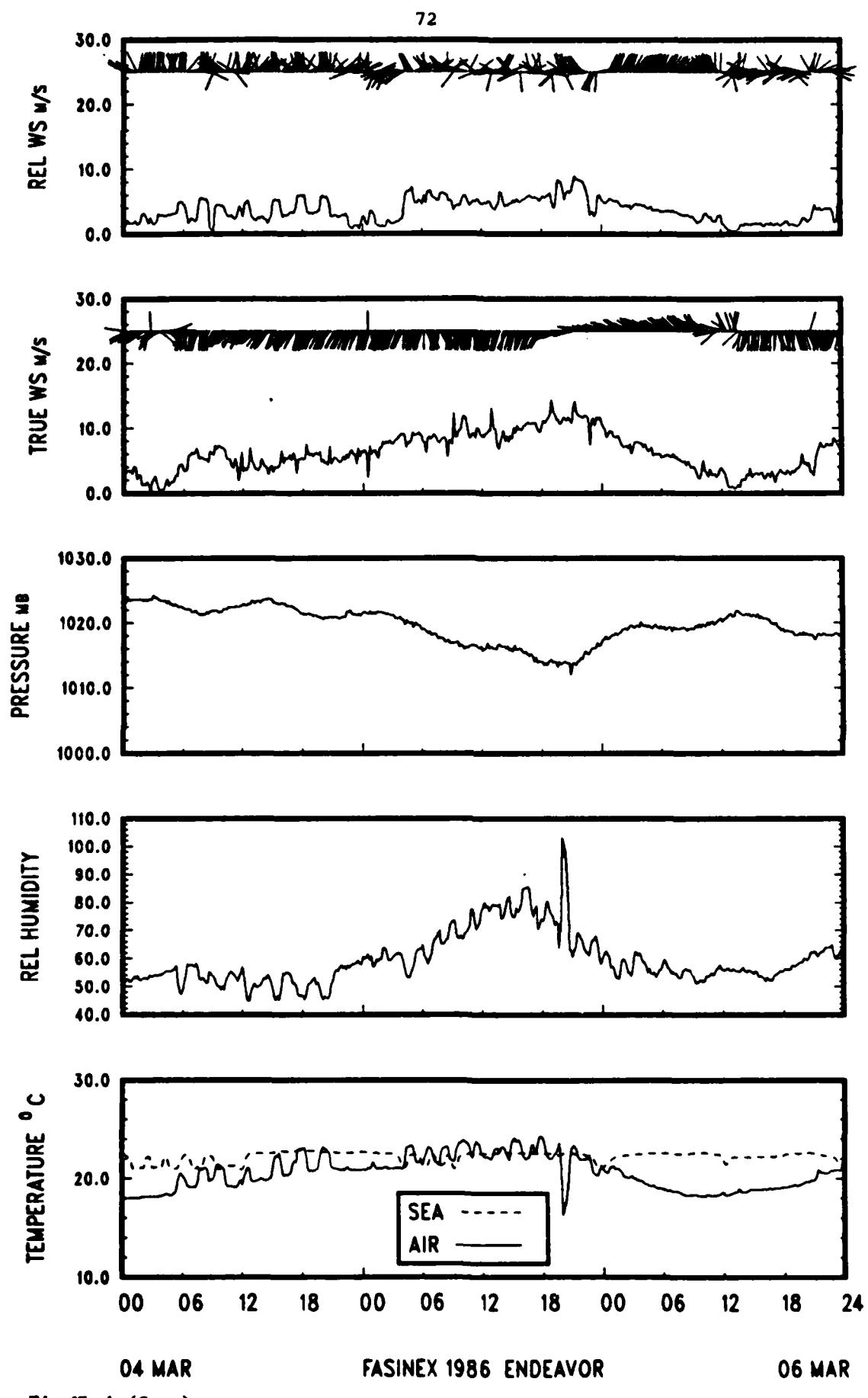


Fig Vb-1 (Cont)

FASINEX RADIOSONDES

04 MAR - 06 MAR

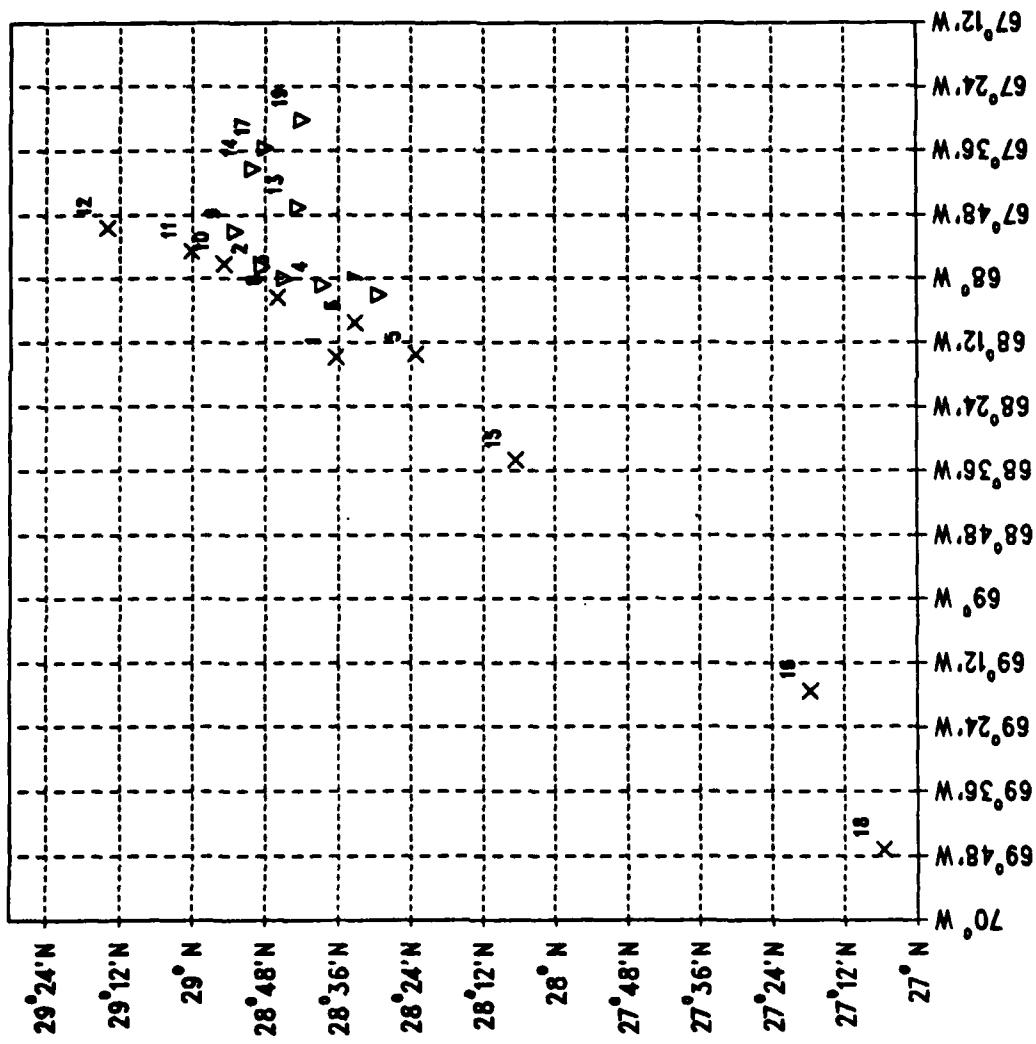


Fig Vb-1 (Cont)

1	4	557	OCE
2	4	1114	END
3	4	1156	END
4	4	1310	END
5	4	1926	OCE
6	4	2348	OCE
7	5	14	END
8	5	542	OCE
9	5	616	END
10	5	952	OCE
11	5	1331	OCE
12	5	1952	OCE
13	5	2054	END
14	6	5	END
15	6	602	OCE
16	6	1151	OCE
17	6	1226	END
18	6	1757	OCE
19	6	2001	END

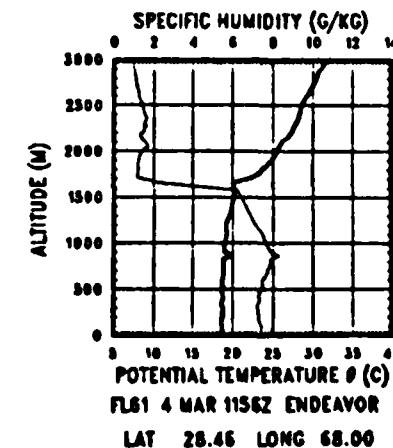
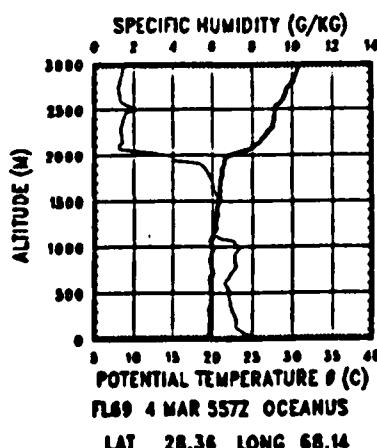
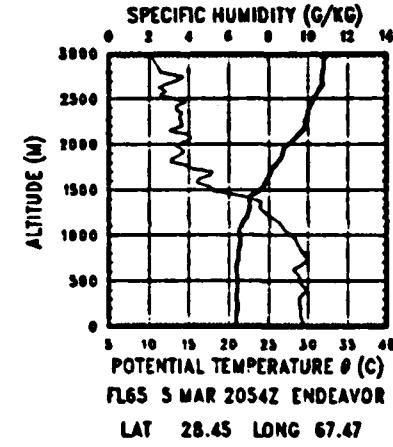
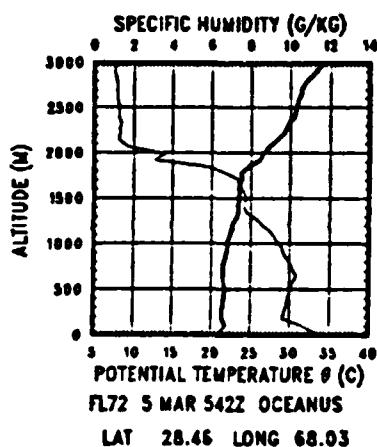
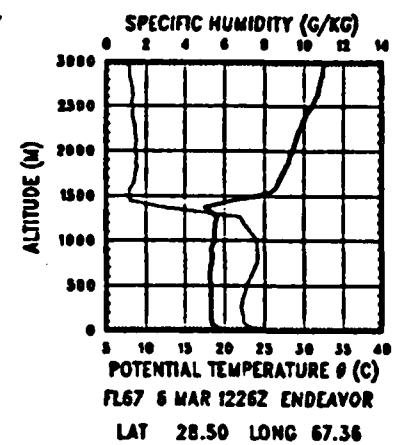
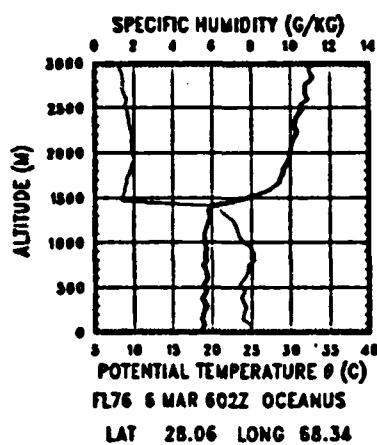


Fig Vb-1 (Cont)

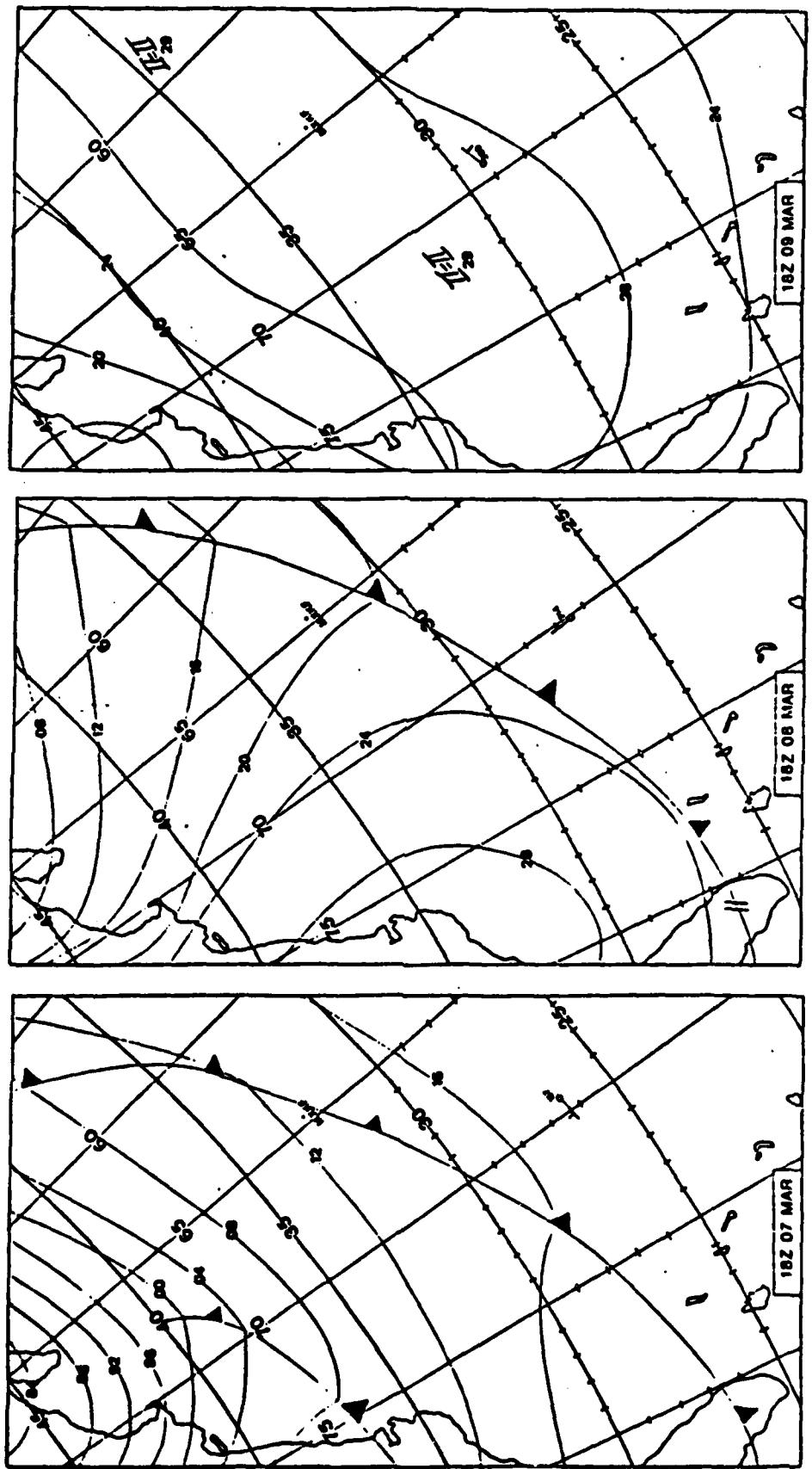


Fig Vb-1 (Cont)

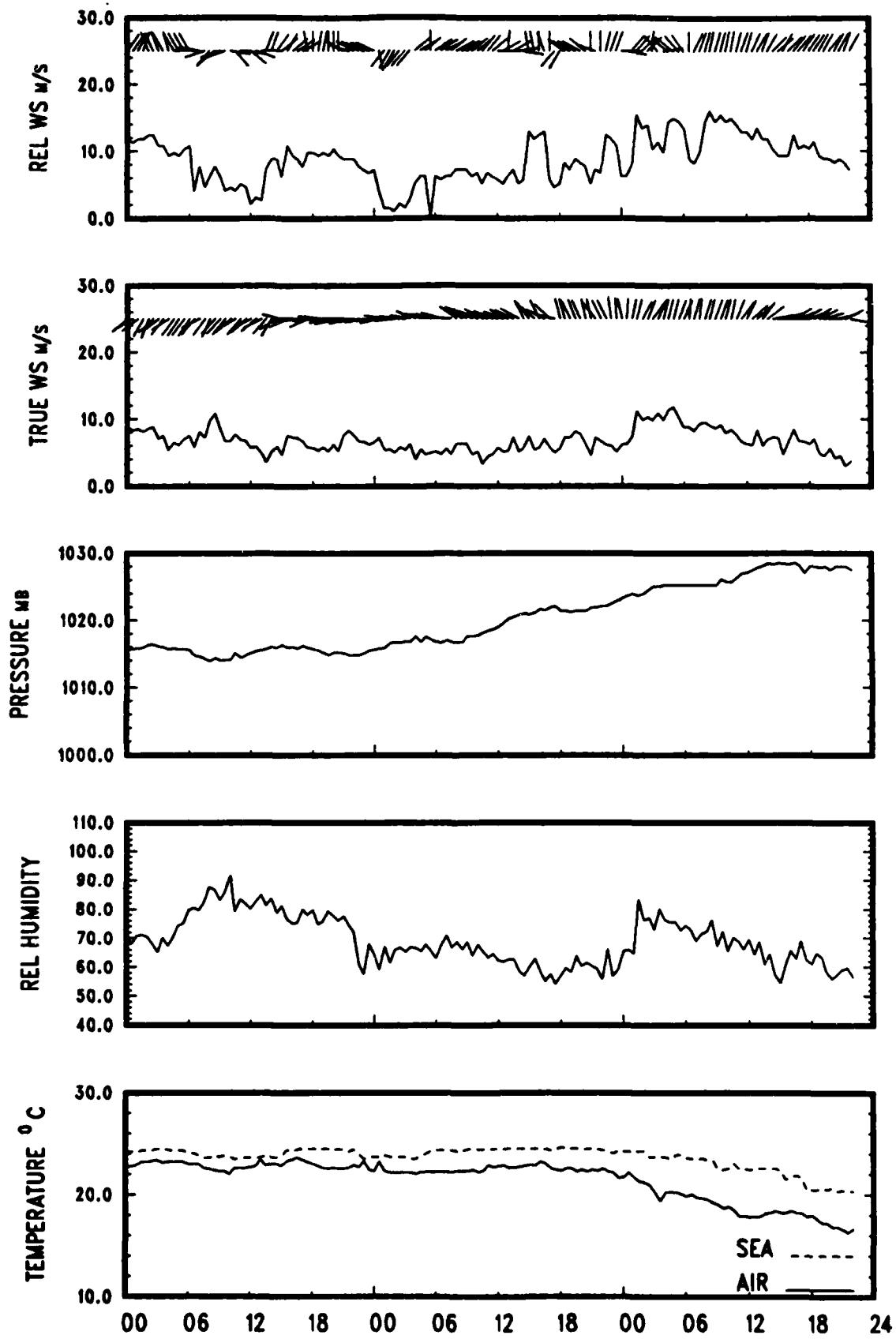


Fig Vb-1 (Cont)

07 MAR

FASINEX 1986 OCEANUS

09 MAR

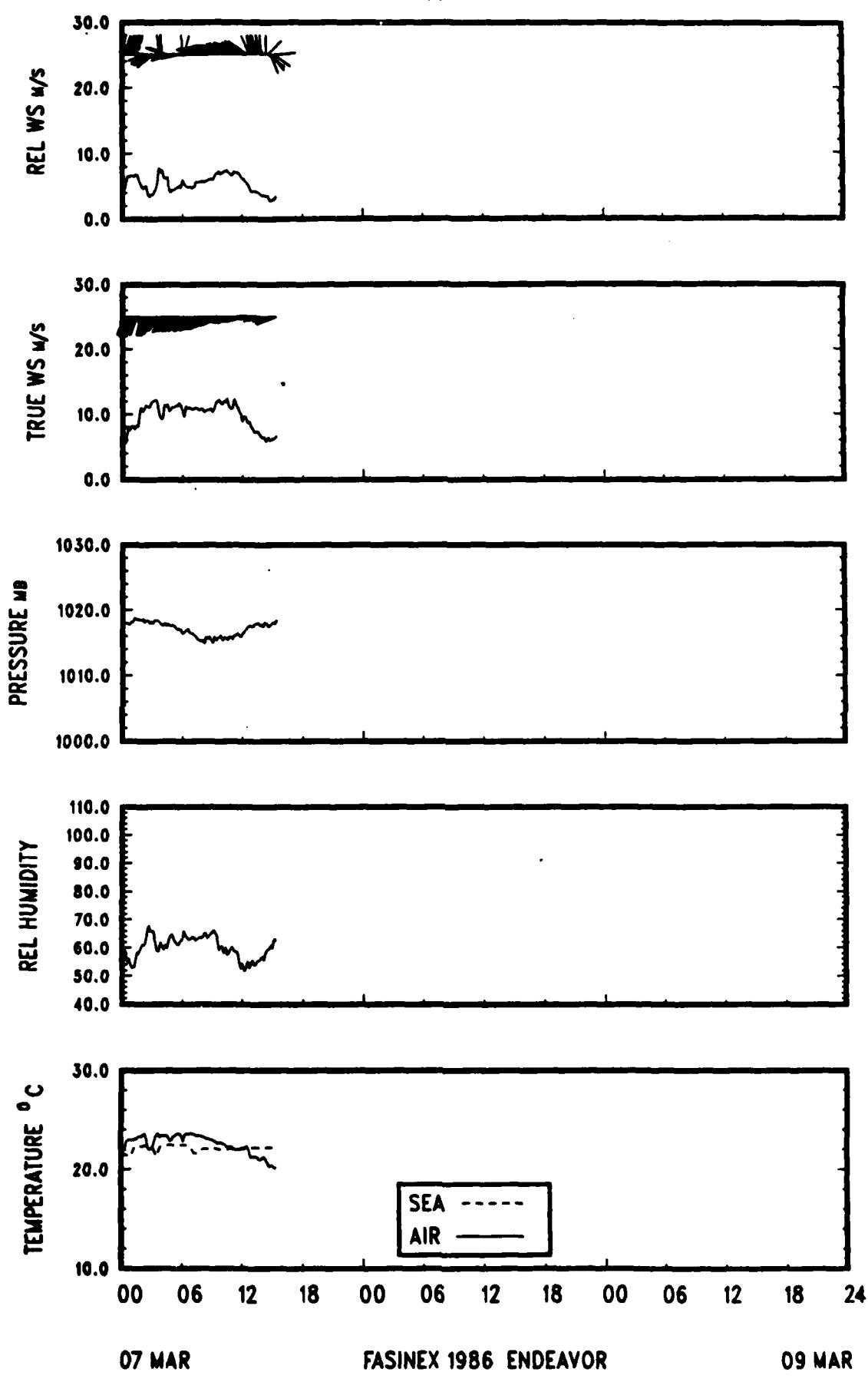


Fig Vb-1 (Cont)

FASINEX 1986 ENDEAVOR

FASINEX RADIOSONDES
07 MAR - 09 MAR

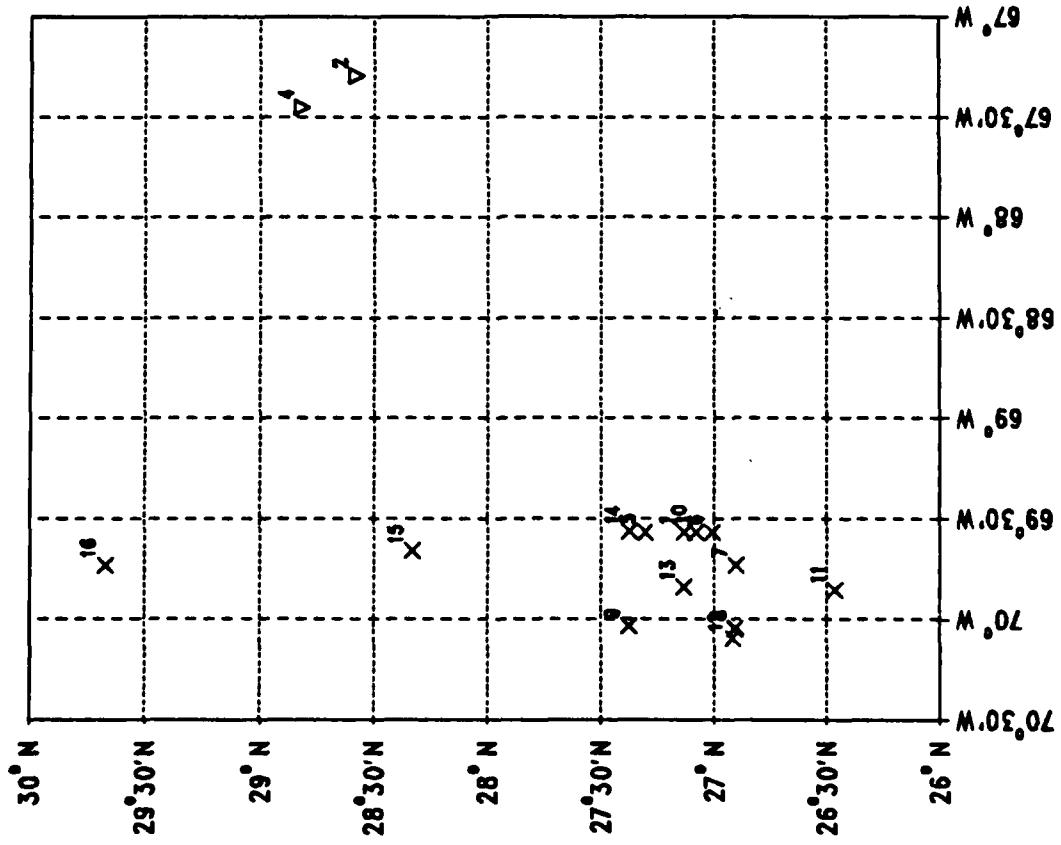


Fig Vb-1 (Cont)

1	7	11	OCE
2	7	14	END
3	7	551	OCE
4	7	606	END
5	7	1346	OCE
6	7	1609	OCE
7	7	1807	OCE
8	7	2026	OCE
9	8	25	OCE
10	8	611	OCE
11	8	1216	OCE
12	8	1756	OCE
13	8	2358	OCE
14	9	637	OCE
15	9	1223	OCE
16	9	1849	OCE

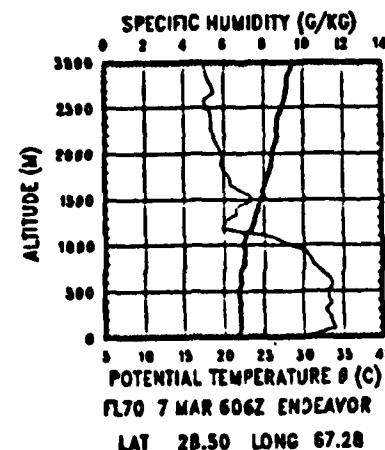
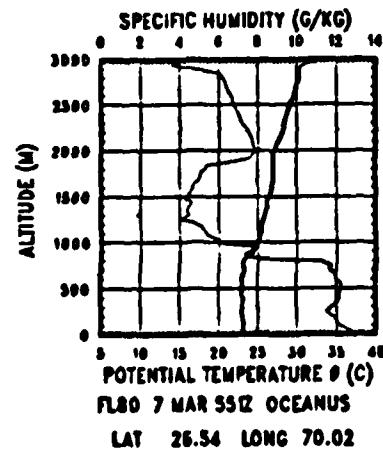
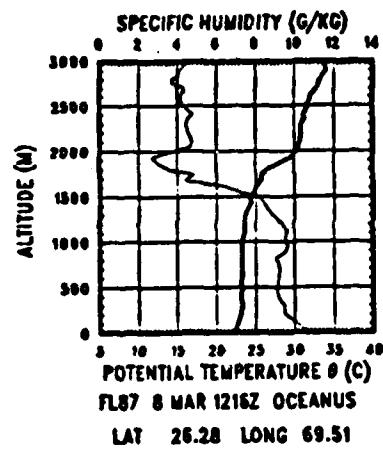
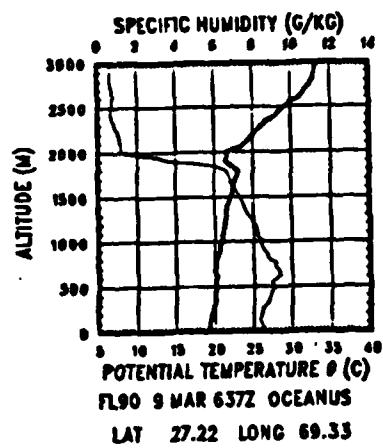


Fig Vb-1 (Cont)

FASINEX RADIOSONDES

10 MAR

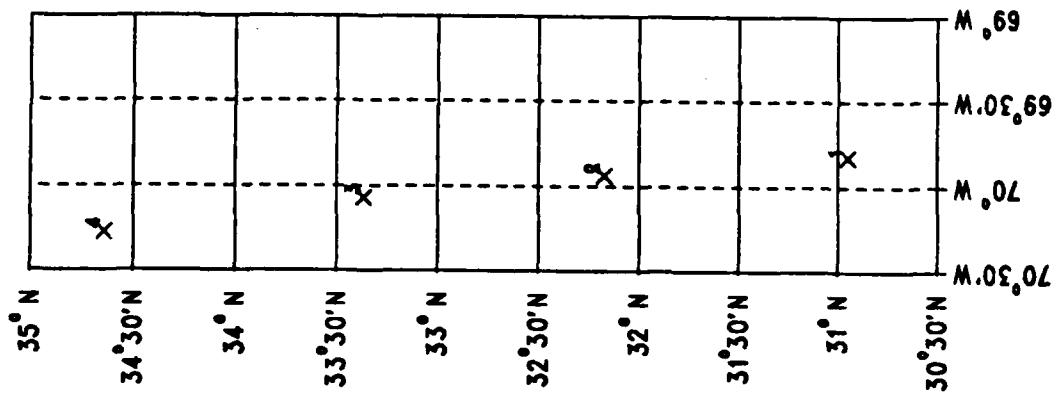


Fig Vb-1 (Cont)

TABLE Vb-1

**Naval Postgraduate School and University of Washington
Shipboard Meteorological Measurements**

Measurements on Endeavor only except those indicated by *.
***Indicates measurements on both Endeavor and Oceanus.**

<u>Measurements</u>	<u>Sensor/System</u>	<u>Endeavor and Oceanus Frequency</u>
Radiation (down)	Long/short wave radiometers (U of Washington)	Continuous
Sea Surface Temperature	Floating thermister	Continuous
Mean Surface layer: *Wind (speed, direction)	Cup anemometer, bivane	Continuous
Temperature	Resistance thermometer	Continuous
Humidity	Cool mirror	Continuous
Aerosols	Optical counters (.3 to 300 μm)	Continuous
*Turbulent Kinetic Energy Dissipation Rate	Hot film and miniature cups	Continuous
Humidity Variance Dissipation Rate	Lyman- α	Continuous
*Inversion Height	SODAR	Continuous
*Temperature, Humidity, and Wind Profiles	Radiosonde (LORAN-C Omega)	2 to 6/day

FASINEX Oceanus & Endeavor Radiosondes
o129

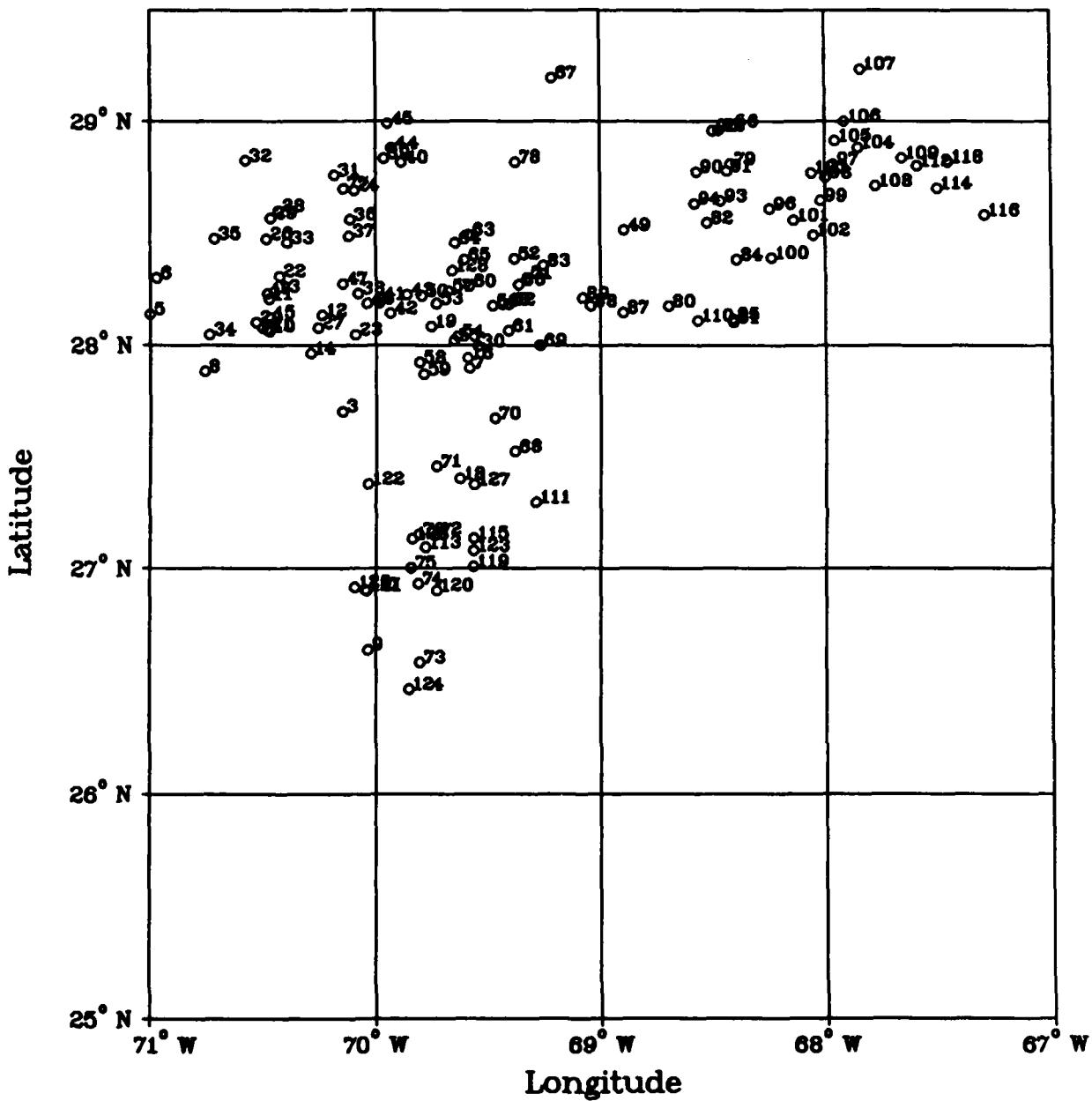


Figure Vb-2: Radiosonde Station Positions.

SAS			
DATE	TIME	SHIP	LOC
860213	1204	ENDEAVOR	69 59.13 28 11.22
	1714	OCEANUS	68 01.47 29 59.32
	1845	ENDEAVOR	70 09.01 27 42.26
860214	0018	ENDEAVOR	70 30.05 28 04.67
	1245	ENDEAVOR	71 00.10 28 08.30
	1510	ENDEAVOR	70 58.32 28 17.96
	1532	OCEANUS	69 35.13 27 53.93
	2345	ENDEAVOR	70 45.57 27 52.99
860215	0545	OCEANUS	70 02.09 26 39.35
	1207	ENDEAVOR	70 23.31 28 03.75
	1821	ENDEAVOR	70 28.51 28 12.38
860216	0043	ENDEAVOR	70 14.29 28 08.03
	0603	ENDEAVOR	70 27.01 28 14.38
	1731	OCEANUS	70 17.39 27 57.80
	1259	ENDEAVOR	70 28.07 28 07.39
	1933	OCEANUS	69 35.54 27 56.54
	2358	ENDEAVOR	70 26.94 28 13.86
	2358	OCEANUS	69 37.66 27 24.04
860217	0607	OCEANUS	69 45.21 28 05.03
	1213	ENDEAVOR	70 31.38 28 00.13
	1804	ENDEAVOR	70 29.00 28 04.26
	2352	ENDEAVOR	70 25.53 28 18.42
860218	0049	OCEANUS	70 05.40 28 02.31
	0548	OCEANUS	70 25.72 28 41.39
	1200	ENDEAVOR	70 27.71 28 22.99
	1459	ENDEAVOR	70 29.03 28 26.41
	1621	OCEANUS	70 15.38 26 54.59
	1826	ENDEAVOR	70 25.38 28 35.92
860219	0010	ENDEAVOR	70 27.97 28 33.97
	0603	OCEANUS	69 32.79 27 59.76
	1212	ENDEAVOR	70 11.11 29 45.57
	1215	OCEANUS	70 34.58 28 49.43
	1757	ENDEAVOR	70 23.53 28 27.37
	2027	OCEANUS	70 44.21 28 32.86
	2334	OCEANUS	70 42.97 29 28.46
860220	0645	OCEANUS	70 26.81 28 33.56
	1211	ENDEAVOR	70 07.10 28 29.11
	1441	OCEANUS	70 04.78 28 13.83
	1507	ENDEAVOR	69 57.75 28 50.03
	1854	ENDEAVOR	69 53.26 28 49.03
	2023	OCEANUS	69 59.12 28 12.43
860221	0052	ENDEAVOR	69 56.15 28 08.54
	1216	ENDEAVOR	69 51.76 28 13.52
	1515	OCEANUS	69 55.77 28 52.47
	1915	OCEANUS	69 56.90 28 59.45
	1952	ENDEAVOR	70 02.33 28 11.17
860222	0001	ENDEAVOR	70 08.97 28 16.42
	0612	OCEANUS	69 26.19 28 10.94
	1201	ENDEAVOR	68 53.62 28 30.80
	1825	OCEANUS	69 47.84 28 13.19
	1919	ENDEAVOR	69 19.05 28 18.03
860223	0000	ENDEAVOR	69 23.01 28 23.11
	0516	OCEANUS	69 43.86 28 11.17
	1201	ENDEAVOR	69 38.11 28 02.33
	2027	ENDEAVOR	69 41.65 28 02.23

Table Vb-2: Radiosonde Launch Times and Locations.

SAS				
DATE	TIME	SHIP	LOC	
860224	0001	ENDEAVOR	69 39.06	28 01.19
	0545	OCEANUS	69 28.86	28 10.58
	1359	OCEANUS	69 50.73	28 14.46
	1413	ENDEAVOR	69 48.43	27 55.41
	1832	ENDEAVOR	69 47.29	27 52.28
	2020	OCEANUS	69 35.10	28 15.82
	2356	ENDEAVOR	69 24.61	28 03.90
860225	0601	OCEANUS	69 24.55	28 10.97
	1230	ENDEAVOR	69 35.23	28 29.52
	1343	ENDEAVOR	69 39.81	28 27.29
	1759	ENDEAVOR	69 30.40	28 22.79
	2233	OCEANUS	69 21.94	28 16.19
860226	0008	ENDEAVOR	69 12.33	28 11.75
	1150	ENDEAVOR	69 23.00	28 15.21
	1402	OCEANUS	69 16.18	27 59.98
	1325	OCEANUS	69 26.38	27 40.36
	2306	ENDEAVOR	69 43.80	27 27.35
860227	0315	ENDEAVOR	69 43.94	27 09.06
	0557	OCEANUS	69 48.25	26 35.02
	1213	ENDEAVOR	69 48.66	26 55.91
	1826	ENDEAVOR	69 50.62	27 00.17
	2357	OCEANUS	69 48.58	27 09.05
860228	0016	OCEANUS	70 08.60	28 41.90
	0549	OCEANUS	69 22.50	28 49.08
	1156	OCEANUS	68 25.35	28 48.61
	1400	ENDEAVOR	68 41.37	29 10.54
	1748	OCEANUS	68 24.42	28 26.24
	2351	ENDEAVOR	68 31.40	28 32.70
860301	0554	OCEANUS	69 15.22	28 21.31
	1414	ENDEAVOR	68 23.59	28 22.91
860302	0008	ENDEAVOR	68 24.54	28 07.01
	0554	OCEANUS	68 24.66	28 58.81
	1449	ENDEAVOR	68 53.95	28 08.76
	1806	ENDEAVOR	69 02.73	28 10.55
860303	0010	ENDEAVOR	69 04.83	23 12.56
	0558	OCEANUS	68 34.19	24 46.46
	1157	ENDEAVOR	68 20.10	23 46.70
	1520	ENDEAVOR	68 28.22	28 57.64
	2054	ENDEAVOR	68 27.82	28 38.64
	2210	OCEANUS	68 34.80	28 37.87
	2359	ENDEAVOR	68 29.85	28 57.48
860304	0557	OCEANUS	68 14.71	28 36.52
	1114	ENDEAVOR	67 57.68	28 48.56
	1156	ENDEAVOR	67 59.86	28 44.93
	1310	ENDEAVOR	68 01.15	28 38.68
	1926	OCEANUS	68 14.29	28 23.36
	2348	OCEANUS	68 08.31	28 33.42
860305	0014	ENDEAVOR	68 03.72	28 29.44
	0542	OCEANUS	68 03.56	28 46.17
	0616	ENDEAVOR	67 51.10	28 53.00
	0952	OCEANUS	67 57.23	28 54.86
	1331	OCEANUS	67 54.77	29 00.13
	1752	OCEANUS	67 50.41	29 14.12
	2054	ENDEAVOR	67 46.56	29 42.65
860306	0005	ENDEAVOR	67 39.44	28 50.15
	0602	OCEANUS	68 34.00	28 06.60
	1151	OCEANUS	69 17.30	27 17.70
	1226	ENDEAVOR	67 35.44	28 48.04
	1757	OCEANUS	69 46.84	27 05.61
	2001	ENDEAVOR	67 30.19	28 42.00

Table Vb-2 (Cont)

SAS			
DATE	TIME	SHIP	LOC
860307	0011	OCEANUS	69 33-98 27 08-04
	0014	ENDEAVOR	69 17-67 28 34-03
	0551	OCEANUS	70 04-76 26 54-37
	0606	ENDEAVOR	69 21-18 28 59-12
	1346	OCEANUS	69 23-96 27 18-29
	1609	OCEANUS	69 24-04 27 00-52
	1807	OCEANUS	69 23-73 26 54-14
860308	2726	OCEANUS	70 02-42 26 54-08
	0025	OCEANUS	70 22-06 27 22-57
	0611	OCEANUS	69 23-99 27 04-78
	1216	OCEANUS	69 24-21 26 27-90
	1756	OCEANUS	70 25-57 26 54-97
860309	2358	OCEANUS	69 25-37 27 07-88
	0637	OCEANUS	69 33-79 27 22-50
	1223	OCEANUS	69 39-60 28 19-30
860310	1849	OCEANUS	69 43-72 29 40-40
	0036	OCEANUS	69 49-57 30 57-14
	0612	OCEANUS	69 56-28 32 10-46
	1144	OCEANUS	70 14-51 34 21-94
	1740	OCEANUS	70 16-51 34 38-44

Table Vb-2 (Cont)

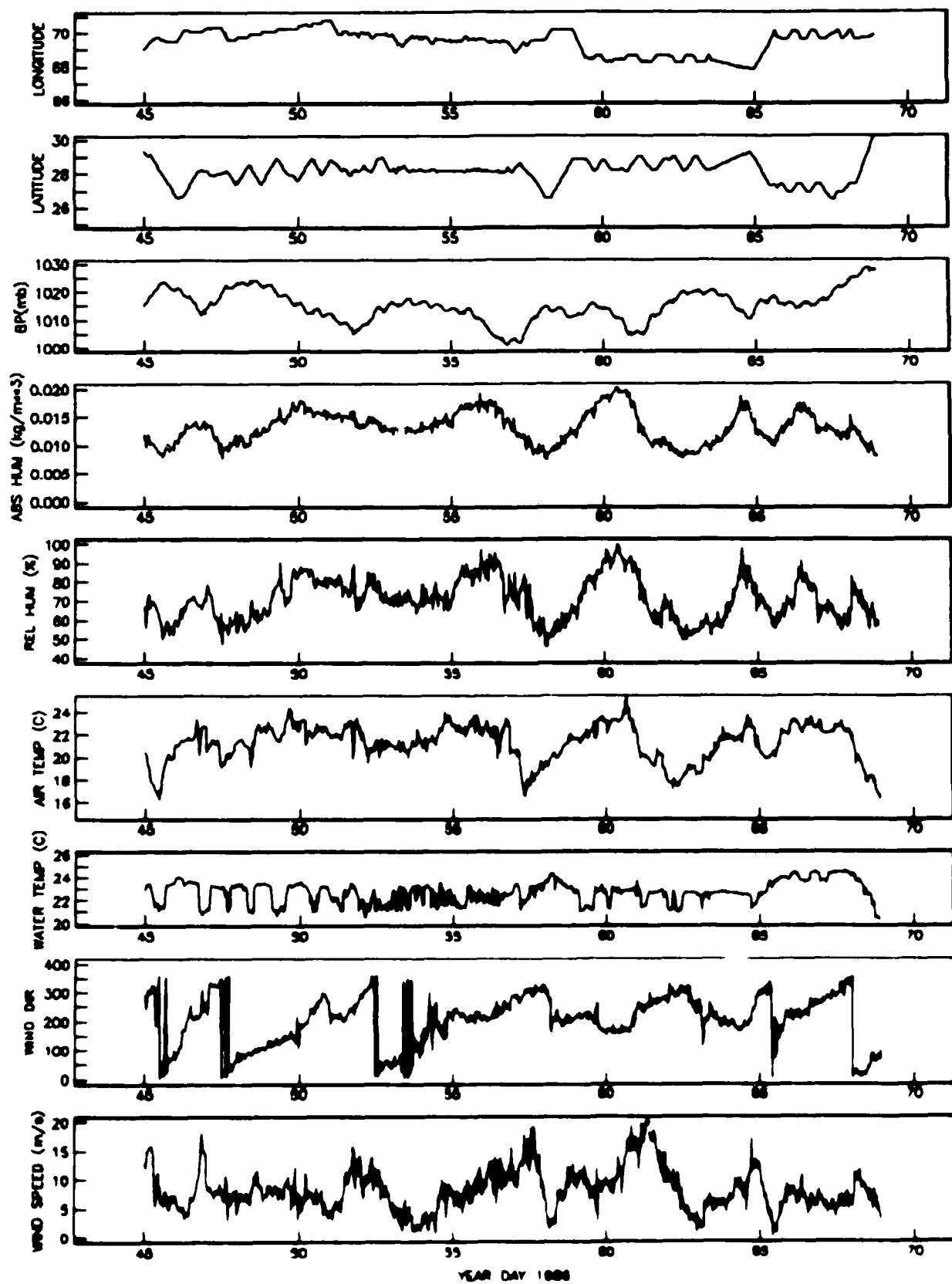


Figure Vb-3: Payne's Meteorological Plot for OCEANUS 125.

OCEANUS CRUISE 173 MANUAL MET OBSERVATIONS

NOTES ON PARAMETERS:

1. Date - Month/day
2. Time - UTC, hours
3. Lat and Long - Positions are from Internav Loran receiver.
4. WS,WD - True wind speed and direction derived from apparent wind speed and direction and ship course and speed. Direction is direction from which meteorological convention.
5. AT - Dry bulb air temperature, from Asman psychrometer, thermometer divisions are 0.2C.
6. RH - Relative humidity computed from wet and dry bulb temperatures from Asman by equations and constants in Smithsonian Meteorological Tables.
7. ABS HUM - Absolute humidity in kg/m³.
8. SST - Sea surface temperature (C) from bucket.
9. BP - Barometric pressure (mb) from bow MR for 2/14 0000Z to 2/21 1730Z. The remaining values are from the bridge corrected to agree with the bow MR.
10. CLOUD - Cloud observations. The four digits are: total octants covered, cloud type for low, medium and high clouds.
11. WAVES - The four two digit numbers are: sea wave period and height, predominant swell direction and height. Heights in feet, direc. 'on in 10s of degrees.
12. SC,SS - Ship's course and speed (kt) from gyro and ship's speed log.
13. AD,AS - Apparent wind direction and speed. AD is from bridge readout of ship's wind vane. AS is whichever was considered the best value at the time of observation: ship's anemometer, SAIL anemometer, Davidsen cups on mast or, if cups not operational, Davidsen hot wire anemometer on mast. AS in kts. If SC,SS,AD,AS are all 0 then WS and WD are linearly interpolated values.
14. TW - Wet bulb temperature (C). If this 0 then AT,RH,AM are linearly interpolated values.

oo

DATE	TIME	LAT	LONG	WS	WD	AT	RH	ABS HUM	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW		
2/14	0 29 18.04	69	0.33	12.6	292	20.4	67.4	0.1188-01	22.9	1015.4			240	8	40	30	16.2		
2/14	100 29 13.73	69	6.04	11.9	243	20.3	56.2	0.9768-02	23.4	1016.1			230	9	10	32	14.7		
2/14	200 29 9.43	69	12.81	14.9	313	19.4	70.5	0.1188-01	23.4	1016.3			240	8	60	32	15.7		
2/14	300 29 5.33	69	19.76	15.2	301	19.1	73.7	0.1188-01	23.5	1017.1			240	8	50	34	15.8		
2/14	400 29 3.14	69	23.98	15.6	298	18.0	66.4	0.1018-01	23.1	1018.8			330	2	330	32	14.0		
2/14	500 29 8.76	69	29.84	15.8	324	17.7	68.3	0.1038-01	23.6	1018.8			230	8	60	31	0.0		
2/14	600 28 39.36	69	35.88	15.2	323	17.5	70.2	0.1048-01	22.1	1019.2			230	7	60	30	14.0		
2/14	700 28 32.43	69	39.71	9.9	211	17.2	68.5	0.1008-01	21.4	1020.3			200	7	90	18	0.0		
2/14	800 28 45.04	69	42.09	5.3	182	16.9	66.8	0.9508-02	21.8	1020.5			200	8	350	18	0.0		
2/14	900 28 37.66	69	44.48	6.3	270	16.6	65.1	0.9138-02	21.8	1021.0			0	0	0	0	0.0		
2/14	1000 28 30.27	69	46.86	11.2	357	16.3	63.4	0.8728-02	21.1	1021.4			190	8	160	14	12.2		
2/14	1100 28 22.73	69	47.19	7.7	339	17.1	62.6	0.9028-02	21.1	1022.0	7	2 08	6	160	8	230	8	12.8	
2/14	1200 28 15.62	69	49.00	8.7	2	16.8	59.6	0.8438-02	21.4	1023.1		2 04	8	160	8	220	10	12.2	
2/14	1300 28 8.53	69	41.38	5.9	16	17.8	57.5	0.8438-02	21.6	1023.2	1	2 04	7	160	8	260	7	12.8	
2/14	1400 27 39.64	69	37.77	6.3	19	18.6	50.5	0.7948-02	21.3	1023.3	4	1	2 24	10	160	8	260	8	12.6
2/14	1500 27 34.42	69	35.39	5.5	11	19.2	52.2	0.8498-02	21.6	1023.7	1	3	2 34	10	160	7	230	6	13.3
2/14	1600 27 47.81	69	33.07	8.0	354	19.6	55.9	0.9318-02	23.4	1023.3	4	2 34	9	160	8	210	8	14.1	
2/14	1700 27 40.40	69	32.80	7.3	21	20.1	59.7	0.1028-01	23.3	1023.0	6	2 34	9	160	7	230	8	15.0	
2/14	1800 27 32.90	69	32.50	3.1	73	20.3	58.4	0.1018-01	23.4	1022.4	8		180	8	300	11	19.0		
2/14	1900 27 36.51	69	32.23	6.7	60	19.9	52.4	0.8988-02	23.4	1022.0	2		170	8	300	10	13.9		
2/14	2000 27 19.69	69	30.67	7.0	66	19.8	57.0	0.9068-02	23.3	1021.4	8		170	8	290	14	14.4		
2/14	2100 27 12.17	69	21.36	7.4	78	19.9	56.3	0.9358-02	23.3	1021.2	4		180	8	290	13	14.4		
2/14	2200 27 5.00	69	32.48	6.3	83	20.0	52.6	0.8988-02	23.3	1021.1	41	1 32	10	6	180	8	300	14	14.0
2/14	2300 26 36.37	69	32.64	6.0	98	20.7	57.4	0.1028-01	23.3	1021.2	4	1 32	10	5	180	8	310	13	13.2
2/15	0 26 31.11	69	32.07	7.4	66	21.2	60.4	0.1108-01	24.0	1020.8			170	8	290	13	16.0		
2/15	100 26 44.03	69	31.33	6.4	90	21.1	59.3	0.1088-01	24.0	1021.0			170	8	310	16	13.8		
2/15	200 26 37.09	69	30.86	3.1	89	21.0	57.0	0.1038-01	24.1	1021.6			270	8	180	2	13.4		
2/15	300 26 37.19	69	30.74	4.6	116	21.3	50.3	0.1118-01	24.0	1021.3			270	8	270	4	16.1		
2/15	400 26 37.70	69	47.04	5.3	109	21.3	68.2	0.1238-01	24.0	1021.9			270	8	240	6	17.0		
2/15	500 26 37.93	69	36.02	4.4	173	21.6	41.6	0.1158-01	23.7	1020.2			270	8	310	11	16.5		
2/15	600 26 34.22	70	4.20	3.3	169	21.4	66.9	0.1238-01	23.3	1021.9			270	8	300	12	17.0		
2/15	700 26 43.30	70	8.34	3.1	170	21.5	64.6	0.1208-01	23.5	1021.8			0	8	30	2	16.8		
2/15	800 26 49.12	70	7.78	4.4	200	21.3	74.2	0.1308-01	23.5	1021.8			0	8	270	3	18.0		
2/15	900 26 37.24	70	8.11	4.2	209	21.8	70.3	0.1338-01	23.6	1021.8			0	7	270	4	17.8		
2/15	1000 27 5.04	70	7.49	3.7	226	21.6	70.3	0.1318-01	23.7	1021.7			0	8	300	6	17.6		
2/15	1100 27 12.80	70	6.97	7.0	236	21.6	71.9	0.1348-01	23.5	1021.8	3	1 33	9	4	0	8	290	14	17.8
2/15	1200 27 20.99	70	6.68	6.2	226	21.3	71.8	0.1338-01	23.5	1021.7	9	1 33	9	4	0	8	270	9	17.7
2/15	1300 27 29.06	70	6.12	6.7	214	21.6	71.1	0.1338-01	23.6	1021.7	4	1 33	9	3	0	8	230	8	17.7
2/15	1400 27 37.23	70	6.06	6.3	203	21.7	72.8	0.1378-01	23.5	1021.6	8	1	3	0	8	240	6	18.0	
2/15	1500 27 43.27	70	5.00	7.1	209	22.0	70.7	0.1358-01	23.6	1021.6	2	2	3	0	8	240	8	18.0	
2/15	1600 27 53.14	70	3.09	8.1	222	22.4	69.0	0.1428-01	23.4	1021.6	2	2	3	0	8	230	11	19.0	
2/15	1700 28 0.91	70	3.83	9.9	200	22.4	68.0	0.1338-01	23.5	1021.4	2		180	8	240	14	18.0		
2/15	1800 28 8.76	70	2.80	10.4	218	20.2	67.8	0.1318-01	23.1	1021.3			330	8	230	16	0.0		
2/15	1900 28 13.29	70	6.32	14.5	218	22.0	67.6	0.1298-01	23.1	1021.2	2		240	2	340	30	17.6		
2/15	2000 28 12.33	70	6.61	18.0	309	22.8	65.4	0.1308-01	23.7	1021.9	1		330	0	340	35	18.0		
2/15	2100 28 13.74	70	4.33	14.9	232	22.8	65.3	0.1378-01	23.1	1021.2			20	6	230	24	0.0		
2/15	2200 28 12.16	70	9.69	14.9	249	22.8	71.3	0.1418-01	23.1	1021.8	2	2 23	6	0	250	6	33	18.8	
2/15	2300 28 10.62	70	12.85	13.9	239	22.6	69.6	0.1308-01	23.1	1021.4	2	2 20	5	0	270	2	350	29	18.6
2/15	0 28 10.69	70	13.00	9.8	200	20.4	74.1	0.1398-01	23.3	1021.3			270	3	0	22	17.0		
2/15	100 28 10.93	70	13.90	8.4	224	20.7	78.6	0.1398-01	23.3	1021.4	1		200	6	20	20	17.8		
2/15	200 28 10.44	70	17.90	8.1	311	21.0	74.6	0.1338-01	23.1	1021.6			270	4	50	18	17.6		
2/15	300 28 1.82	70	17.12	8.9	133	21.0	73.8	0.1338-01	23.4	1021.5			180	9	130	10	17.5		
2/15	400 27 54.46	70	16.94	7.7	329	21.3	72.6	0.1338-01	23.3	1021.6	7	2 30	6	330	1	0	16	17.8	
2/15	500 27 53.40	70	17.07	7.7	319	21.5	66.2	0.1338-01	23.3	1021.5	7		330	1	0	16	17.0		
2/15	600 27 36.69	70	17.36	6.7	279	21.2	62.0	0.1138-01	23.3	1021.5			330	2	0	19	16.2		
2/15	700 27 37.37	70	17.30	8.2	319	21.2	60.4	0.1108-01	23.1	1021.3			330	1	330	17	16.0		
2/15	800 27 36.24	70	17.69	7.7	329	21.0	57.9	0.1048-01	23.1	1021.7			330	1	0	16	15.5		

Table Vb-3 (Cont)

DATE	TIME	LAT	LONG	WS	WD	AT	RH	ABS HUM	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW	
2/16	1000	27 59.91	70 17.47	9.3	331	19.4	53.4	0.879E-02	23.0	1017.7			330	1	20	19	13.6	
2/16	1030	28 0.42	70 17.66	7.7	341	19.6	52.9	0.880E-02	23.0	1017.8	1	1 30	4	330	2	10	17	13.7
2/16	1100	28 0.85	70 17.90	8.5	14	19.3	62.8	0.103E-01	23.1	1018.3	1	1 30	3	330	2	40	18	14.7
2/16	1130	28 1.27	70 18.15	8.3	331	19.1	64.3	0.104E-01	23.1	1018.6	1	1 30	3	340	2	10	18	14.7
2/16	1200	28 1.57	70 18.47	7.7	1	19.3	54.8	0.897E-02	23.2	1019.2	1	1 32	5	350	2	10	17	13.7
2/16	1230	28 2.37	70 18.19	7.8	12	19.3	47.3	0.793E-02	23.2	1020.0	1	1 32	3	350	2	20	17	12.9
2/16	1300	28 4.04	70 13.47	6.7	12	19.5	59.0	0.977E-02	23.2	1019.8	1	1 34	5	70	12	330	22	14.4
2/16	1330	28 5.77	70 6.79	6.4	19	19.3	57.7	0.954E-02	22.4	1020.5			0	0	0	0	0.0	
2/16	1400	28 4.11	70 4.62	6.1	25	19.4	56.4	0.930E-02	22.8	1021.1	1	1 32	5	150	5	260	10	14.0
2/16	1430	28 3.79	70 4.87	8.4	14	19.9	55.9	0.945E-02	22.9	1021.5			0	0	0	0	0.0	
2/16	1500	28 5.31	69 36.53	10.7	357	20.3	55.3	0.959E-02	22.5	1021.8	1	3 00	5	65	8	310	25	14.6
2/16	1530	28 7.19	69 37.55	9.6	9	20.1	56.6	0.970E-02	21.0	1022.2			0	0	0	0	0.0	
2/16	1600	28 9.02	69 47.18	8.5	16	19.9	57.9	0.981E-02	21.0	1022.5	1	3 00	4	60	8	330	23	14.6
2/16	1630	28 10.83	69 43.02	3.0	359	20.3	54.0	0.948E-02	21.1	1022.1			60	8	335	12	14.6	
2/16	1700	28 12.71	69 38.99	7.0	53	20.0	52.6	0.896E-02	21.4	1021.9	1	3	4	180	8	270	11	14.0
2/16	1730	28 12.20	69 35.38	7.0	56	20.0	52.6	0.896E-02	21.3	1021.7			0	0	0	0	14.0	
2/16	1800	28 8.27	69 34.91	6.9	58	20.2	53.2	0.951E-02	21.4	1021.3	1	2	190	9	270	10	14.5	
2/16	1830	28 4.51	69 34.71	7.7	34	20.0	62.0	0.106E-01	23.0	1021.6			195	8	220	8	15.2	
2/16	1900	28 0.81	69 35.09	5.7	26	20.2	57.5	0.992E-02	23.4	1021.4	1	1	4	190	8	230	4	14.8
2/16	1930	27 35.76	69 35.38	6.0	29	20.3	57.7	0.100E-01	23.3	1021.3			0	0	0	0	0.0	
2/16	2000	27 53.35	69 35.56	6.3	32	20.4	57.8	0.101E-01	23.3	1021.6	1	1	4	180	8	250	7	15.0
2/16	2030	27 49.45	69 35.85	7.2	41	20.5	58.7	0.103E-01	23.2	1021.7			0	0	0	0	0.0	
2/16	2100	27 44.72	69 36.10	8.0	49	20.6	59.6	0.105E-01	23.1	1021.8	1	1	4	180	8	260	12	15.4
2/16	2130	27 42.00	69 36.06	7.6	57	21.0	59.7	0.108E-01	23.3	1021.7			0	0	0	0	0.0	
2/16	2200	27 38.10	69 35.84	7.2	65	21.3	59.7	0.110E-01	23.4	1022.3	2	2 09	3	180	8	280	13	16.0
2/16	2230	27 34.24	69 35.68	7.7	63	21.3	62.4	0.115E-01	23.4	1022.3			0	0	0	0	0.0	
2/16	2300	27 30.42	69 35.37	8.3	60	21.3	65.1	0.119E-01	23.3	1022.3	2	2 09	3	180	8	270	14	16.7
2/16	2330	27 26.72	69 35.88	6.1	78	21.3	59.4	0.109E-01	23.3	1022.6			0	0	0	0	0.0	
2/17	0	27 24.07	69 37.86	3.8	95	21.3	53.6	0.984E-02	23.5	1022.9	1		270	8	310	1	15.2	
2/17	30	27 24.50	69 42.25	4.6	95	21.3	54.2	0.100E-01	23.4	1023.1			0	0	0	0	0.0	
2/17	100	27 35.31	69 46.63	5.4	95	21.6	54.8	0.102E-01	23.5	1023.3	1		0	7	60	12	15.6	
2/17	130	27 29.36	69 46.56	6.1	79	21.6	58.5	0.109E-01	23.3	1023.2			0	0	0	0	0.0	
2/17	200	27 33.46	69 46.10	6.7	63	21.5	62.2	0.115E-01	23.4	1023.0	1		0	8	40	18	16.5	
2/17	230	27 37.37	69 45.54	7.3	68	21.6	62.7	0.117E-01	23.5	1023.1			0	0	0	0	0.0	
2/17	300	27 41.28	69 45.24	7.8	73	21.7	63.2	0.119E-01	23.4	1023.3	1		0	8	50	19	16.8	
2/17	330	27 45.29	69 44.80	7.3	83	21.5	62.7	0.117E-01	23.2	1023.4			0	0	0	0	0.0	
2/17	400	27 49.04	69 44.91	6.7	92	21.4	62.1	0.115E-01	22.9	1023.5			0	8	60	15	16.4	
2/17	430	27 52.67	69 44.72	6.5	88	21.2	58.8	0.112E-01	23.0	1023.4			0	0	0	0	0.0	
2/17	500	27 56.54	69 45.12	6.3	84	21.0	55.5	0.100E-01	23.1	1023.3			350	8	60	14	15.2	
2/17	530	28 0.29	69 45.21	6.7	82	21.0	54.8	0.987E-02	23.1	1023.3			0	0	0	0	0.0	
2/17	600	28 4.22	69 45.27	7.1	79	21.0	54.0	0.974E-02	23.2	1023.2			350	8	60	16	15.0	
2/17	630	28 7.79	69 44.93	6.4	69	21.0	55.5	0.100E-01	23.0	1023.0			350	8	50	16	15.2	
2/17	700	28 11.45	69 44.44	7.9	89	21.0	55.5	0.100E-01	22.9	1022.8			350	8	70	16	15.2	
2/17	730	28 14.91	69 44.32	7.7	91	21.0	57.8	0.104E-01	22.0	1022.9			340	8	80	14	15.5	
2/17	800	28 18.56	69 45.35	6.1	89	20.8	56.7	0.101E-01	21.1	1022.8			340	8	70	12	15.2	
2/17	830	28 22.15	69 46.17	6.3	94	20.8	58.3	0.104E-01	21.1	1022.3			0	8	60	14	15.4	
2/17	900	28 25.97	69 46.12	6.7	92	20.8	56.7	0.101E-01	21.1	1022.7			0	8	60	15	15.2	
2/17	930	28 29.49	69 45.82	5.8	97	20.5	57.1	0.100E-01	21.0	1022.8			0	8	60	13	15.0	
2/17	1000	28 30.28	69 49.82	5.7	39	19.1	64.2	0.104E-01	21.0	1023.2			270	8	180	3	14.7	
2/17	1030	28 30.41	69 54.50	7.3	86	19.6	67.6	0.113E-01	21.2	1024.1			0	0	0	0	0.0	
2/17	1100	28 27.08	69 55.84	8.8	83	20.0	71.0	0.121E-01	21.0	1023.2	4		180	8	290	18	16.3	
2/17	1130	28 23.16	69 55.97	7.6	91	20.2	69.6	0.120E-01	20.9	1023.6	6	1 09	3	180	8	300	17	16.3
2/17	1200	28 29.38	69 56.29	8.0	93	21.4	64.4	0.119E-01	20.8	1023.6	6	1 09	3	180	8	300	18	16.7
2/17	1230	28 15.37	69 55.69	9.0	96	21.1	64.9	0.118E-01	21.0	1023.9	8	1 09	3	180	8	300	20	16.5
2/17	1300	28 21.55	69 54.86	10.4	99	21.1	63.7	0.119E-01	23.1	1023.5	8	1 09	3	180	8	300	23	16.6
2/17	1330	28 7.94	69 55.06	9.7	106	22.0	60.3	0.116E-01	23.2	1023.8	1	1 09	3	200	8	290	20	16.7
2/17	1400	28 4.31	69 55.83	10.4	99	22.2	64.6	0.125E-01	23.3	1023.9	1	3 01	3	180	8	300	23	17.4
2/17	1430	28 0.77	69 55.78	11.1	89	22.7	61.3	0.122E-01	23.3	1024.2	1	3 01	5	180	8	290	23	17.4
2/17	1500	27 56.96	69 55.81	11.3	95	22.7	63.6	0.127E-01	23.5	1024.1			0	0	0	0	0.0	
2/17	1530	27 53.25	69 55.72	11.4	101	22.7	63.9	0.131E-01	23.5	1024.0	1	4 01	3	180	8	300	25	18.0
2/17	1600	27 49.63	69 55.64	8.8	108	23.0	58.0	0.117E-01	23.4	1024.2	1	4 01	3	180	8	310	21	17.2
2/17	1630	27 45.00	69 55.80	9.0	96	22.5	59.8	0.117E-01	23.3	1023.6	1	4 10	3	180	8	300	20	17.0
2/17	1700	27 41.65	69 55.85	9.2	100	22.6	60.5	0.119E-01	23.3	1023.5	1	4 10	5	170	8	310	22	17.2
2/17	1730	27 37.66	69 55.60	8.3	107	22.4	61.8	0.121E-01	23.4	1023.1	1	3 10	4	180	8	310	20	17.2
2/17	1800	27 35.17	69 55.83	8.3	107	22.2	61.5	0.119E-01	23.4	1022.6	1	3 10	4	180	8	310	20	17.0
2/17	1830	27 31.35	69 55.62	8.3	107	22.4	62.3	0.122E-01	23.4	1022.4	1	3 10	4					

Table Vb-3 (Cont)

DATE	TIME	LAT	LONG	WS	WD	AT	RH	ABS HUM	SST	RF	CLOUD	WAVES	SC	SS	AD	AS	TW	
2/18	500	28 35.28	70 5.90	8.9	127	21.8	76.1	0.144E-01	21.2	1021.0			0	8	100	14	18.5	
2/18	530	28 39.15	70 5.80	9.0	143	21.6	76.4	0.146E-01	21.2	1020.9			0	8	120	12	18.6	
2/18	600	28 44.72	70 6.00	8.5	127	21.5	76.3	0.145E-01	21.1	1020.5			350	8	110	12	18.5	
2/18	630	28 40.74	70 5.81	8.0	120	21.5	77.5	0.144E-01	20.6	1020.0			350	8	100	12	18.4	
2/18	700	28 51.94	70 5.92	8.1	128	21.5	78.3	0.145E-01	21.0	1020.0			350	8	110	11	18.5	
2/18	730	28 34.61	70 6.26	8.5	134	21.4	78.3	0.144E-01	21.1	1019.9			350	8	120	11	18.4	
2/18	800	28 35.02	70 10.04	6.3	122	21.4	80.0	0.148E-01	20.9	1019.2			270	8	250	7	18.6	
2/18	830	28 53.73	70 15.59	8.0	135	21.5	80.9	0.150E-01	21.0	1018.8 1			180	8	330	22	18.6	
2/18	900	28 51.79	70 15.36	8.6	122	21.5	82.6	0.153E-01	21.4	1018.5			180	8	320	22	19.0	
2/18	930	28 47.98	70 15.67	7.0	132	21.4	90.4	0.167E-01	21.6	1018.5			180	8	330	20	19.6	
2/18	1000	28 44.07	70 15.54	8.0	135	22.1	79.7	0.153E-01	21.6	1018.5			180	8	330	22	19.2	
2/18	1030	28 39.92	70 15.67	7.5	134	21.9	76.2	0.145E-01	21.4	1018.4			180	8	330	21	18.6	
2/18	1100	28 35.68	70 15.84	7.1	148	22.2	74.9	0.144E-01	21.1	1018.5 1 9	2		0	180	8	340	21	18.7
2/18	1130	28 31.93	70 15.79	6.5	131	22.1	75.6	0.145E-01	21.0	1018.6 6	6		0	180	8	330	19	18.7
2/18	1200	28 28.12	70 16.20	7.1	148	22.2	75.7	0.146E-01	21.0	1018.5 6	3		0	180	8	340	21	18.8
2/18	1230	28 24.19	70 16.07	6.6	147	22.5	72.0	0.140E-01	21.1	1018.6 6	3		0	180	8	340	20	18.5
2/18	1300	28 21.62	70 15.99	8.9	155	22.7	71.4	0.142E-01	21.1	1019.1 6	3		0	180	4	340	21	18.7
2/18	1330	28 18.21	70 16.03	9.5	137	23.2	67.2	0.137E-01	22.1	1018.9 5	7	3	0	180	8	330	25	18.6
2/18	1400	28 15.16	70 16.14	9.6	148	23.3	71.2	0.146E-01	22.6	1019.0 178	3	0	180	5	335	23	19.2	
2/18	1430	28 11.63	70 15.62	9.1	151	23.4	71.3	0.147E-01	22.8	1019.0 178	3	0	180	8	340	25	19.3	
2/18	1500	28 7.77	70 15.42	9.8	144	23.6	69.2	0.144E-01	23.2	1019.0 17	4	0	180	8	335	26	19.2	
2/18	1530	28 4.07	70 15.38	10.4	140	24.2	72.0	0.155E-01	23.4	1018.7 2	8	4	0	180	7	330	26	20.1
2/18	1600	28 0.04	70 15.95	8.5	141	24.4	69.2	0.151E-01	23.4	1018.6 2	8	4	0	185	8	330	23	19.9
2/18	1630	27 59.24	70 16.13	8.6	150	24.3	70.7	0.153E-01	23.4	1018.1			0	0	0	0	0	0
2/18	1700	27 58.77	70 15.95	8.7	160	24.2	72.1	0.155E-01	23.4	1017.7	2	4	0	0	0	0	0	0
2/18	1730	27 58.65	70 15.95	8.8	169	24.0	72.1	0.155E-01	23.2	1017.5	7	4	3	170	1	0	18	20.0
2/18	1800	27 58.42	70 16.02	4.7	147	23.4	73.6	0.152E-01	23.1	1017.6	3	1	3	170	1	340	10	19.6
2/18	1830	27 58.33	70 15.88	5.2	159	23.2	79.8	0.163E-01	23.2	1017.1	3	1 18	3	170	1	350	11	20.2
2/18	1900	27 58.41	70 15.60	6.7	139	22.5	85.0	0.167E-01	23.3	1016.5	3		150	1	350	14	20.2	
2/18	1930	27 58.49	70 15.31	5.7	139	23.4	84.9	0.175E-01	23.3	1016.3	3		150	1	350	12	21.0	
2/18	2000	27 58.55	70 14.97	5.7	149	23.0	87.9	0.177E-01	23.3	1016.3	3		150	1	0	12	21.0	
2/18	2030	27 58.12	70 14.28	9.0	137	22.8	85.3	0.170E-01	23.4	1015.8			0	0	0	0	0	0
2/18	2100	27 56.23	70 13.71	12.2	124	22.6	82.6	0.163E-01	23.5	1015.4	8		190	8	310	26	20.0	
2/18	2130	27 52.88	70 14.71	7.6	129	22.6	86.0	0.170E-01	23.5	1015.8	7	2 16	4	190	8	320	20	20.4
2/18	2200	27 49.46	70 13.68	6.6	147	23.3	81.0	0.167E-01	23.5	1015.3	7	3 16	4	180	8	340	20	20.5
2/18	2230	27 45.85	70 15.83	7.8	217	22.4	81.6	0.159E-01	23.5	1016.1	7	3 16	4	180	8	25	22	19.7
2/18	2300	27 42.26	70 15.92	7.0	132	22.5	82.5	0.162E-01	23.4	1015.5	7	3 16	4	180	8	330	20	19.9
2/18	2330	27 38.60	70 15.72	2.9	103	22.3	83.2	0.162E-01	23.4	1016.0	7		180	8	330	11	19.8	
2/19	0	27 35.30	70 15.69	6.1	180	22.6	86.0	0.170E-01	23.6	1015.8			230	8	330	18	20.4	
2/19	30	27 35.02	70 19.59	7.7	192	22.5	85.1	0.167E-01	23.5	1015.8			270	9	310	19	20.2	
2/19	100	27 35.78	70 23.85	6.9	192	23.1	87.2	0.177E-01	23.6	1016.1	2		270	8	310	17	21.0	
2/19	130	27 38.43	70 26.45	5.2	189	23.2	80.1	0.180E-01	23.6	1016.2	2		0	9	240	2	21.2	
2/19	200	27 42.88	70 26.20	4.5	184	23.3	86.5	0.177E-01	23.6	1016.2	2		0	8	220	1	21.1	
2/19	230	27 47.47	70 25.91	5.7	184	23.4	84.9	0.175E-01	23.4	1016.0	2		350	8	230	4	21.0	
2/19	300	27 51.72	70 26.30	4.7	180	23.3	86.5	0.177E-01	23.2	1015.5	2		350	8	240	2	21.1	
2/19	330	27 55.82	70 26.28	7.1	188	23.3	86.5	0.177E-01	23.2	1015.3	2		0	8	200	6	21.1	
2/19	400	27 39.77	70 26.29	6.5	191	23.2	87.2	0.178E-01	23.2	1015.0	7		0	8	210	5	21.1	
2/19	430	28 3.70	70 26.78	6.1	186	23.2	86.4	0.176E-01	23.3	1014.5	7		0	8	200	4	21.0	
2/19	500	28 3.56	70 27.26	11.3	196	21.0	86.6	0.156E-01	23.3	1013.9	7		10	8	190	14	19.0	
2/19	530	28 9.16	70 27.74	10.2	195	21.3	86.6	0.159E-01	23.1	1013.7			0	0	0	0	0	0
2/19	600	28 14.14	70 28.22	9.1	194	21.5	87.0	0.161E-01	23.0	1013.6			0	0	0	0	0	0
2/19	630	28 20.36	70 28.70	8.0	193	21.8	87.0	0.164E-01	22.9	1013.4	53		340	8	240	10	19.8	
2/19	700	28 23.39	70 28.49	6.7	194	22.0	87.3	0.167E-01	22.9	1012.7	3		340	8	250	8	20.0	
2/19	730	28 27.01	70 28.41	7.4	207	22.2	84.9	0.164E-01	22.9	1012.4			0	0	0	0	0	0
2/19	800	28 30.62	70 28.32	8.0	219	22.4	82.5	0.161E-01	22.4	1012.2			350	8	260	12	19.8	
2/19	830	28 33.57	70 25.86	7.4	248	22.3	84.0	0.162E-01	21.8	1012.3	2		350	8	290	15	19.8	
2/19	900	28 37.28	70 26.26	7.7	238	22.0	87.3	0.167E-01	21.8	1012.3			350	8	280	14	20.0	
2/19	930	28 41.16	70 26.16	7.9	228	22.0	87.3	0.167E-01	22.4	1012.2			350	8	270	13	20.0	
2/19	1000	28 44.92	70 25.88	7.4	248	21.7	85.4	0.160E-01	20.9	1012.3	5		350	8	290	15	19.5	
2/19	1030	28 48.73	70 25.73	6.6	243	21.7	86.2	0.162E-01	21.2	1012.6			350	8	290	13	19.6	
2/19	1100	28 52.46	70 25.77	7.3	234	22.1	82.3	0.158E-01	21.0	1012.8	5		310	8	310	18	19.3	
2/19	1130	28 52.76	70 29.54	5.6	225	22.0	78.9	0.150E-01	21.1	1012.4	6		260	8	340	18	19.0	
2/19	1200	28 52.28	70 33.86	6.2	229	22.0	76.9	0.150E-01	21.0	1012.4	6		230	8	0	20	19.0	
2/19	1230	28 46.85	70 34.56	6.2	235	22.4	77.3	0.151E-01	21.1	1012.9	6	2	190	8	40	17	19.2	
2/19	1300	28 45.04	70 34.77	7.3	255	22.7	77.0	0.153E-01	21.9	1013.5	4	2	180	8	50	18	19.4	
2/19	1330	28 45.48	70 31.77	7.3	253	22.7	79.4	0.158E-01										

Table Vb-3 (Cont)

DATE	TIME	LAT	LONG	WE	WD	AT	RH	AWS	MNH	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW	
2/21	1900	28 38.97	69 36.20	7.8	31	20.7	70.2	0.124B-01	21.7	1013.4	1	5		20	1	30	16	16.8	
2/21	1930	28 39.87	69 36.86	6.8	62	21.0	71.3	0.129B-01	21.7	1012.9	1	4		20	1	40	14	17.2	
2/21	2000	28 35.51	69 36.15	9.1	64	21.3	72.6	0.135B-01	21.3	1012.9	1	4		170	11	290	18	17.8	
2/21	2030	28 30.63	69 35.23	8.2	39	20.8	73.2	0.134B-01	21.2	1013.4	1	3		170	11	290	16	17.5	
2/21	2100	28 43.48	69 34.03	7.9	57	21.0	69.7	0.126B-01	21.1	1013.4	1	3		170	11	290	15	17.0	
2/21	2130	28 40.51	69 32.84	7.3	67	21.2	69.9	0.127B-01	21.8	1013.8	1	3 30	6	6	170	11	300	16	17.2
2/21	2200	28 35.58	69 37.51	7.6	42	21.4	69.3	0.126B-01	21.9	1014.5	1	2 02	4	4	170	11	280	12	17.3
2/21	2230	28 30.11	69 30.62	6.6	61	21.2	70.7	0.129B-01	21.8	1014.4	2	2 02	10	4	170	11	300	14	17.3
2/21	2300	28 24.90	69 49.88	9.4	45	21.0	71.3	0.129B-01	21.3	1015.0	2	1 02	10	4	170	11	300	10	17.2
2/21	2330	28 19.32	69 48.93	5.4	45	21.2	68.2	0.124B-01	21.4	1015.3	1				170	11	300	10	17.0
2/22	0	28 15.11	69 48.17	4.4	34	21.1	68.9	0.125B-01	21.2	1015.7	1			170	6	270	6	17.0	
2/22	30	28 12.23	69 48.13	5.4	49	21.1	71.4	0.129B-01	22.5	1013.9				200	6	240	6	17.3	
2/22	100	28 9.39	69 48.33	6.1	47	21.0	71.3	0.129B-01	22.9	1016.2	1			200	6	230	7	17.2	
2/22	130	28 8.92	69 30.14	3.7	86	21.0	72.1	0.130B-01	23.0	1016.3	1			320	6	60	8	17.3	
2/22	200	28 11.01	69 31.44	3.9	49	21.1	73.0	0.132B-01	22.8	1016.5				270	6	110	8	17.3	
2/22	230	28 11.09	69 33.96	3.1	80	20.9	70.3	0.126B-01	22.7	1016.4				300	6	70	4	17.0	
2/22	300	28 13.15	69 34.38	5.1	49	20.8	67.0	0.117B-01	22.7	1016.0				50	8	0	18	16.5	
2/22	330	28 16.03	69 50.19	4.1	49	20.7	71.8	0.127B-01	21.2	1016.4				50	11	0	19	17.0	
2/22	400	28 19.38	69 45.68	5.3	36	20.8	73.5	0.131B-01	21.1	1015.9				140	11	320	16	17.3	
2/22	430	28 15.93	69 41.42	4.6	38	20.8	71.9	0.128B-01	21.1	1015.7				130	11	320	14	17.1	
2/22	500	28 11.44	69 37.57	4.0	44	21.0	73.7	0.133B-01	22.3	1015.3	1			130	10	320	12	17.3	
2/22	530	28 8.96	69 33.55	3.1	63	21.0	69.8	0.126B-01	23.0	1015.2	1			130	10	330	12	17.0	
2/22	600	28 0.18	69 26.50	2.6	59	21.5	67.0	0.124B-01	23.2	1015.2	1			60	10	0	15	17.1	
2/22	630	28 12.78	69 23.79	2.8	78	20.6	73.0	0.132B-01	23.2	1015.2	1			50	10	10	15	17.3	
2/22	700	28 16.34	69 18.95	2.3	82	20.5	75.8	0.133B-01	23.1	1014.8	1			50	10	10	14	17.3	
2/22	730	28 20.70	69 18.03	5.1	83	20.8	71.9	0.128B-01	22.9	1015.5	1			310	11	60	8	17.1	
2/22	800	28 24.86	69 21.80	2.3	38	20.6	72.5	0.128B-01	21.1	1015.3	1			180	11	340	8	17.0	
2/22	830	28 30.03	69 21.54	1.8	23	21.0	68.0	0.123B-01	22.3	1015.5	1			180	11	350	8	16.8	
2/22	900	28 15.29	69 20.92	1.1	96	21.2	69.0	0.126B-01	23.0	1015.2	1			220	11	350	10	17.1	
2/22	930	28 15.93	69 19.82	2.3	341	21.4	67.4	0.125B-01	23.1	1015.2	1			40	8	340	11	17.1	
2/22	1000	28 20.23	69 15.51	4.3	17	20.8	71.9	0.128B-01	23.0	1015.5	1			40	10	350	18	17.1	
2/22	1030	28 24.32	69 11.03	5.7	3	30.8	71.9	0.128B-01	23.0	1015.3	1	2	3	40	9	340	19	17.1	
2/22	1100	28 27.52	69 9.33	6.6	161	20.4	74.8	0.130B-01	22.6	1016.0	1	2 04	5	270	11	300	14	17.1	
2/22	1130	28 37.04	69 14.09	3.0	10	20.4	73.2	0.128B-01	21.7	1016.2	1	2 04	9	5	270	8	40	9	16.9
2/22	1200	28 28.26	69 18.93	2.1	14	20.5	71.6	0.126B-01	21.3	1016.6	1	2 04	9	6	270	8	30	8	16.8
2/22	1230	28 26.93	69 21.59	1.9	352	20.5	69.1	0.121B-01	21.2	1017.0	1	2 04	9	5	200	8	20	5	16.5
2/22	1300	28 22.74	69 24.03	3.4	12	20.7	71.8	0.127B-01	21.2	1017.1		1 04	9	5	220	11	30	6	17.0
2/22	1330	28 20.77	69 29.18	2.8	9	20.0	77.0	0.121B-01	21.3	1017.3		1 04	9	5	230	11	30	10	17.0
2/22	1400	28 18.79	69 33.92	3.7	335	20.5	73.6	0.133B-01	21.3	1017.4		1 04	9	5	150	11	350	4	17.3
2/22	1430	28 14.09	69 30.59	5.4	23	20.7	74.3	0.132B-01	21.3	1017.7		1 04	9	5	150	11	300	10	17.3
2/22	1500	28 11.12	69 30.80	3.7	15	20.7	73.4	0.130B-01	22.8	1017.8		1 04	9	5	250	11	40	9	17.2
2/22	1530	28 9.70	69 35.53	3.7	31	20.8	71.9	0.128B-01	22.9	1017.7		1 04	9	5	250	11	40	7	17.1
2/22	1600	28 8.50	69 39.43	3.2	347	21.0	70.4	0.127B-01	23.0	1017.6		1 04	9	4	250	6	50	8	17.1
2/22	1630	28 8.03	69 41.91	3.7	46	21.5	70.1	0.130B-01	23.1	1017.4		1 04	9	4	270	6	80	5	17.3
2/22	1700	28 8.26	69 43.96	1.0	119	21.2	68.2	0.124B-01	23.2	1016.7		1 04	9	4	300	6	0	4	17.0
2/22	1730	28 10.18	69 46.03	1.0	119	21.0	69.6	0.126B-01	23.2	1016.2		1 04	9	3	300	6	0	4	17.0
2/22	1800	28 10.36	69 48.10	1.4	143	21.2	69.8	0.127B-01	23.3	1015.7		1 04	9	3	0	11	10	9	17.2
2/22	1830	28 13.85	69 47.72	1.0	94	21.0	69.6	0.126B-01	22.1	1015.7		1 04	9	3	0	11	10	11	17.0
2/22	1900	28 13.96	69 47.63	1.9	131	21.1	68.9	0.125B-01	21.9	1015.7		1 04	9	3	90	11	10	14	17.0
2/22	1930	28 13.63	69 42.13	1.0	99	21.1	67.3	0.122B-01	22.1	1015.7		1 04	9	3	100	3	0	3	16.8
2/22	2000	28 11.76	69 41.70	1.9	120	21.3	68.2	0.123B-01	23.4	1015.7	2	04	8	3	210	1	290	3	17.0
2/22	2030	28 11.71	69 46.63	2.3	23	22.3	63.4	0.124B-01	23.4	1015.7	2	04	8	3	270	11	340	8	17.3
2/22	2100	28 11.87	69 45.37	2.1	113	22.3	63.0	0.125B-01	23.1	1015.7	2	04	8	3	100	0	0	0	0.0
2/22	2130	28 11.84	69 44.52	1.9	99	22.0	66.3	0.127B-01	23.3	1015.7	1	04	8	3	340	0	0	0	0.0
2/22	2200	28 11.82	69 43.86	1.7	84	21.8	68.1	0.128B-01	23.2	1015.7	1	04	8	2	0	0	0	3	17.3
2/22	2230	28 11.67	69 44.31	1.5	69	21.4	68.4	0.126B-01	23.0	1015.9	1	04	8	2	250	3	0	0	17.2
2/22	2300	28 11.06	69 44.78	2.1	99	21.3	69.9	0.128B-01	23.0	1016.0	1	04	8	2	140	0	320	4	17.3
2/23	0	28 13.85	69 37.30	2.1	89	20.9	74.5	0.124B-01	21.7	1015.9	1			320	11	20	9	17.3	
2/23	30	28 16.48	69 42.00	4.0	104	20.8	78.6	0.140B-01	21.3	1016.2	1			270	11	330	4	17.9	
2/23	100	28 15.04	69 47.57	2.1	179	20.8	76.6	0.140B-01	21.5	1016.2	1			180	11	0	15	17.9	
2/23	130	28 12.54	69 46.20	2.2	144	21.3	67.3	0.124B-01	22.9	1016.6	1			120	6	10	10	17.0	
2/23	200	28 10.87	69 40.33	2.6	119	21.3	73.2	0.134B-01	23.1	1016.6	1			120	6	0	11	17.7	
2/23	230	28 8.89	69 36.70	3.9	148	21.3	70.7	0.130B-01	23.1	1016.7	1			280	7	290	6	17.4	
2/23	300	28 8.34	69 39.35	4.3	134	21.8	68.1	0.128B-0											

Table Vb-3 (Cont)

	DATE	TIME	LAT	LONG	WS	WD	AT	RH	AMS	NHM	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW		
2/23	1400	28	5.33	69 35.83	5.9	162	22.5	73.3	0.144E-01	23.4	1013.8	3	04	8	1	140	14	10	23	18.8	
2/23	1430	28	3.62	69 34.64	7.0	157	22.5	73.1	0.143E-01	23.6	1013.7					0	0	0	0	0	
2/23	1500	28	3.74	69 34.19	8.0	152	22.4	72.6	0.142E-01	23.4	1013.6					0	0	0	0	0	
2/23	1530	28	9.92	69 33.07	9.1	147	22.4	72.2	0.140E-01	23.0	1013.4					0	0	0	0	0	
2/23	1600	28	10.31	69 33.58	10.1	142	22.3	71.7	0.139E-01	21.8	1013.3	3				210	3	300	21	18.4	
2/23	1630	28	9.65	69 34.09	7.3	188	22.9	70.8	0.142E-01	22.9	1014.9	2				270	3	290	15	18.8	
2/23	1700	28	10.16	69 34.57	6.9	134	23.0	70.9	0.143E-01	21.6	1013.2					0	4	120	11	18.9	
2/23	1730	28	10.99	69 34.00	6.2	159	23.0	71.7	0.145E-01	21.6	1014.6	2	06	4	230	0	320	12	19.0		
2/23	1800	28	11.16	69 33.90	9.3	209	24.0	65.1	0.139E-01	21.5	1014.3	2	06	3	280	0	290	18	19.0		
2/23	1830	28	10.95	69 33.97	8.0	206	23.5	72.1	0.150E-01	21.5	1013.8	2	06	3	270	1	300	16	19.5		
2/23	1900	28	10.83	69 33.62	3.1	159	23.2	74.2	0.151E-01	21.5	1013.8	2	06	3	140	10	0	16	19.5		
2/23	1930	28	10.36	69 32.97	6.6	211	23.1	74.9	0.152E-01	21.6	1013.4	2				140	3	60	14	19.5	
2/23	2000	28	9.50	69 31.28	8.4	220	23.6	75.4	0.157E-01	22.6	1013.1	2				140	3	70	17	20.0	
2/23	2030	28	9.51	69 29.80	8.8	239	23.5	76.1	0.156E-01	22.9	1013.4	2				120	0	120	17	20.0	
2/23	2100	28	10.16	69 29.61	8.3	226	23.7	67.0	0.141E-01	22.1	1013.0	2				240	6	350	22	19.0	
2/23	2130	28	9.19	69 30.17	9.3	229	23.7	64.8	0.136E-01	22.8	1013.4	2				130	0	100	18	18.7	
2/23	2200	28	8.93	69 29.93	7.8	228	23.5	69.9	0.145E-01	23.0	1013.4	2	20	8	3	240	3	350	18	19.2	
2/23	2230	28	8.93	69 30.34	8.9	230	23.3	65.9	0.135E-01	23.0	1013.4	4	20	8	3	300	3	290	18	18.3	
2/23	2300	28	10.05	69 30.96	7.1	229	22.9	69.9	0.134E-01	21.7	1013.8	4	20			300	3	300	15	18.3	
2/23	2330	28	10.10	69 31.51	8.4	234	22.8	68.4	0.136E-01	21.5	1013.8	1				250	3	340	21	18.4	
2/24	0	28	9.95	69 33.14	7.9	196	22.8	70.7	0.141E-01	21.7	1013.9	1				30	7	80	15	18.7	
2/24	30	28	9.39	69 31.23	7.8	242	22.8	71.3	0.143E-01	21.8	1014.1	1				2	140	6	80	15	18.8
2/24	100	28	10.40	69 27.75	3.1	227	22.8	76.2	0.152E-01	22.0	1014.4	1				2	40	3	190	7	19.4
2/24	130	28	9.59	69 27.15	7.8	227	23.0	71.7	0.145E-01	22.3	1014.1	1				2	240	4	350	19	19.0
2/24	200	28	9.94	69 27.35	7.2	232	22.8	77.0	0.154E-01	22.3	1014.0	5				2	300	10	320	20	19.5
2/24	230	28	12.51	69 31.75	5.8	246	22.5	77.6	0.152E-01	21.4	1014.1	2				2	230	7	10	18	19.3
2/24	300	28	10.51	69 31.16	6.7	247	22.3	80.7	0.157E-01	21.5	1014.4	5				2	100	7	120	8	19.3
2/24	330	28	9.39	69 30.79	6.2	81	22.8	77.8	0.135E-01	21.4	1014.0	5				2	140	6	320	16	19.6
2/24	400	28	8.19	69 29.02	8.1	232	22.3	79.2	0.135E-01	21.9	1013.9	5				2	40	6	300	10	19.5
2/24	430	28	10.43	69 29.34	3.7	229	22.3	81.3	0.136E-01	21.3	1013.7	5				2	230	6	0	17	19.6
2/24	500	28	8.72	69 30.85	3.1	226	22.9	79.3	0.160E-01	21.5	1013.7	5				2	90	6	100	7	19.9
2/24	530	28	9.65	69 27.75	7.7	229	22.4	81.6	0.139E-01	21.6	1013.5	1				2	310	6	300	17	19.7
2/24	600	28	9.60	69 29.39	7.0	211	22.8	81.1	0.162E-01	21.3	1012.9	1				2	240	6	340	19	20.0
2/24	630	28	8.93	69 29.05	6.8	221	22.2	85.7	0.165E-01	21.4	1012.9	1				2	90	7	100	10	20.0
2/24	700	28	9.97	69 28.62	5.3	212	22.5	85.9	0.169E-01	21.3	1012.4	1				2	260	6	330	15	20.3
2/24	730	28	9.00	69 29.55	4.6	219	22.4	85.0	0.166E-01	21.4	1012.4	5				2	90	7	80	7	20.1
2/24	800	28	9.75	69 27.81	3.2	227	22.2	85.7	0.165E-01	21.4	1012.6	5				2	290	6	320	14	20.0
2/24	830	28	9.15	69 30.15	4.0	230	22.2	89.1	0.172E-01	21.4	1012.9	5				2	90	6	90	3	20.4
2/24	900	28	9.31	69 26.49	8.7	222	22.2	85.7	0.163E-01	21.4	1012.4	5				2	300	6	300	19	20.0
2/24	930	28	10.91	69 29.15	5.7	224	22.4	84.1	0.164E-01	21.4	1012.4	2				2	240	6	350	17	20.0
2/24	1000	28	9.47	69 28.28	8.1	217	22.8	82.7	0.165E-01	21.3	1013.4	1				2	300	7	300	18	20.2
2/24	1030	28	9.72	69 35.92	7.2	202	21.8	88.0	0.164E-01	21.3	1012.2	3				2	270	10	320	20	19.9
2/24	1100	28	8.43	69 37.83	7.7	204	22.2	85.7	0.163E-01	22.3	1012.3	3				2	240	10	340	24	20.0
2/24	1130	28	6.24	69 42.05	10.1	194	22.3	90.0	0.173E-01	23.1	1013.0	5				2	270	6	300	22	20.6
2/24	1200	28	6.26	69 45.44	9.6	205	22.3	85.9	0.169E-01	23.3	1013.1	3				2	270	6	310	22	20.3
2/24	1230	28	7.16	69 46.34	7.7	202	22.7	84.3	0.167E-01	23.3	1013.5					0	0	0	0	0.0	
2/24	1300	28	11.20	69 45.84	5.7	199	22.0	82.7	0.165E-01	23.4	1014.0	9				2	0	9	250	4	20.2
2/24	1330	28	14.60	69 44.15	8.8	221	23.3	84.8	0.174E-01	23.2	1014.2	5				2	90	9	100	13	20.9
2/24	1400	28	14.46	69 40.75	8.2	224	23.3	83.6	0.168E-01	23.0	1014.2	2				2	90	7	110	12	20.4
2/24	1430	28	14.03	69 36.42	8.5	206	22.8	86.1	0.172E-01	22.5	1014.3	9				2	90	10	80	13	20.6
2/24	1500	28	12.36	69 31.53	6.6	206	22.8	84.4	0.168E-01	21.8	1014.4	9				3	150	2	50	14	20.4
2/24	1530	28	10.89	69 33.52	8.0	212	23.0	86.2	0.174E-01	22.0	1014.0	9				240	6	340	21	20.8	
2/24	1600	28	9.91	69 35.10	5.8	203	23.4	78.3	0.162E-01	22.0	1013.8	7				320	5	270	10	20.2	
2/24	1630	28	11.62	69 36.89	9.5	204	23.5	80.8	0.168E-01	22.3	1013.4	7				280	2	290	19	20.6	
2/24	1700	28	12.83	69 36.15	8.8	219	23.8	77.7	0.164E-01	22.8	1013.1	7				40	3	180	12	20.3	
2/24	1730	28	14.38	69 34.90	8.2	189	22.2	87.4	0.169E-01	22.3	1011.9	7				200	1	350	17	20.2	
2/24	1800	28	14.13	69 35.12	10.3	239	23.2	83.1	0.169E-01	22.3	1011.9	7				240	0	0	20	20.6	
2/24	1830	28	12.97	69 33.18	7.3	231	23.1	85.3	0.173E-01	21.9	1011.5	2				120	10	70	14	20.8	
2/24	1900	28	10.62	69 32.18	8.4	223	23.7	86.2	0.173E-01	21.7	1011.0	237				240	10	350	26	21.0	
2/24	1930	28	8.94	69 36.96	11.6	214	23.2	84.7	0.173E-01	22.1	1010.8	2				280	10	280	22	20.8	
2/24	2000	28	12.97	69 36.35	9.9	224	23.2	86.4	0.176E-01	22.3	1011.0	7									

Table Vb-3 (Cont)

	DATE	TIME	LAT	LONG	WS	WD	AT	RH	ABS HUM	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW
2/25	800	28	6.30	69 28.99	12.3	209	22.2	87.5	0.169E-01	21.5	1005.3	5	70	9	120	18	20.2	
2/25	830	28	7.72	69 24.60	10.9	229	22.7	90.4	0.179E-01	22.2	1005.3	5	120	7	90	20	21.0	
2/25	900	28	6.97	69 22.95	11.6	245	22.6	85.3	0.170E-01	22.9	1004.9	5	220	6	20	28	20.5	
2/25	930	28	6.62	69 26.28	13.9	220	22.5	86.8	0.170E-01	22.0	1004.4	5	270	7	320	32	20.4	
2/25	1000	28	7.17	69 27.61	10.8	214	22.7	87.0	0.173E-01	21.3	1004.3	5	65	9	130	14	20.6	
2/25	1030	28	7.93	69 24.31	3.7	273	21.2	95.7	0.175E-01	22.5	1004.2	5	120	9	100	5	20.2	
2/25	1100	28	7.03	69 25.18	11.1	213	22.6	89.5	0.177E-01	22.8	1003.7	7	3	240	7	340	28	20.8
2/25	1130	28	6.16	69 26.05	10.0	243	19.8	80.6	0.149E-01	22.1	1004.1	9	4	270	6	340	25	18.1
2/25	1200	28	5.06	69 29.11	10.9	254	21.1	91.2	0.165E-01	21.4	1003.6	9	4	215	7	30	27	19.6
2/25	1230	28	5.50	69 25.30	13.2	231	21.3	91.3	0.167E-01	22.2	1003.8	9	3	65	9	160	17	19.8
2/25	1300	28	8.02	69 24.14	13.7	235	20.4	89.8	0.157E-01	22.0	1003.6	5	3	270	4	330	30	18.8
2/25	1330	28	8.26	69 26.00	12.0	221	21.4	90.5	0.167E-01	22.4	1003.3	5	5	290	4	300	25	19.8
2/25	1400	28	9.06	69 27.37	12.8	237	21.5	87.0	0.161E-01	22.3	1003.5	5	5	110	8	110	21	19.5
2/25	1430	28	6.49	69 24.32	9.8	241	22.0	82.2	0.157E-01	22.3	1003.4	5	5	140	7	80	19	19.4
2/25	1500	28	4.49	69 24.45	8.0	241	22.1	86.6	0.166E-01	22.5	1003.2	5	5	270	7	340	22	20.0
2/25	1530	28	3.52	69 28.04	8.9	228	22.7	81.1	0.161E-01	22.0	1002.9	5	6	270	7	330	23	19.9
2/25	1600	28	3.35	69 22.30	11.8	269	22.2	85.8	0.165E-01	22.2	1003.0	5	5	90	8	180	15	20.0
2/25	1630	28	3.39	69 24.34	9.2	271	22.6	79.4	0.157E-01	22.8	1002.3	5	4	0	6	290	19	19.6
2/25	1700	28	4.24	69 24.35	10.3	269	22.9	72.5	0.145E-01	22.7	1003.4	5	4	160	0	110	20	19.0
2/25	1730	28	4.26	69 30.41	9.9	235	23.1	63.6	0.129E-01	22.4	1002.3	13	4	270	8	350	27	18.0
2/25	1800	28	3.03	69 30.37	8.8	241	23.5	68.5	0.142E-01	22.4	1002.0	13	3	220	1	20	18	19.0
2/25	1830	28	3.56	69 29.52	11.2	256	22.9	72.5	0.145E-01	22.4	1001.6	13	5	50	8	220	15	19.0
2/25	1900	28	5.12	69 26.66	10.7	257	22.8	69.3	0.138E-01	22.4	1001.6	23	5	50	7	220	15	18.5
2/25	1930	28	7.05	69 25.08	11.5	232	23.2	70.5	0.144E-01	22.5	1001.6	23	5	220	2	30	24	19.0
2/25	2000	28	7.04	69 25.82	12.5	250	22.9	72.5	0.145E-01	22.4	1001.1	23	5	350	4	270	24	19.0
2/25	2030	28	8.02	69 26.30	12.5	230	22.6	74.8	0.149E-01	22.3	1000.9	23	5	340	8	270	23	19.2
2/25	2100	28	11.99	69 26.46	9.9	263	20.2	84.4	0.145E-01	22.6	1001.1	33	5	10	8	280	19	18.0
2/25	2130	28	15.56	69 26.11	12.1	261	21.0	83.5	0.147E-01	22.7	1001.1	53	5	350	8	290	25	18.4
2/25	2200	28	19.04	69 25.82	13.6	292	20.5	80.2	0.141E-01	22.5	1001.7	58	6	135	8	150	23	17.8
2/25	2230	28	16.57	69 22.33	11.7	291	20.7	79.3	0.141E-01	22.7	1001.9	5	6	125	8	160	15	17.9
2/25	2300	28	13.81	69 18.84	12.5	289	20.6	72.7	0.128E-01	22.7	1002.3	5	6	130	8	150	17	17.0
2/25	2330	28	10.92	69 15.35	10.9	33	20.6	72.7	0.128E-01	22.7	1002.7			135	8	260	21	17.0
2/26	0	28	7.99	69 12.64	8.8	16	20.5	70.1	0.123E-01	23.3	1002.8			135	8	270	15	16.6
2/26	30	28	5.24	69 9.14	11.3	281	20.5	70.1	0.123E-01	23.4	1002.7	1		140	8	130	16	16.6
2/26	100	28	2.26	69 5.95	10.3	281	20.7	71.1	0.126E-01	23.4	1003.0	5		45	8	260	17	16.9
2/26	130	28	3.38	69 1.91	10.8	297	20.4	85.4	0.149E-01	23.4	1003.2			60	8	260	18	18.3
2/26	200	28	6.43	68 59.13	8.9	277	20.7	67.7	0.120E-01	23.3	1003.4			45	8	260	14	16.5
2/26	230	28	9.33	68 55.65	10.4	297	20.1	76.4	0.131E-01	23.5	1003.4			40	8	280	20	17.0
2/26	300	28	12.58	68 52.44	8.3	275	20.7	69.5	0.123E-01	23.4	1003.1			35	8	270	14	16.7
2/26	330	28	15.58	68 48.96	11.6	279	20.7	67.9	0.120E-01	23.3	1002.9			30	8	270	21	16.5
2/26	400	28	19.01	68 46.01	12.1	260	20.2	68.2	0.117E-01	23.1	1002.4			300	8	330	30	16.1
2/26	430	28	21.67	68 48.19	12.6	264	20.4	65.2	0.114E-01	22.7	1001.9			290	7	340	31	15.9
2/26	500	28	23.83	68 31.16	12.7	273	19.5	73.3	0.121E-01	21.3	1002.0			300	8	340	32	16.1
2/26	530	28	26.11	68 34.01	13.1	270	19.0	74.6	0.120E-01	21.1	1002.0			310	8	330	32	15.8
2/26	600	28	28.53	68 36.78	12.7	282	18.5	76.3	0.119E-01	21.4	1001.8			0	0	0	0	0.0
2/26	630	28	30.85	68 39.91	12.2	293	17.9	78.0	0.118E-01	21.8	1001.6			320	8	340	31	15.2
2/26	700	28	33.34	69 2.46	13.7	284	17.4	75.8	0.111E-01	22.0	1001.6			310	8	340	34	14.3
2/26	730	28	34.17	69 5.61	13.5	293	17.0	81.0	0.116E-01	22.0	1002.0		6	230	9	50	35	14.7
2/26	800	28	31.44	69 8.66	17.9	311	16.5	96.5	0.134E-01	21.7	1002.3	7		240	8	60	38	15.8
2/26	830	28	28.17	69 14.01	14.5	312	16.6	6.0	0.000E+00	21.9	1003.0	7		240	7	60	31	0.0
2/26	900	28	27.08	69 15.43	13.9	314	16.7	86.4	0.119E-01	22.0	1003.4	7		240	8	60	30	14.8
2/26	930	28	23.01	69 17.77	15.1	294	17.4	75.7	0.111E-01	21.8	1004.4	5		210	8	70	31	14.5
2/26	1000	28	21.46	69 20.69	15.9	308	17.2	82.1	0.119E-01	22.0	1003.1	6		235	8	60	34	15.0
2/26	1030	28	17.71	69 23.33	12.8	308	17.7	67.1	0.100E-01	22.2	1005.1	5		135	8	170	17	13.8
2/26	1100	28	16.40	69 21.89	17.0	314	18.1	60.7	0.926E-02	22.2	1006.1	7		135	8	180	25	13.4
2/26	1130	28	13.32	69 18.43	12.3	303	17.5	69.5	0.102E-01	22.5	1006.9	2		130	8	170	16	13.9
2/26	1200	28	11.07	69 18.07	11.3	303	17.5	66.6	0.985E-02	22.2	1006.7	2		130	8	180	14	13.6
2/26	1230	28	5.97	69 10.15	11.4	24	17.7	74.2	0.111E-01	23.2	1007.2	2		125	8	280	22	14.6
2/26	1300	28	5.03	69 10.90	17.8	316	17.6	78.6	0.117E-01	23.2	1007.9	8		225	7	80	35	15.0
2/26	1330	28	2.63	69 13.27	19.1	289	17.9	67.9	0.102E-01	23.1	1008.4	5		220	7	60	40	14.0
2/26	1400	28	0.23	69 15.72	17.5	278	18.9	60.8	0.973E-02	23.0	1008.6	1		220	7	50	38	14.1
2/26	1430	27	57.93	69 18.33	14.6	308	18.3	71.2	0.110E-01	23.3	1009.2	5		225	7	70	30	14.8
2/26	1500	27	55.43	69 21.26	17.7	293	18.1	70.1	0.107E-01	23.0	1009.4	1		225	6	60	37	14.5
2/26	1530	27	54.88	69 24.04	13.8	300	18.2	65.0	0.998E-02	23.2	1010.0	1		265	5	30	31	14.0
2/26	1600	27	54.98	69 26.96	19.2	292	17.9	59.5</										

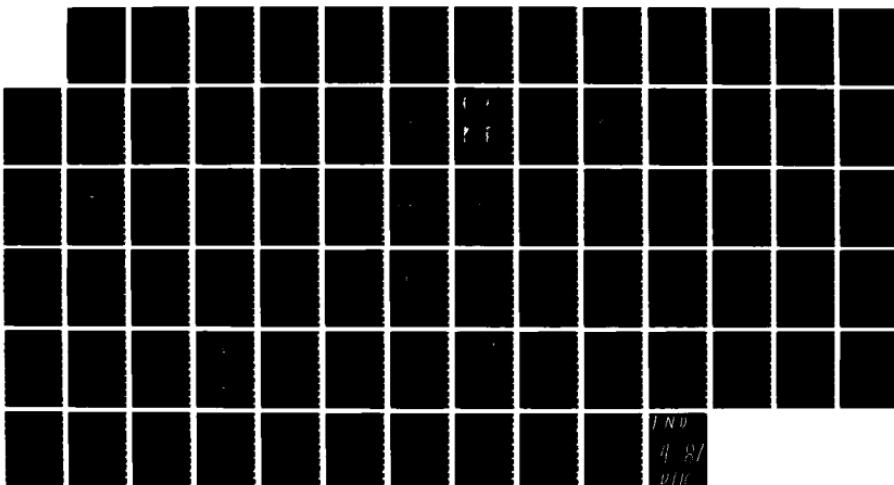
Table Vb-3 (Cont)

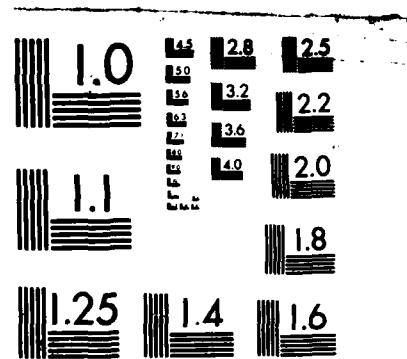
	DATE	TIME	LAT	LONG	WS	WD	AT	RH	AMS	MNM	SST	BP	CLOUD	WAVES	SC	SS	AD	AS	TW	
2/27	300	26 38.34	69 29.65	3.0	280	19.2	46.1	0.750E-02	23.5	1014.7	1	1 28	3	180	8	40	9	12.5		
2/27	330	26 34.48	69 30.00	3.1	269	19.2	46.1	0.750E-02	24.0	1014.7	5	28	3	270	7	0	13	12.5		
2/27	400	26 33.45	69 33.71	1.5	269	19.3	53.2	0.871E-02	24.1	1014.6	5	28	3	270	7	0	10	13.5		
2/27	430	26 34.23	69 37.47	1.5	279	19.8	51.6	0.869E-02	24.3	1014.8	5	28	3	280	8	0	11	13.7		
2/27	500	26 34.73	69 41.60	1.4	169	19.8	50.1	0.843E-02	24.1	1014.8	5	270	8	340	8	13	13.5			
2/27	530	26 34.89	69 45.65	2.8	159	20.0	51.1	0.871E-02	24.2	1014.3	5	270	8	320	8	13	8			
2/27	600	26 34.86	69 49.50	2.9	183	20.0	51.1	0.872E-02	24.3	1013.4	5	260	8	330	11	13	8			
2/27	630	26 35.08	69 54.27	3.2	213	20.2	53.0	0.913E-02	24.3	1013.4	5	260	8	340	13	14	2			
2/27	700	26 34.70	69 57.76	2.3	201	20.3	54.6	0.947E-02	24.2	1013.4	5	260	8	340	11	14	5			
2/27	730	26 34.61	70 1.76	2.7	208	20.2	55.3	0.953E-02	24.0	1012.9	5	260	8	340	12	14	5			
2/27	800	26 34.32	70 6.08	2.3	201	20.4	51.0	0.889E-02	22.8	1012.9	5	260	8	340	11	14	1			
2/27	830	26 33.29	70 9.62	4.6	206	20.0	58.9	0.100E-01	24.0	1012.9	5	0	8	270	4	14	8			
2/27	900	26 39.35	70 8.88	2.1	236	20.0	52.7	0.898E-02	24.0	1013.2	5	10	8	330	6	14	0			
2/27	930	26 45.09	70 8.46	4.4	200	20.0	56.5	0.964E-02	24.0	1013.1	5	1 32	9	3	0	8	270	3	14	5
2/27	1000	26 47.19	70 8.57	3.8	242	19.9	54.8	0.929E-02	24.0	1013.3	5	1 32	9	3	355	8	290	11	14	2
2/27	1030	26 51.22	70 8.73	8.0	229	19.8	53.9	0.909E-02	24.0	1013.0	5	1 32	9	3	0	8	260	12	14	0
2/27	1100	26 55.36	70 8.68	6.7	207	19.9	54.1	0.916E-02	23.8	1013.2	1	1 32	9	3	0	8	240	7	14	1
2/27	1130	26 59.47	70 8.58	7.6	215	20.0	60.5	0.103E-01	23.8	1013.1	1	1 32	9	3	0	7	240	10	15	0
2/27	1200	27 3.36	70 8.97	6.5	191	20.2	55.2	0.952E-02	23.7	1013.8	1	1 33	9	5	0	8	210	5	14	5
2/27	1230	27 7.78	70 8.38	8.4	207	20.4	57.8	0.101E-01	23.5	1014.0	1	1 33	9	5	0	8	230	10	15	0
2/27	1300	27 11.68	70 7.98	6.3	205	20.4	54.0	0.941E-02	23.7	1014.3	1	1 33	9	5	0	8	240	6	14	5
2/27	1330	27 15.66	70 8.00	7.2	179	20.3	55.4	0.960E-02	23.5	1014.4	1	1 33	9	4	0	8	180	6	14	6
2/27	1400	27 19.62	70 7.90	7.3	198	20.7	57.5	0.102E-01	23.4	1014.1	4	1 33	9	4	0	8	220	7	15	2
2/27	1430	27 23.59	70 7.88	6.1	198	20.9	63.9	0.115E-01	23.3	1014.1	4	1 35	9	4	0	8	230	5	16	2
2/27	1500	27 27.47	70 7.86	8.0	184	20.9	60.0	0.108E-01	23.4	1014.3	5	2 35	9	4	350	8	210	6	15	7
2/27	1530	27 31.46	70 8.04	7.3	193	21.0	58.2	0.105E-01	23.5	1014.0	0	0	0	0	0	0	0	0	0	
2/27	1600	27 35.31	70 8.29	6.5	201	21.0	56.3	0.102E-01	23.3	1013.8	5	2 35	4	0	8	230	6	15	3	
2/27	1630	27 39.34	70 8.38	7.2	194	21.0	61.7	0.111E-01	23.4	1013.9	5	2 35	4	10	8	190	6	16	0	
2/27	1700	27 43.33	70 7.80	9.2	213	21.2	61.9	0.113E-01	23.1	1013.8	2	2 35	4	10	8	220	11	16	2	
2/27	1730	27 47.35	70 7.84	9.9	227	21.2	55.1	0.101E-01	23.0	1013.4	2	3 33	4	0	8	250	15	15	3	
2/27	1800	27 51.36	70 7.82	11.9	222	21.2	63.5	0.116E-01	23.0	1012.9	2	3 33	4	0	8	240	18	16	4	
2/27	1830	27 55.35	70 7.90	12.2	193	21.2	62.8	0.114E-01	23.0	1011.9	2	4 30	4	0	8	200	16	16	3	
2/27	1900	27 59.29	70 7.87	8.5	215	21.8	62.7	0.116E-01	23.0	1011.9	2	4 30	4	0	8	240	11	16	8	
2/27	1930	28 3.29	70 7.75	9.9	218	21.8	60.4	0.114E-01	23.1	1011.5	2	4 30	4	0	8	240	14	16	5	
2/27	2000	28 7.26	70 7.75	10.7	205	22.0	59.2	0.113E-01	23.0	1011.0	2	4 30	4	0	8	220	14	16	5	
2/27	2030	28 11.30	70 7.77	10.7	195	22.0	61.4	0.117E-01	23.0	1011.0	2	3 30	4	350	8	220	14	16	8	
2/27	2100	28 15.33	70 7.83	11.2	196	21.4	63.8	0.118E-01	23.0	1011.2	1	4 30	2	350	8	220	15	16	6	
2/27	2130	28 19.37	70 7.94	10.4	209	21.8	65.0	0.123E-01	23.3	1011.0	1	4	350	8	240	15	17	1		
2/27	2200	28 23.36	70 7.80	12.7	197	21.8	64.2	0.121E-01	22.9	1011.0	1	4	350	8	220	18	17	0		
2/27	2230	28 27.28	70 7.68	11.3	203	21.8	68.9	0.130E-01	22.8	1010.8	1	4	350	8	230	16	17	6		
2/27	2300	28 31.32	70 7.87	9.0	206	21.6	65.6	0.122E-01	22.6	1010.9	1	4	350	8	240	12	17	0		
2/27	2330	28 35.42	70 8.10	10.9	210	21.5	65.5	0.121E-01	22.5	1011.0	0	350	8	240	16	16	9			
2/28	0	28 39.10	70 8.35	9.9	208	21.7	63.4	0.119E-01	22.6	1010.9	0	350	8	240	14	16	8			
2/28	30	28 43.65	70 8.42	9.0	219	21.5	67.0	0.124E-01	22.9	1011.2	0	355	8	250	13	17	1			
2/28	100	28 47.74	70 8.58	8.4	221	21.7	64.1	0.120E-01	22.9	1011.1	1	350	8	260	13	16	9			
2/28	130	28 49.02	70 4.70	10.7	223	21.7	66.5	0.125E-01	22.9	1011.1	1	90	9	110	16	17	2			
2/28	200	28 49.02	69 59.65	9.4	224	21.7	64.1	0.120E-01	22.8	1011.1	1	90	8	110	14	16	9			
2/28	230	28 48.90	69 55.00	10.9	220	21.5	60.0	0.111E-01	22.5	1011.5	0	90	8	110	17	16	2			
2/28	300	28 48.56	69 49.50	10.4	230	21.6	65.6	0.122E-01	22.2	1011.5	0	90	8	120	15	17	0			
2/28	330	28 48.46	69 44.83	11.8	219	21.3	70.8	0.130E-01	21.0	1011.6	1	90	8	110	19	17	4			
2/28	400	28 48.64	69 39.99	10.9	210	21.3	71.6	0.131E-01	20.9	1011.9	1	80	8	110	17	17	3			
2/28	430	28 48.86	69 35.13	10.3	213	21.2	72.3	0.132E-01	21.0	1012.0	1	90	8	100	17	17	5			
2/28	500	28 48.93	69 30.28	10.4	220	21.5	72.6	0.135E-01	21.0	1012.4	1	80	8	120	15	17	8			
2/28	530	28 49.09	69 25.57	10.9	210	21.5	74.2	0.138E-01	21.0	1012.4	3	80	8	110	17	18	0			
2/28	600	28 49.02	69 20.82	11.4	209	21.8	69.7	0.132E-01	21.0	1011.9	3	80	8	110	18	17	7			
2/28	630	28 48.97	69 15.97	9.0	225	21.6	76.0	0.142E-01	21.0	1011.9	3	90	8	110	13	18	3			
2/28	700	28 48.88	69 11.01	12.4	226	22.0	73.0	0.141E-01	21.0	1011.9	3	90	8	120	19	18	4			
2/28	730	28 48.86	69 6.13	10.9	229	22.0	80.5	0.154E-01	21.3	1011.9	3	90	8	120	16	19	2			
2/28	800	28 49.43	69 1.31	10.6	223	22.0	78.8	0.150E-01	21.5	1011.9	3	90	8	123	15	19	0			
2/28	830	28 49.23	68 56.23	9.0	233	22.2	77.3	0.149E-01	21.5	1012.0	2	90	7	120	12	19	0			
2/28	900	28 49.17	68 51.30	9.2	206	22.5	73.6	0.144E-01	21.5	1012.0	2	90	8	90	16	18	8			
2/28	930	28 48.92	68 46.37	8.3	219	22.2	77.3	0.149E-01	21.5	1012.4	2	100	8	90	14	19	0			
2/28	1000	28 48.65	68 41.68	8.5	234	21.7	82.3	0.160E-01	21.5	1012.6	1	3	90	8	120	11	18	9		
2/28	1030	28 48.70	68 36.82	10.1	203	22.3	82.4	0.1												

Table Vb-3 (Cont.)

	DATE	TIME	LAT	LONG	WS	WD	AT	RH	ABS HUM	SST	RF	CLOUD	WAVES	SC	SS	AD	AS	TW
	2/28	2200	28 28.77	68 34.90	8.7	169	23.1	88.0	0.179E-01	22.8	1024.1	15	2 28	8	3	355	8 170	9 21.1
	2/28	2230	28 32.48	68 34.71	9.7	169	23.1	88.8	0.180E-01	22.9	1013.9	1	2 29	8	3	355	8 170	11 21.2
	2/28	2300	28 36.03	68 34.32	9.1	163	23.1	92.3	0.187E-01	22.9	1014.1	1	2 29	8	3	355	8 160	10 21.6
	2/28	2330	28 39.59	68 34.26	9.8	159	23.2	90.6	0.185E-01	22.9	1013.7					340	8 180	11 21.5
3/1	0	28 43.39	68 34.83	10.2	160	23.2	89.7	0.183E-01	22.8	1013.7					350	8 165	12 21.4	
3/1	30	28 44.54	68 31.07	9.2	149	23.0	92.2	0.186E-01	22.3	1013.6					80	8 50	22 21.5	
3/1	100	28 44.64	68 26.10	9.0	173	23.3	89.8	0.184E-01	21.8	1013.7					90	8 60	20 21.5	
3/1	130	28 44.66	68 21.66	9.0	173	22.0	97.0	0.185E-01	21.3	1014.0					90	8 60	20 21.1	
3/1	200	28 44.61	68 16.73	8.5	174	22.6	92.0	0.181E-01	21.4	1013.9					90	8 60	19 21.1	
3/1	230	28 42.84	68 15.00	9.3	176	22.4	96.3	0.188E-01	21.2	1014.2					190	6 350	24 21.4	
3/1	300	28 39.36	68 14.93	7.7	169	23.0	92.2	0.186E-01	21.2	1013.7					170	7 0	22 21.5	
3/1	330	28 36.20	68 14.62	9.8	169	22.9	94.8	0.190E-01	21.3	1013.9					170	6 0	25 21.7	
3/1	400	28 33.01	68 14.40	8.5	162	22.8	92.1	0.184E-01	21.6	1013.8					190	6 340	22 21.3	
3/1	430	28 29.96	68 14.32	9.1	157	23.2	92.3	0.188E-01	22.4	1013.8					185	7 340	24 21.7	
3/1	500	28 27.12	68 14.32	9.9	176	23.0	86.2	0.174E-01	23.1	1013.6					190	7 350	26 20.8	
3/1	530	28 23.98	68 14.53	10.1	152	23.2	89.7	0.183E-01	23.1	1013.6					180	7 340	26 21.4	
3/1	600	28 20.84	68 14.73	7.2	189	23.4	89.0	0.184E-01	23.0	1013.4					190	7 0	21 21.5	
3/1	630	28 17.70	68 14.94	9.6	157	23.3	90.7	0.186E-01	22.8	1012.9					185	7 340	25 21.6	
3/1	700	28 14.51	68 14.81	9.1	152	23.3	89.8	0.184E-01	22.8	1012.1					180	7 340	24 21.5	
3/1	730	28 11.29	68 14.64	10.4	166	23.4	93.3	0.193E-01	22.9	1011.9					180	7 350	27 22.0	
3/1	800	28 8.98	68 14.40	9.8	164	23.4	93.3	0.193E-01	23.0	1011.5	3 18	8	3	175	0 350	19 22.0		
3/1	830	28 9.05	68 14.36	9.8	169	23.2	95.8	0.195E-01	23.0	1011.3	3 18	8	3	180	1 350	20 22.1		
3/1	900	28 9.24	68 17.99	14.0	169	23.3	95.0	0.195E-01	22.8	1010.8					260	10 290	29 22.1	
3/1	930	28 8.72	68 22.91	12.6	153	23.2	97.6	0.199E-01	23.1	1010.5					250	11 290	26 22.3	
3/1	1000	28 8.81	68 23.94	10.8	159	23.0	0.100E.2	0.202E-01	22.8	1010.3	3	3			260	0 260	21 22.4	
3/1	1030	28 8.94	68 24.21	11.3	169	23.1	99.3	0.202E-01	22.8	1010.7	5	3			280	0 250	22 22.4	
3/1	1100	28 9.95	68 23.61	10.8	169	23.1	99.3	0.202E-01	22.8	1010.3	13	3			270	0 260	21 22.4	
3/1	1130	28 10.54	68 23.65	11.8	164	23.2	98.5	0.201E-01	22.8	1010.3	8	3			275	0 230	23 22.4	
3/1	1200	28 11.20	68 23.59	11.3	159	23.2	97.6	0.199E-01	22.4	1010.7	18	3			260	0 260	22 22.3	
3/1	1230	28 11.77	68 23.29	7.2	189	23.3	94.1	0.193E-01	22.8	1010.4	7	3			270	0 280	14 22.0	
3/1	1300	28 12.17	68 23.23	11.3	175	23.4	94.2	0.194E-01	22.8	1010.5	7	4			165	1 10	23 22.1	
3/1	1330	28 12.10	68 23.10	11.9	164	23.5	92.5	0.192E-01	22.8	1010.5	7	4			175	1 350	24 22.0	
3/1	1400	28 12.06	68 22.91	12.4	164	24.2	90.4	0.195E-01	22.8	1010.3	5	4			175	0 350	24 22.4	
3/1	1430	28 12.17	68 22.96	13.4	174	24.2	90.4	0.195E-01	22.8	1010.2	5	4			175	0 0	26 22.4	
3/1	1500	28 14.41	68 24.20	14.2	163	23.8	91.9	0.194E-01	22.9	1010.1	5	4			330	9 200	19 22.2	
3/1	1530	28 14.74	68 24.14	13.9	174	24.3	89.7	0.194E-01	22.9	1009.6	5	3			175	0 0	27 22.4	
3/1	1600	28 14.68	68 28.89	14.4	179	25.0	85.3	0.192E-01	22.9	1009.1	7	5			180	1 0	29 22.5	
3/1	1630	28 14.52	68 23.42	15.5	173	25.2	85.4	0.194E-01	22.8	1008.9	7	6			170	1 5	31 22.7	
3/1	1700	28 13.72	68 22.85	16.5	174	24.6	88.2	0.194E-01	22.9	1008.2	4	6			175	3 0	35 22.5	
3/1	1730	28 11.49	68 22.39	17.2	161	24.4	89.7	0.196E-01	22.9	1007.2	4	6			185	6 340	39 22.5	
3/1	1800	28 9.59	68 23.21	16.9	170	24.4	89.8	0.196E-01	22.8	1006.5	4	6			205	5 330	37 22.5	
3/1	1830	28 7.34	68 24.14	16.5	157	24.2	91.3	0.197E-01	22.9	1006.1	7	7			180	4 340	34 22.5	
3/1	1900	28 6.19	68 26.23	14.6	171	23.2	90.7	0.185E-01	22.8	1005.3	7	7			235	7 290	30 21.5	
3/1	1930	28 6.11	68 30.09	19.4	185	23.3	91.6	0.188E-01	22.8	1005.3	7	9			260	7 295	40 21.7	
3/1	2000	28 6.14	68 33.39	18.3	182	23.3	92.5	0.190E-01	22.9	1004.4	7	9			260	5 290	37 21.8	
3/1	2030	28 8.36	68 34.60	16.3	206	23.4	93.4	0.193E-01	23.0	1005.3	7	6			355	7 220	26 22.3	
3/1	2100	28 11.86	68 34.55	15.0	217	22.6	91.2	0.180E-01	23.0	1005.3	7	8			350	7 240	25 21.0	
3/1	2130	28 15.53	68 34.40	21.6	178	22.3	85.0	0.165E-01	23.0	1005.3	7	8			350	7 190	35 20.0	
3/1	2200	28 18.93	68 34.42	16.3	191	23.2	87.3	0.178E-01	23.1	1004.4	7	10			340	7 220	26 21.1	
3/1	2230	28 22.44	68 34.66	21.9	231	22.2	84.9	0.164E-01	22.9	1004.9	7	10			340	6 260	41 19.9	
3/1	2300	28 25.79	68 34.81	15.0	200	22.6	90.3	0.178E-01	22.7	1004.4	7	10			340	6 230	25 20.9	
3/1	2330	28 29.06	68 34.62	17.3	225	22.5	89.9	0.176E-01	22.4	1004.7	12				345	6 250	31 0.0	
3/2	0	28 32.24	68 34.96	16.3	249	23.3	89.6	0.174E-01	22.3	1005.0					350	6 270	31 0.0	
3/2	30	28 35.04	68 34.58	15.7	248	22.2	89.2	0.172E-01	23.8	1004.7					340	6 280	31 20.4	
3/2	100	28 37.13	68 34.31	13.2	268	21.9	83.8	0.159E-01	22.9	1004.9					340	6 300	28 19.5	
3/2	130	28 40.79	68 34.43	11.6	256	21.2	85.0	0.155E-01	23.0	1005.6					330	6 300	35 19.0	
3/2	200	28 43.59	68 34.46	16.9	262	20.9	81.4	0.146E-01	22.9	1005.7					330	6 290	32 18.4	
3/2	230	28 46.50	68 34.58	15.7	249	20.4	86.2	0.150E-01	22.4	1005.9					330	6 290	32 18.4	
3/2	300	28 49.46	68 34.80	15.3	238	20.1	81.9	0.144E-01	22.5	1005.8					340	6 270	29 18.0	
3/2	330	28 52.48	68 34.35	19.8	236	19.8	86.7	0.146E-01	21.4	1005.6					345	6 280	39 17.9	
3/2	400	28 55.18	68 34.38	17.3	239	20.4	70.0	0.122E-01	21.3	1005.8					340	6 270	33 16.5	
3/2	430	28 58.03	68 35.10	17.6	255	20.2	79.9	0.138E-01	21.3	1005.3					100	7 150	28 17.3	
3/2	500	28 59.12	68 32.04	16.3	233	20.2	71.4	0.123E-01	21.4	1005.3					85	7 140	26 16.5	
3/2	530	28 38.92	68 27.50	16.5	229	20.2	78.2	0.133E-01	21.4	1004.9					90	7 130	27 17.3	
3/2	600	28 38.89	68 24.30	19.4	253	20.2	75.7	0.130E-01	22.1	1004.9					90	6 160	32 17.0	
3/2	630	28 38.08	68 20.26	17.9	231	20.2	75.7	0.130E-01	22.6	1004.9					85	6 140	30 17.0	
3/2																		

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- JUNE 1986) CRUI. (U) WOODS HOLE OCEANOGRAPHIC
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UNCLASSIFIED NO0014-84-C-0134 F/G 8/3 NL





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NATIONAL BUREAU OF STANDARDS-1963-A

VI. OCEANUS Phase Two CTD Stations

Raymond Pollard, IOS completed six CTD stations in the vicinity of the central mooring array during FASINEX Phase Two. A complete summary of the work including times, positions, plots and listings are presented in FASINEX Technical Report #11, SeaSoar CTD Surveys during FASINEX in Appendix A.

Reference IOS Technical Report: Pollard, R.T., Read, J.F. & Smithers, J.
1986 SeaSoar CTD Surveys during FASINEX.
Institute of Oceanographic Sciences,
Report, No. 230, 111pp.

Figure VI-1 CTD Station Locations
Table VI-1 CTD Station Information Table

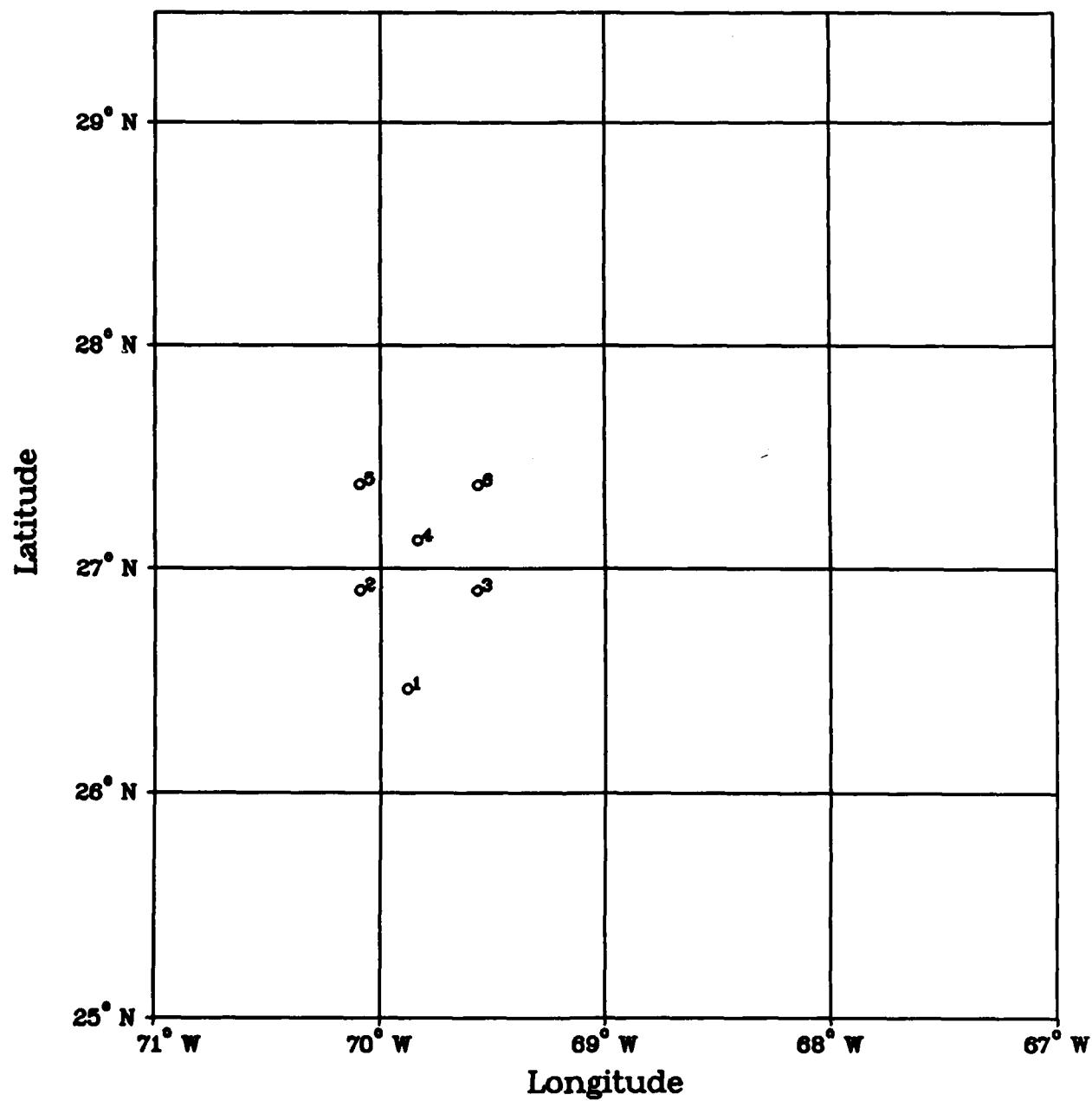
FASINEX Oceanus 175 CTD Stations

Figure VI-1: CTD Station Locations.

FASINEX CTD STATIONS - OCEANUS 175

Station	(GMT) Time	1986	INTERNAV Positions			Comments
			Latitude	Longitude		
1	1400	8 March	26 27.81	69 52.86		South of Central Array
2	1702	8 March	26 54.18	70 05.44		Lower southwest corner of mooring box
3	2043	8 March	26 54.07	69 34.21	F8	
4	2345	8 March	27 07.62	69 50.13		Midway between F6 & F4
5	0408	9 March	27 22.76	70 05.44	F2	
6	0628	9 March	27 22.51	69 33.87	F10	

Table VI-1: CTD Station Information.

VII. Vertical Current Meter (VCM) Data

VCMs are neutrally buoyant, free-floating instruments which are ballasted to sink to a predetermined depth. While floating at that depth the instrument makes measurements of the vertical velocity relative to itself, of pressure, and of temperature.

Relative vertical current is sensed by an array of vanes mounted axially around the float. Because the float compressibility is less than that of water, vertical motions in the water generate relative vertical flow past the vanes causing the entire float to rotate. This rotation is sensed relative to an internal compass. The sum of the pressure change (float vertical motion) and the rotation of the float (flow relative to the float) is a measure of total vertical water displacement, with a resolution of about 2 cm.

The VCM includes an AMF acoustic release receiver and a release of WHOI design. On command from the ship, or on preset command from an internal timer, the float drops a 900 gm weight and returns to the surface for recovery. A flashing light turns on at release time, and the "ping" rate doubles to confirm release.

Two VCM experiments were carried out during Phase Two on OCEANUS. The first dual experiment had a VCM ballasted to 140m and one ballasted to 90m. This is a 60 hour data set. The second deployment included three VCMs ballasted to 150, 95, and 175 m. This is a 48 hour data set.

Lloyd Regier's surface and 50 m drogued drifters were deployed and tracked at approximately the same time as the VCM work.

Some preliminary data are presented.

- Figure VII-1 Schematic of VCM
- Figure VII-2 Area 1 Drift Tracks
- Figure VII-3 Expanded Scale Drift Tracks of VCM 2 and 4
- Figure VII-4 Expanded Scale Drift Tracks of VCM 2, 4 and 5
- Table VII-1 VCM Drift Information
- Figure VII-5 Displacement Plots for VCM 2 and 4 - Deployment 1
- Figure VII-6 Displacement Plots for VCM 2, 4 and 5 - Deployment 2

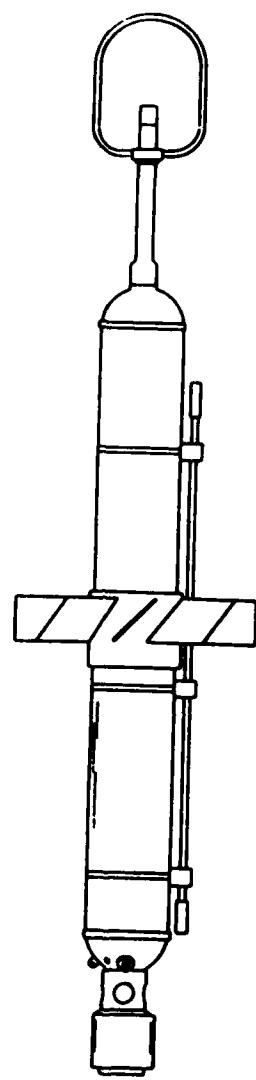


Figure VII-1: Schematic of VCM.

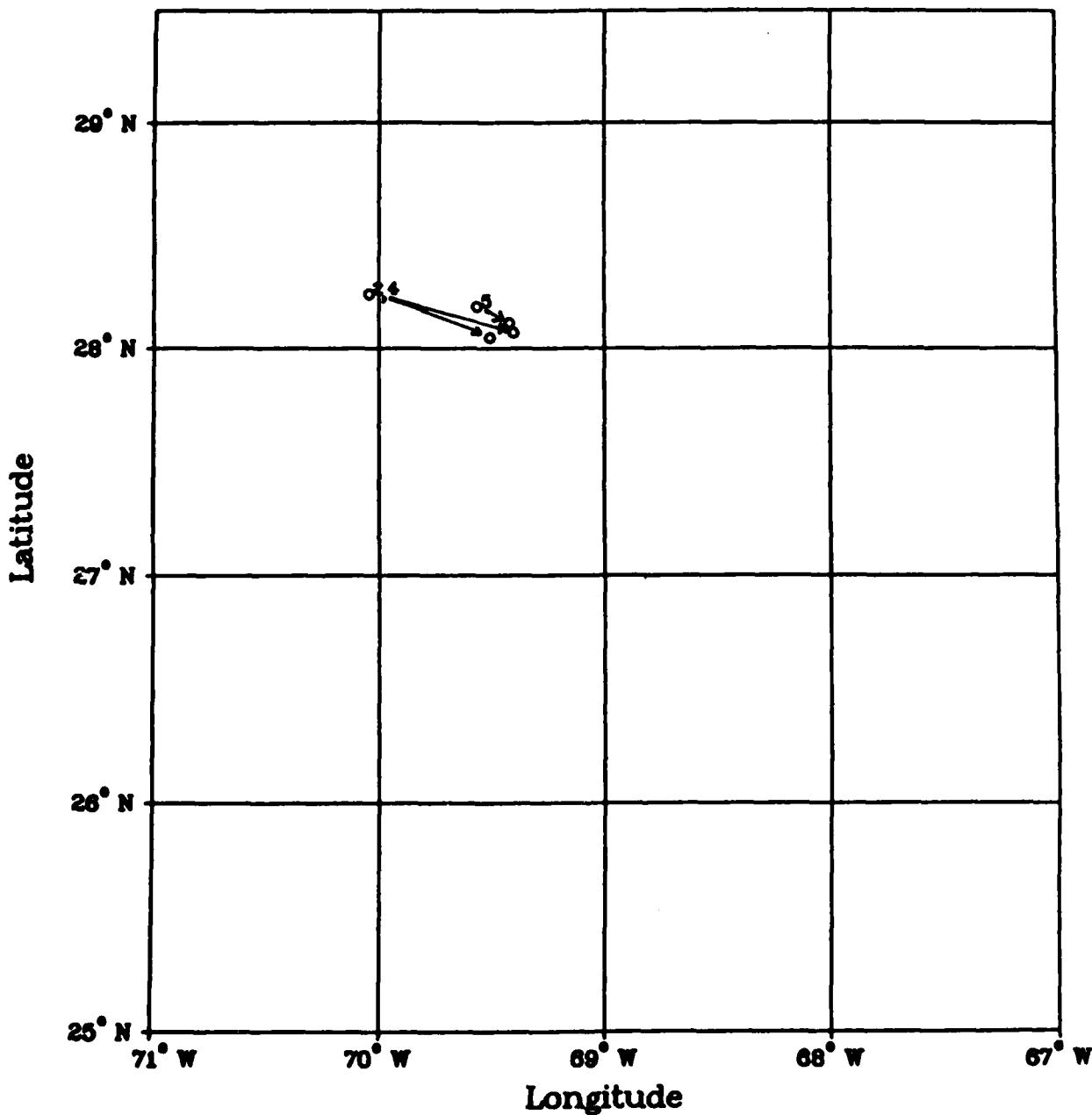
FASINEX Oceanus 175 VCM Drift Tracks

Figure VII-2: Area 1 Drift Tracks.

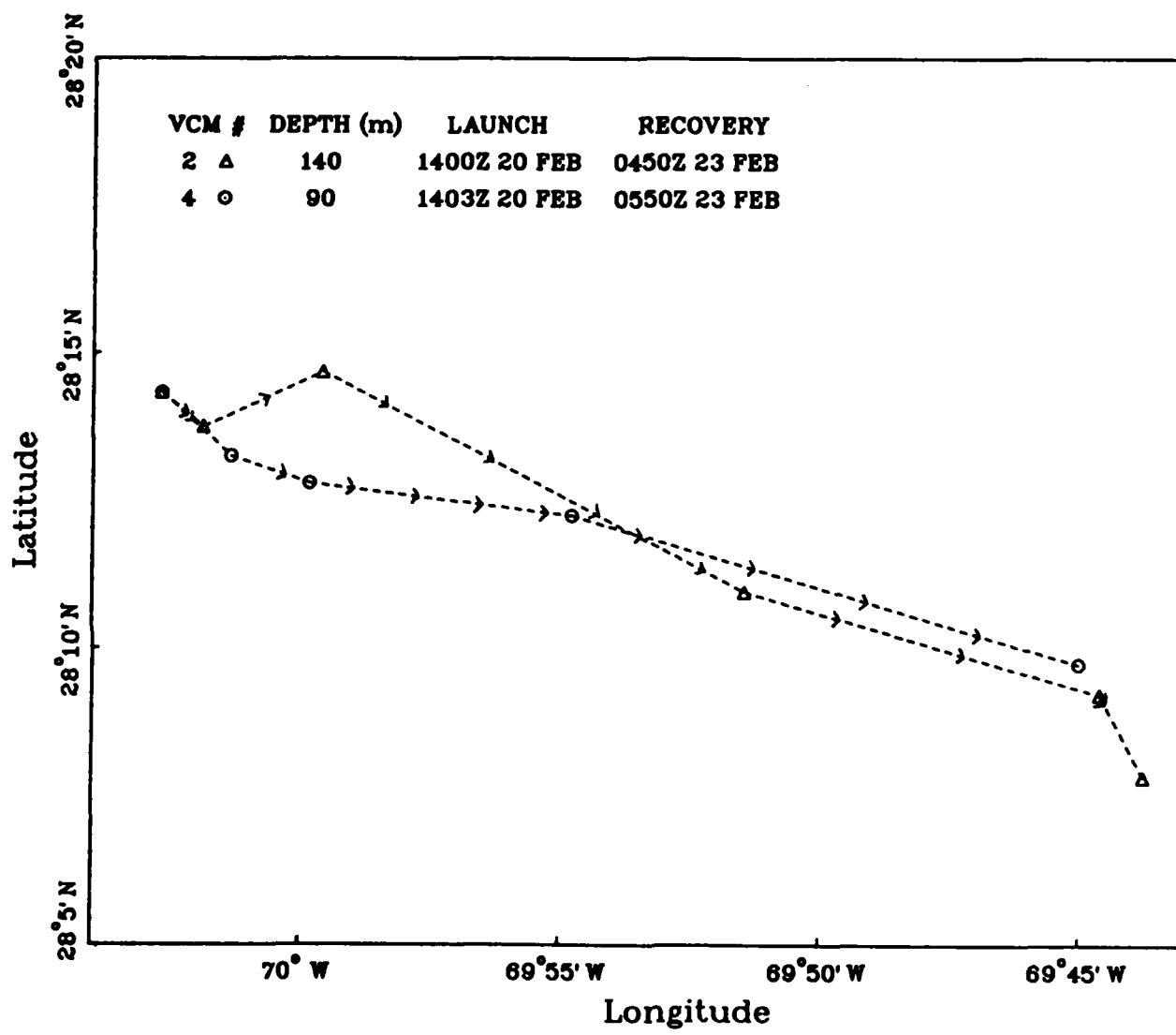


Figure VII-3: Expanded Scale Drift Tracks of VCM 2 and 4.

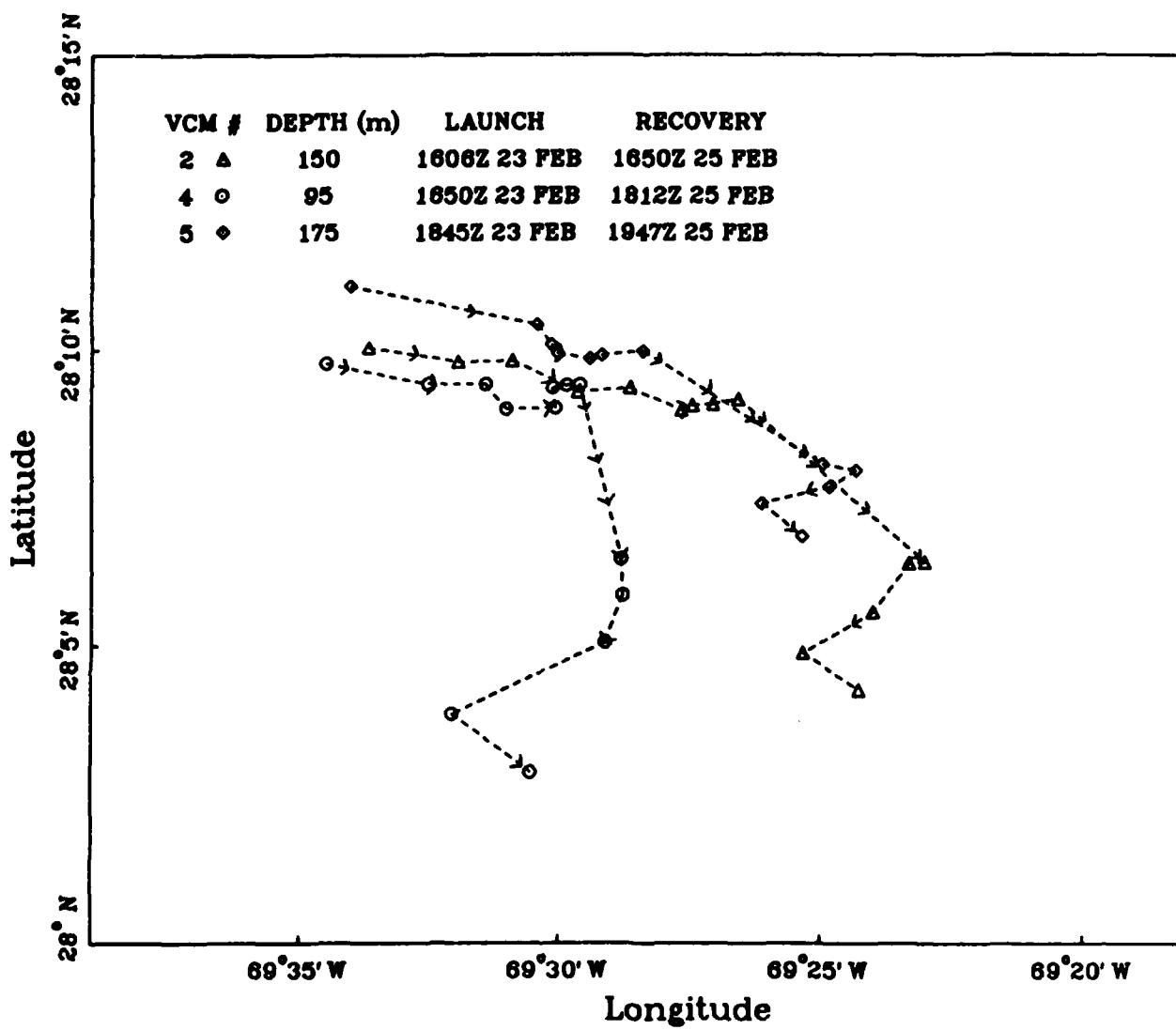


Figure VII-4: Expanded Scale Drift Track of VCM 2, 4 and 5.

OC175

VCM Drop #	Nominal Depth	Data Hours	Start Time (Z)	End Time (Z)	Comment	Deployment Latitude	Position Longitude	Retrieval Latitude	Position Longitude
1	140 m	56.8	20 Feb 86 1400	23 Feb 86 0450	VCM #2	28°14.33'	70°02.68'	28°07.83'	69°43.76'
2	90 m	57.78	20 Feb 86 1403	23 Feb 86 0550	VCM #4	28°14.33'	70°02.68'	28°09.73'	69°44.98'
3	150 m	42.7	23 Feb 86 1606	25 Feb 86 1649	VCM #2	28°10.04'	69°33.67'	28°04.25'	69°24.23'
4	95 m	43.4	23 Feb 86 1650	25 Feb 86 1812	VCM #4	28°09.77'	69°34.49'	28°02.87'	69°30.53'
5	175 m	44.95	23 Feb 86 1650	25 Feb 86 1947	VCM #5	28°11.08'	69°34.02'	28°06.84'	69°25.31'

Table VII-1: VCM Drift Information.

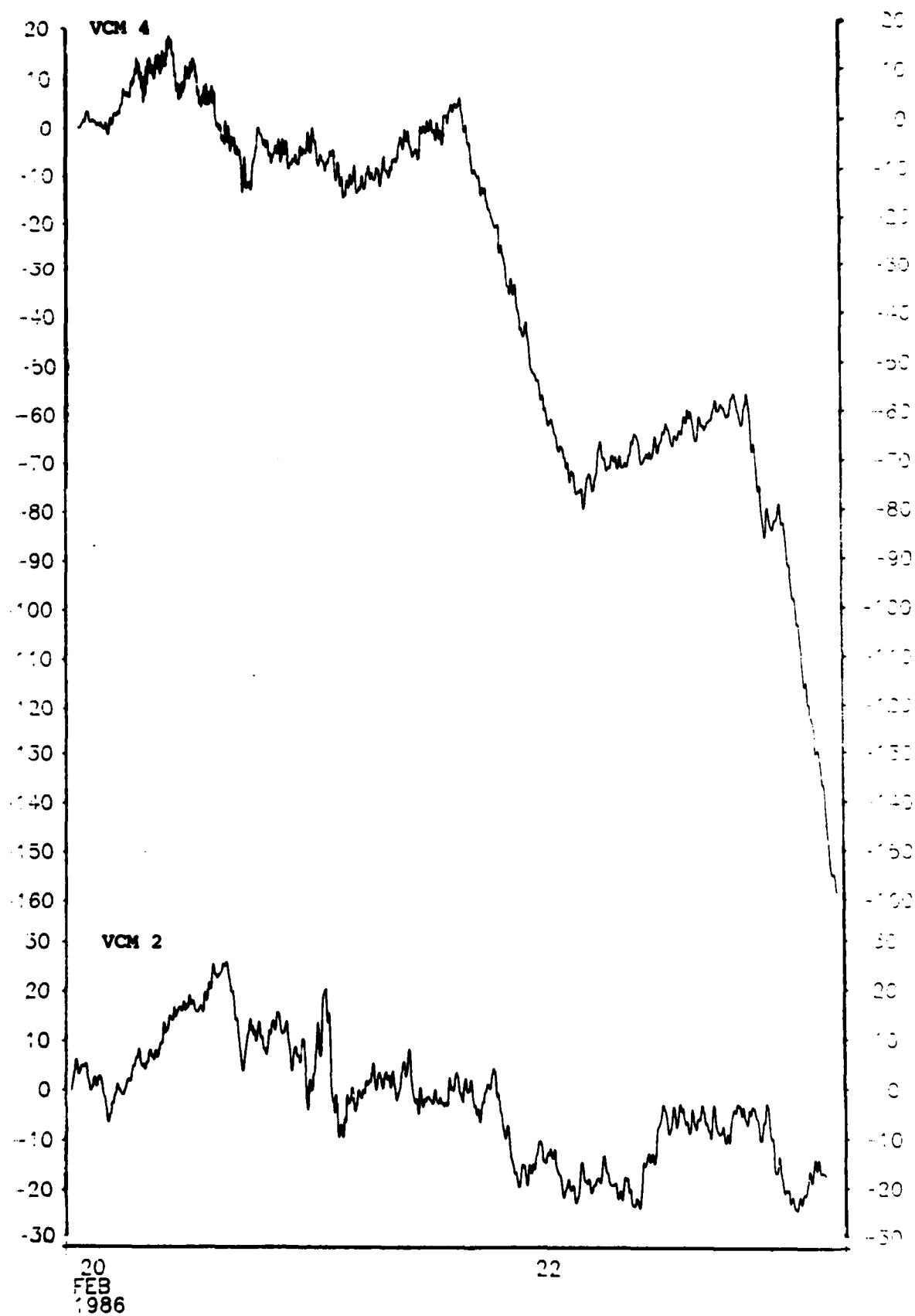


Figure VII-5. Displacement Plots of VCM 2 and 4.

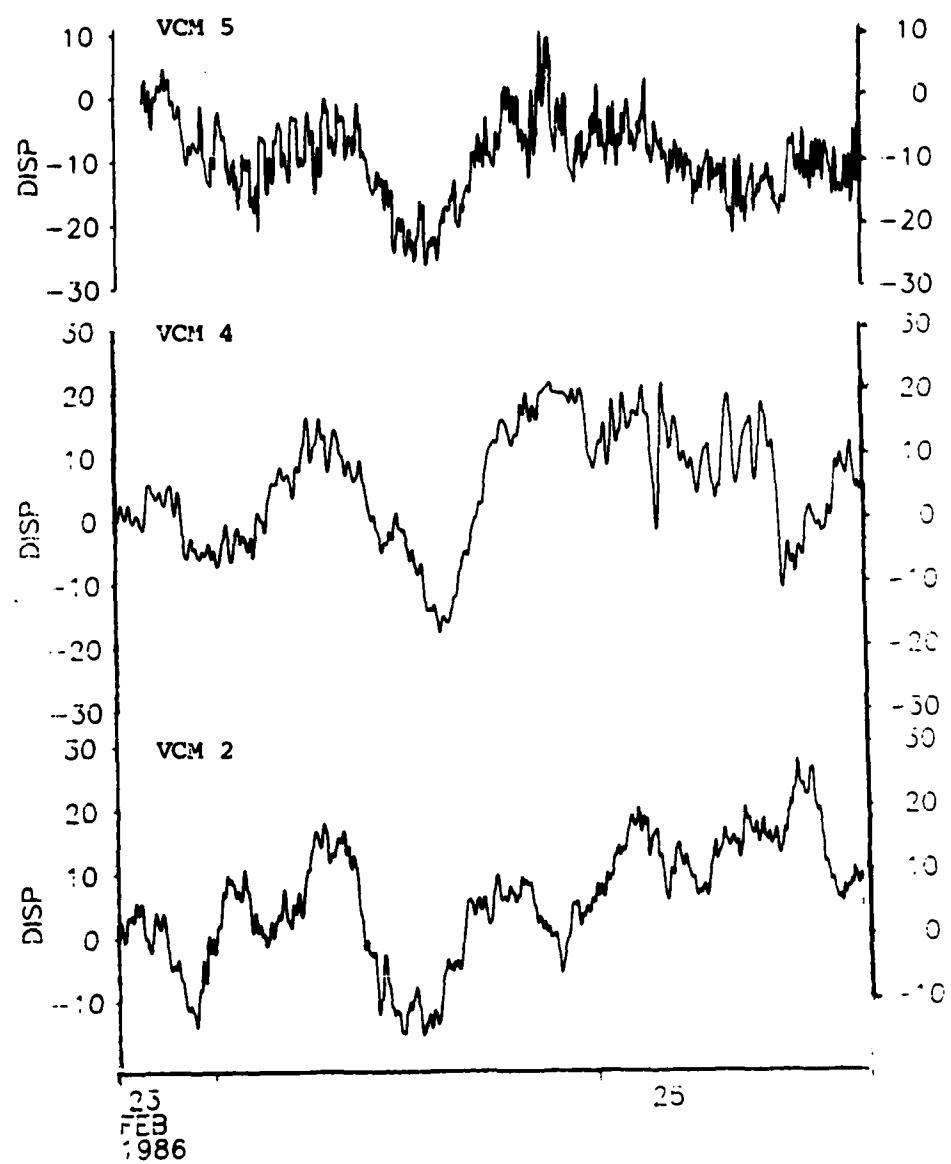


Figure VII-6. Displacement Plots of VCMs 2, 4, and 5.

VIII. Real Time Profiler Data

The RTP directly measures vertical velocities as well as horizontal velocities, temperature, and conductivity. Two velocity sensors, consisting of two cosine-response propellor assemblies are mounted at right angles on the RTP with the axis of rotation of one propeller assembly on each sensor oriented vertically. A fin attached to the pressure case that houses the electronics orients the instrument with respect to the mean flow so that the velocity sensors are upstream of the pressure housing. Two vertically oriented propeller assemblies produce redundant vertical velocity measurements. The two horizontally oriented propeller assemblies measure orthogonal components of velocity, which, together with the heading from the compass in the instrument, can be transformed into the east and north components of horizontal velocity. In addition, the instrument is fitted with an external temperature sensor, a conductivity sensor, a pressure sensor, and two accelerometers that sensed tilt. All other data from the RTP are both recorded internally and transmitted in digital format up the cable every 14 seconds.

An RTP section was completed across a front during Phase Two. The stations consisted of a profile to approximately 300m. Stations one to three were part of an aborted section. Stations four to 17 worked across the front from warm to cold on March 4-5.

Figure VIII-1
Figure VIII-2
Table VIII-1
Figure VIII-3
Figure VIII-4
Figure VIII-5
Figure VIII-6

Schematic of RTP
RTP Station Positions
RTP Station Information
RTP Temperature Sections
RTP Salinity Section
RTP Sigma T Section
3-D Velocity Sticks from Warm and Cold Side of Front

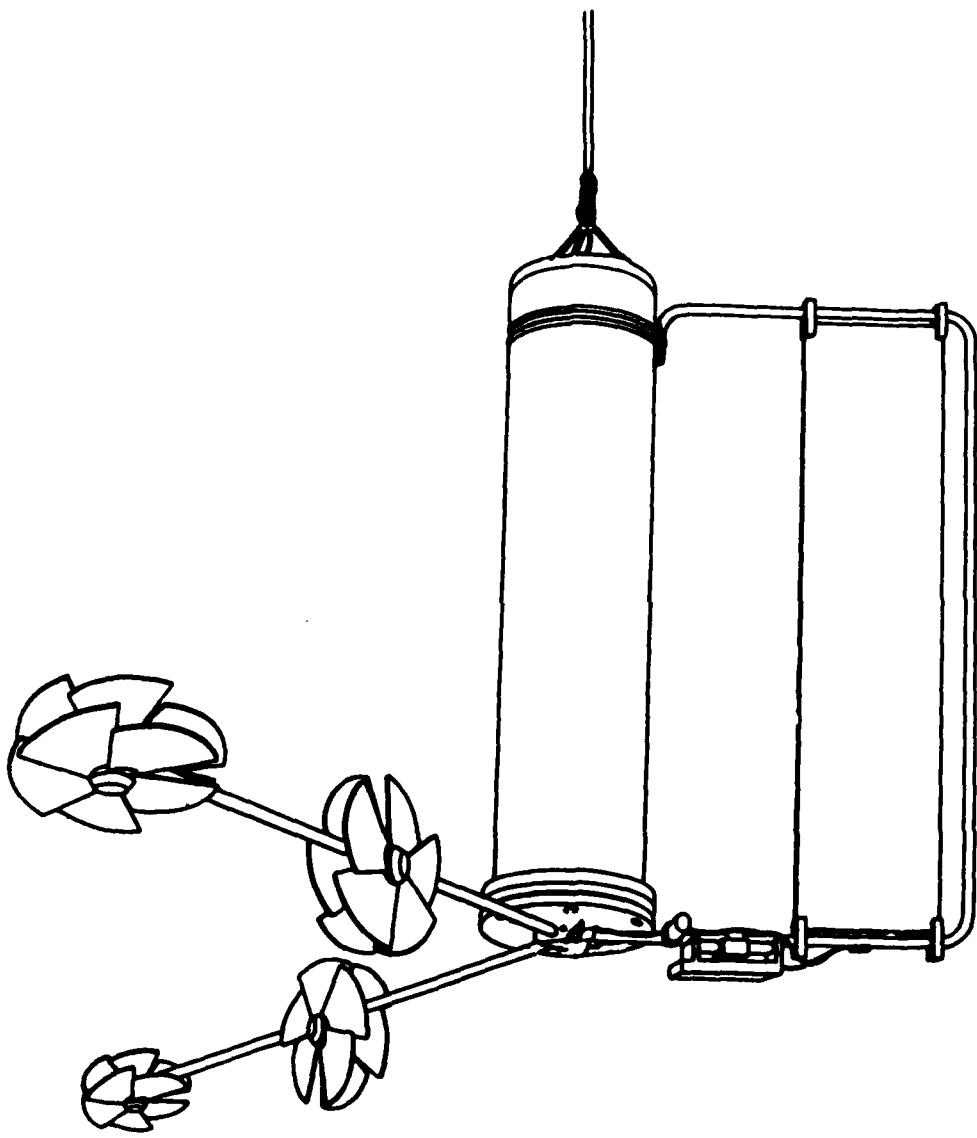


Figure VIII-1: Schematic of RTP.

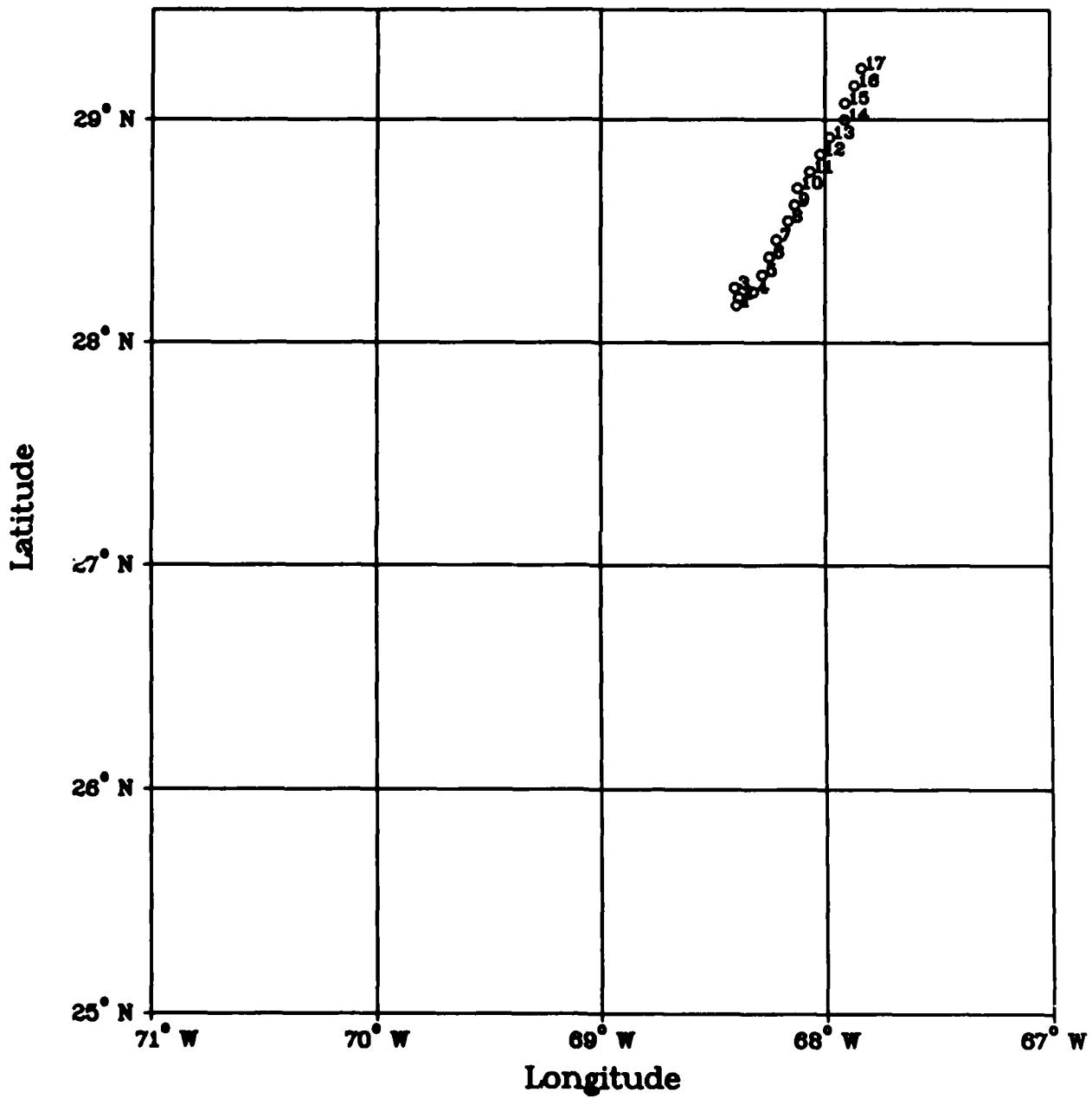
FASINEX Oceanus 175 RTP Stations

Figure VIII-2: RTP Station Positions.

OCEANUS 175 Real Time Profiler (RTP)

Station No.	Start Time (Z)	End Time (Z)	Deployment Latitude	Position Longitude	Retrieval Latitude	Position Longitude	Drop Nos.	Max Depth (m)
1	1106 1 Mar	1242 1 Mar	28°10.06'	68°23.57'	28°12.02'	68°23.09'	1	275
2	1308 1 Mar	1436 1 Mar	28°12.09'	68°23.06'	28°12.16'	68°22.79'	1	295
3	1525 1 Mar	1626 1 Mar	28°14.75'	68°24.18'	28°14.52'	68°23.42'	1	173
4	1439 4 Mar	1607 4 Mar	28°13.64'	68°19.22'	28°13.78'	68°17.59'	1 2	300 20
5	1643 4 Mar	1803 4 Mar	28°18.17'	68°16.80'	28°18.40'	68°15.60'	1	300
6	1842 4 Mar	1958 4 Mar	28°23.02'	68°14.85'	28°23.60'	68°13.73'	1	300
7	2034 4 Mar	2143 4 Mar	28°27.61'	68°12.90'	28°28.51'	68°11.99'	1	300
8	2233 4 Mar	2348 4 Mar	28°32.67'	68°09.92'	28°33.37'	68°08.22'	1	300
9	0022 5 Mar	0207 5 Mar	28°37.00'	68°08.15'	28°36.55'	68°06.57'	1	300
10	0205 5 Mar	0417 5 Mar	28°41.52'	68°07.33'	28°41.59'	68°06.49'	1	300
11	0503 5 Mar	0602 5 Mar	28°45.94'	68°03.97'	28°46.27'	68°03.93'	1	300
12	0659 5 Mar	0815 5 Mar	28°50.66'	68°01.17'	28°50.56'	68°00.27'	1	300
13	0920 5 Mar	1055 5 Mar	28°55.22'	67°58.82'	28°54.18'	67°55.28'	1	300
14	1149 5 Mar	1316 5 Mar	29°00.06'	67°54.74'	28°59.05'	67°54.78'	1	293
15	1539 5 Mar	1638 5 Mar	29°04.58'	67°54.64'	29°04.09'	67°53.49'	1	250
16	1726 5 Mar	1839 5 Mar	29°09.34'	67°52.10'	29°08.68'	67°51.53'	1	300
17	1926 5 Mar	2047 5 Mar	29°14.08'	67°50.29'	29°13.71'	67°50.44'	1	300

Table VIII-1: RTP Station Information.

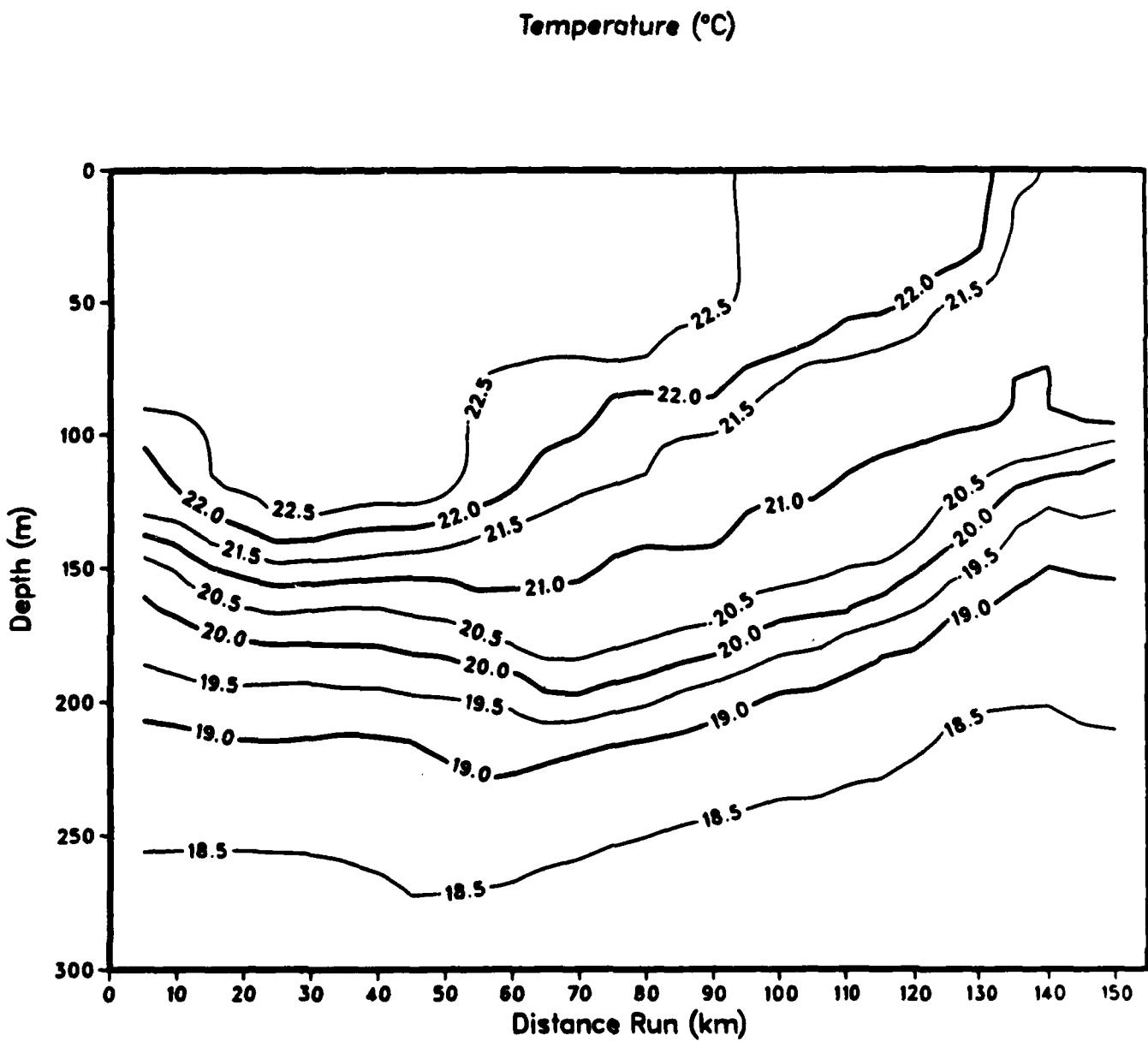


Figure VIII-3: RTP Temperature Sections.

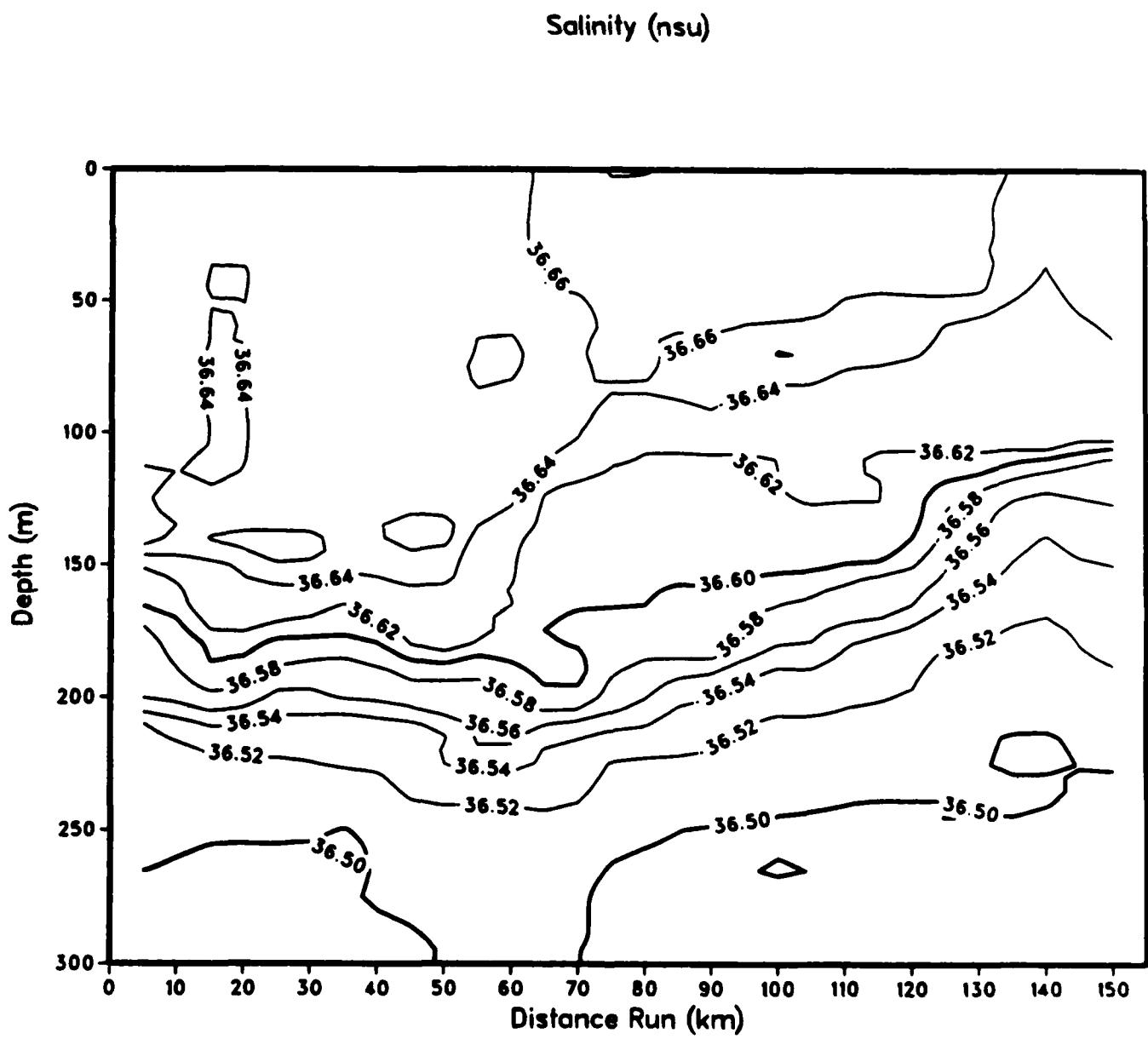


Figure VIII-4: RTP Salinity Section.

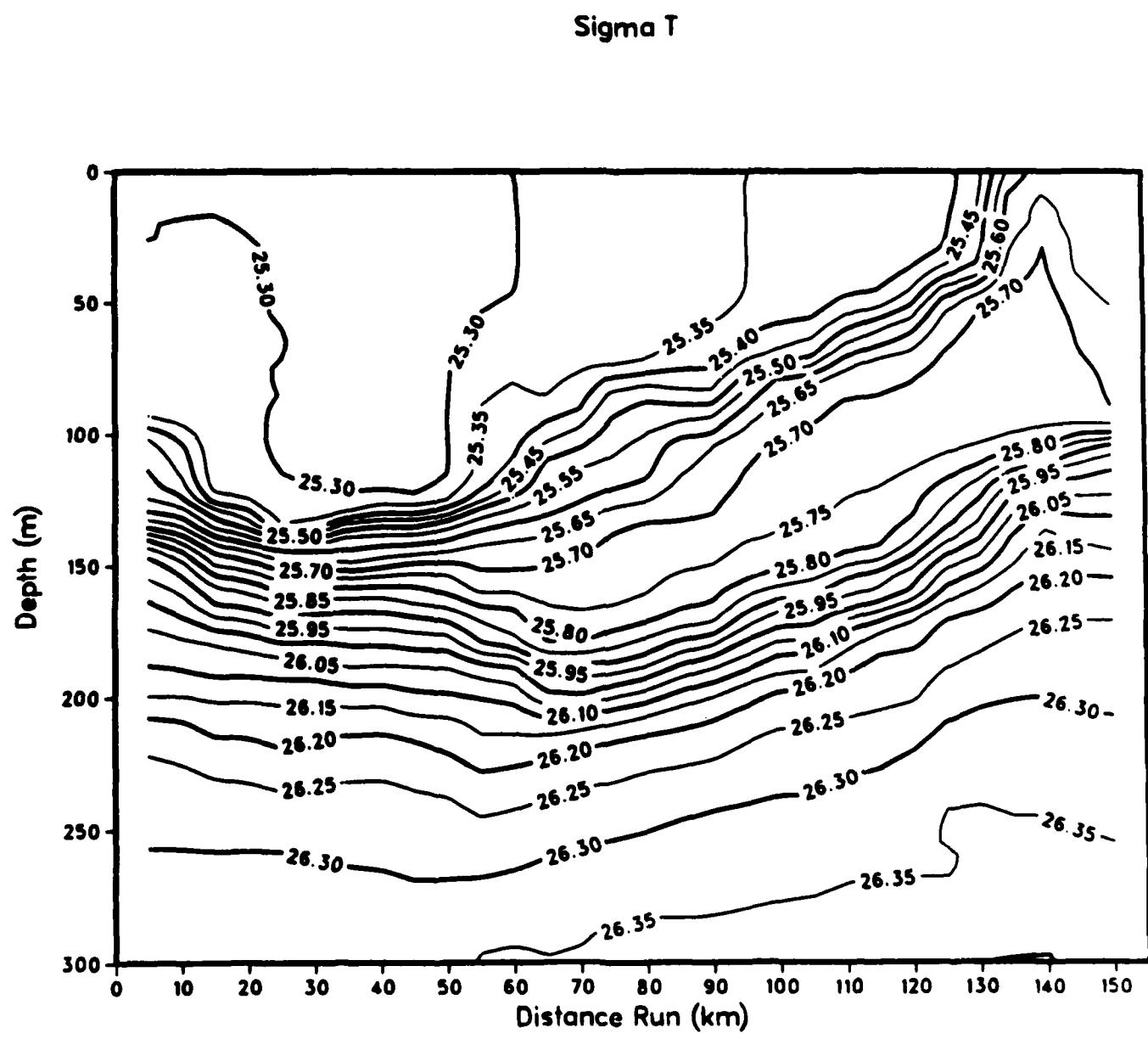


Figure VIII-5: RTP Sigma T Section.

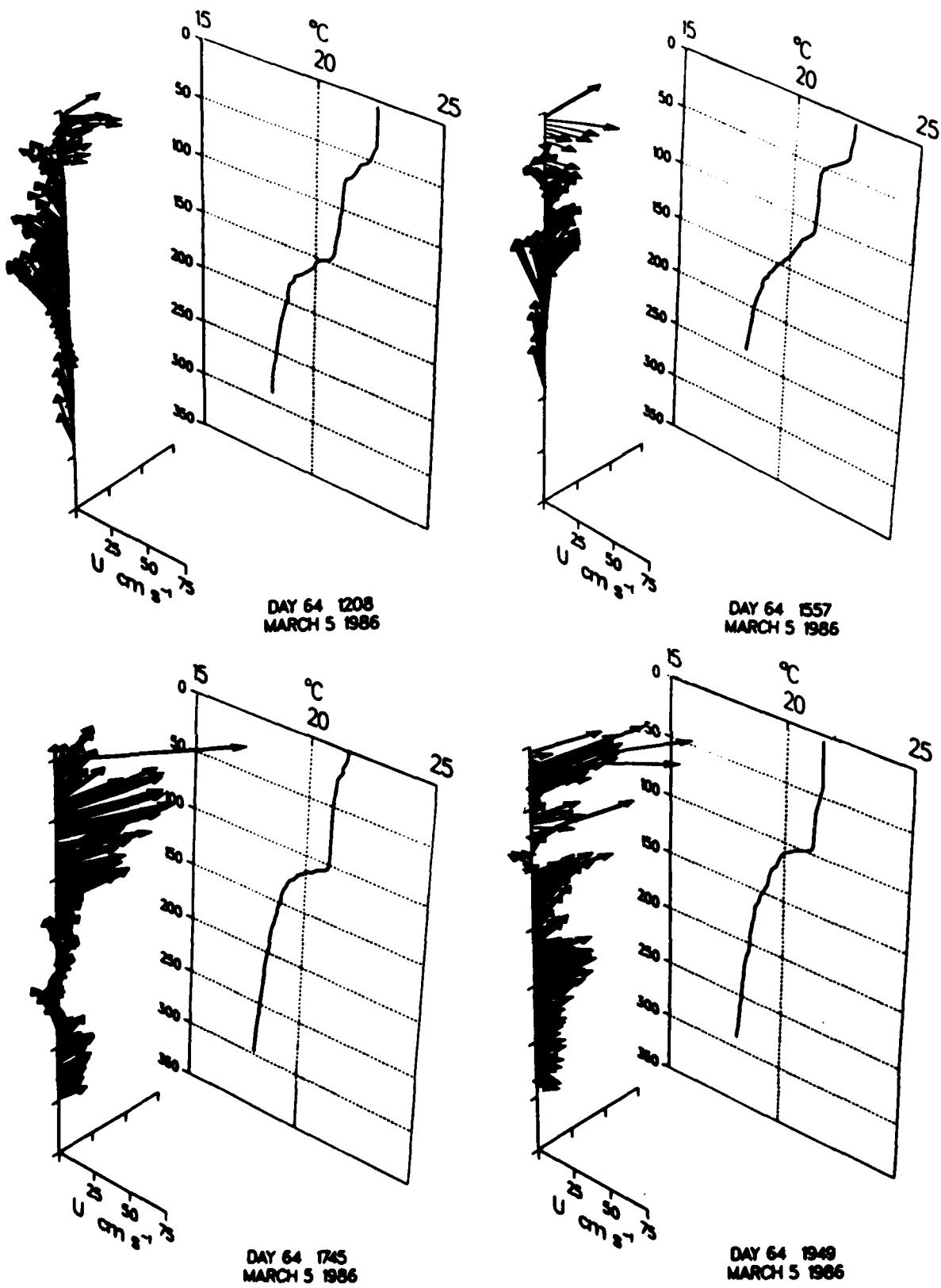


Figure VIII-6: 3-D Velocity Sticks from Warm and Cold Side of Front.

IX. SeaSoar

Towed SeaSoar sections in FASINEX

The Institute of Oceanographic Science's SeaSoar, with faired cable, shallow Neil Brown Instrument Systems CTD instruments, and full NERC shipboard computing facilities was used on R.V. OCEANUS during FASINEX Phase Two. With CTD casts to over 350m at 1 to 2 Km intervals while underway at 8-9 knots, close spaced CTD sections were obtained along and across fronts. The data were calibrated, corrected, plotted and contoured on board ship to provide smoothed (reduced internal wave noise) sections with a few km resolution of temperature, salinity, density and hence pressure gradients and geostrophic velocity shear, within hours of data collection. Temperature/salinity diagrams were used to identify water masses, origins and mixing rates.

SeaSoar specification and capabilities

The SeaSoar (Figure IX-1) is a modified version of the Canadian Batfish (Dessureault, 1976), enlarged to carry a Neil Brown Instrument Systems CTD. The adjustable wings are hydraulically powered by a propellor at the back of the vehicle. A ship speed greater than 5 knots is needed to develop full power. At lower speeds, wing response is sluggish and depth control consequently poor. A speed of 8-9 knots is optimal. Ten knots is possible, but increasing cable tensions reduce the maximum depth and cycling rate.

In automatic mode, the deck unit generates a sawtooth pressure signal (with operator set minimum and maximum depths, rate of ascent and rate of descent). A servo-control compares the CTD pressure signal with the sawtooth function and adjusts the wing angle to match the two. Deviations from a straight line during ascent or descent are generally less than 2 dbar.

Maximum ascent and descent angles are about 1:5 (much greater than frontal slopes of order 1:50 or less). With 600 m of Fathom faired cable, a maximum depth of over 360 m is attainable, giving a horizontal distance between minimum depths of about 3 Km, i.e. a profile (up or down) on average every 1.5 Km. These separations can be reduced by reducing the depth range.

Shipboard data analysis allows profiles and contoured sections to be produced within 3 to 6 hours of data collection.

A data report summarizing the SeaSoar participation is available. It is FASINEX Technical Report #11, SeaSoar CTD Surveys during FASINEX.

Reference IOS Technical Report: Pollard, R.T., Read, J.F. & Smithers, J. 1986
 SeaSoar CTD Surveys during FASINEX.
 Institute of Oceanographic Sciences,
 Report, No. 230, 111pp.

- | | |
|-------------|--|
| Figure IX-1 | SeaSoar Schematic |
| Figure IX-2 | SeaSoar Mooring Survey #1 February 13-18 |
| Figure IX-3 | SeaSoar Radiator Pattern February 18-20 |
| Figure IX-4 | SeaSoar Box Patterns February 25-March 4 |
| Figure IX-5 | SeaSoar Mooring Survey #3 March 6-8 |

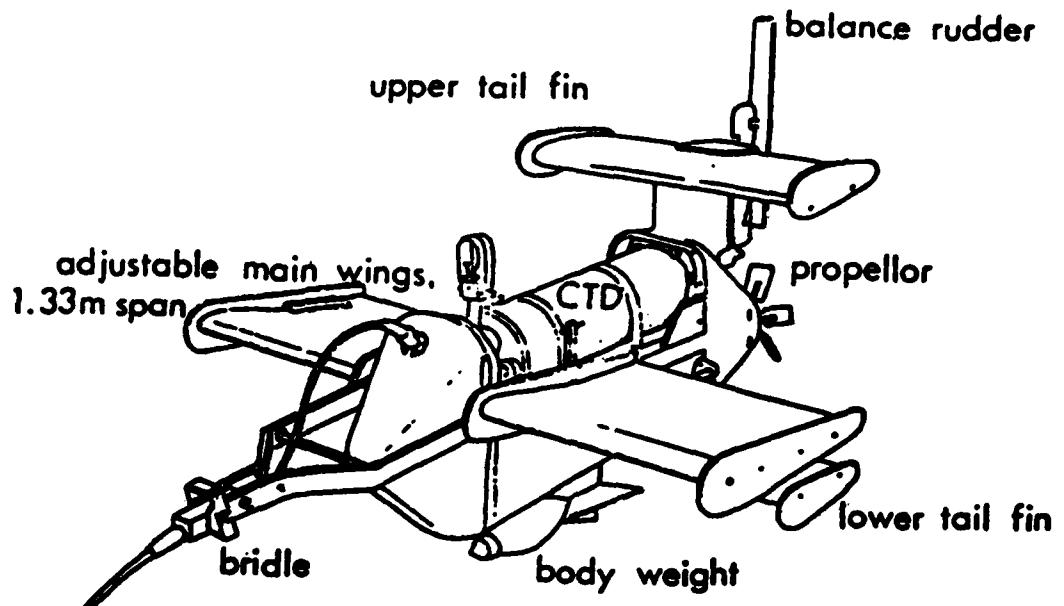


Figure IX-1: SeaSoar Schematic.

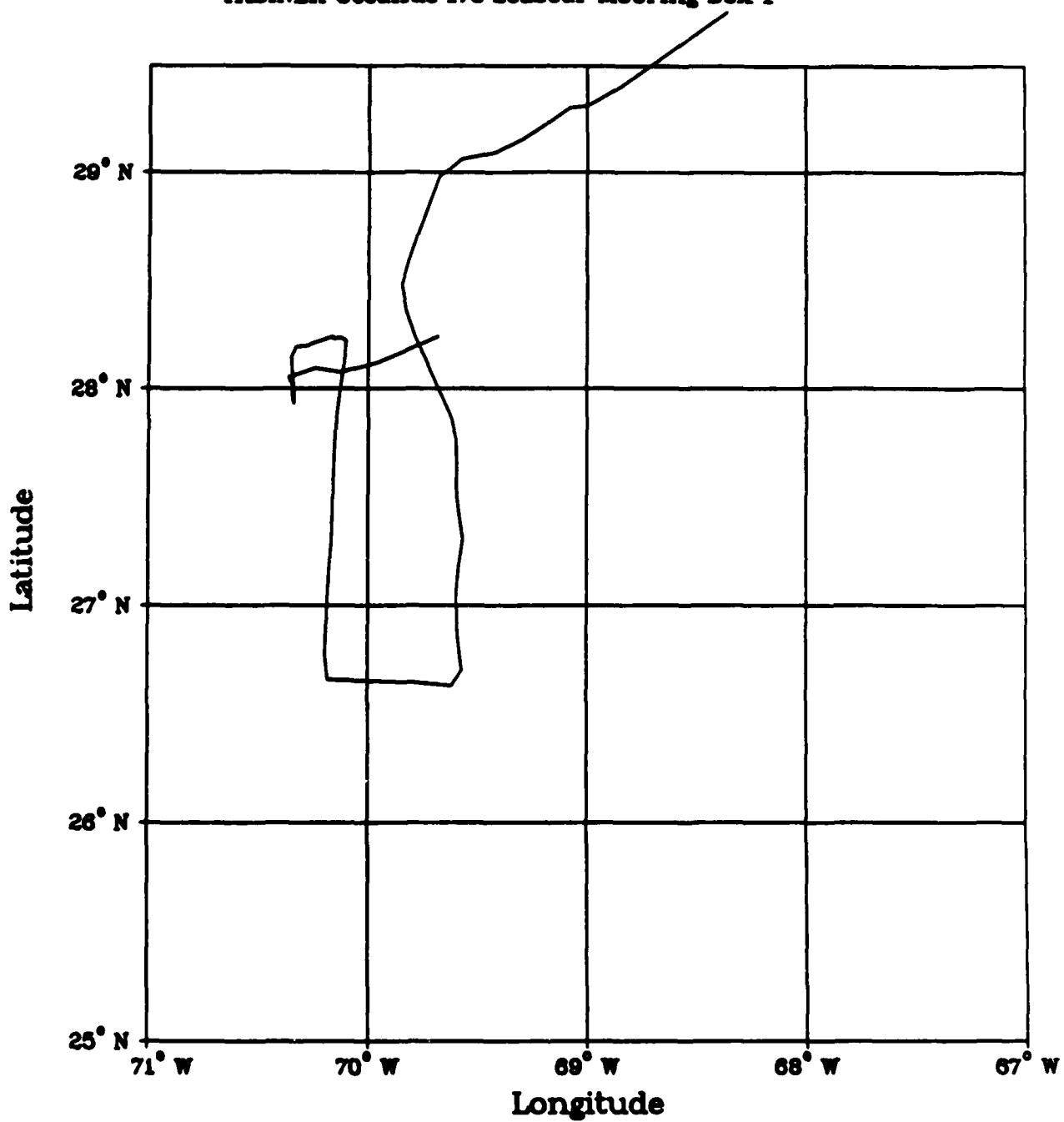
FASINEX Oceanus 175 SeaSoar Mooring Box 1

Figure IX-2: SeaSoar Mooring Survey #1 February 13-18.

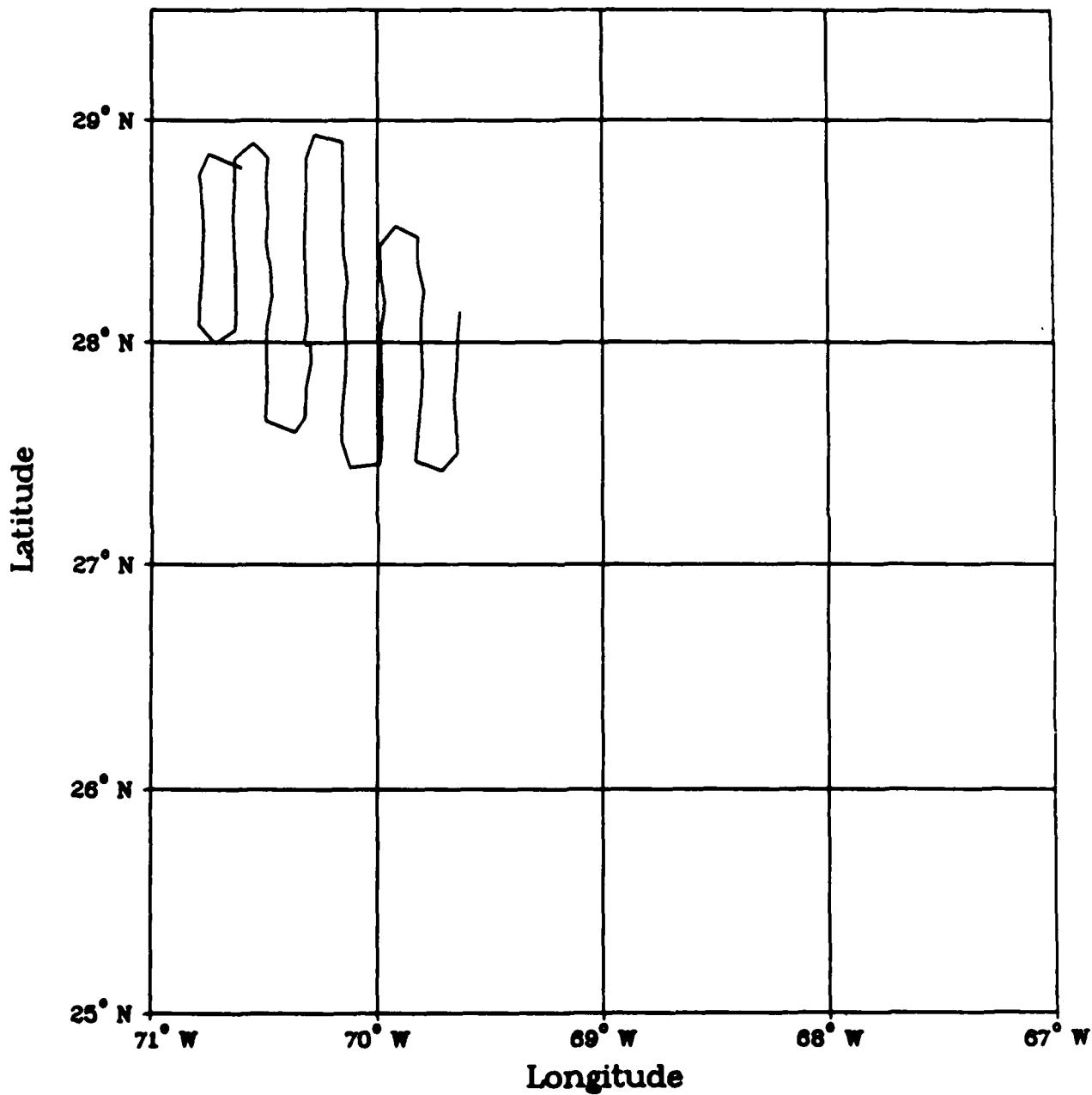
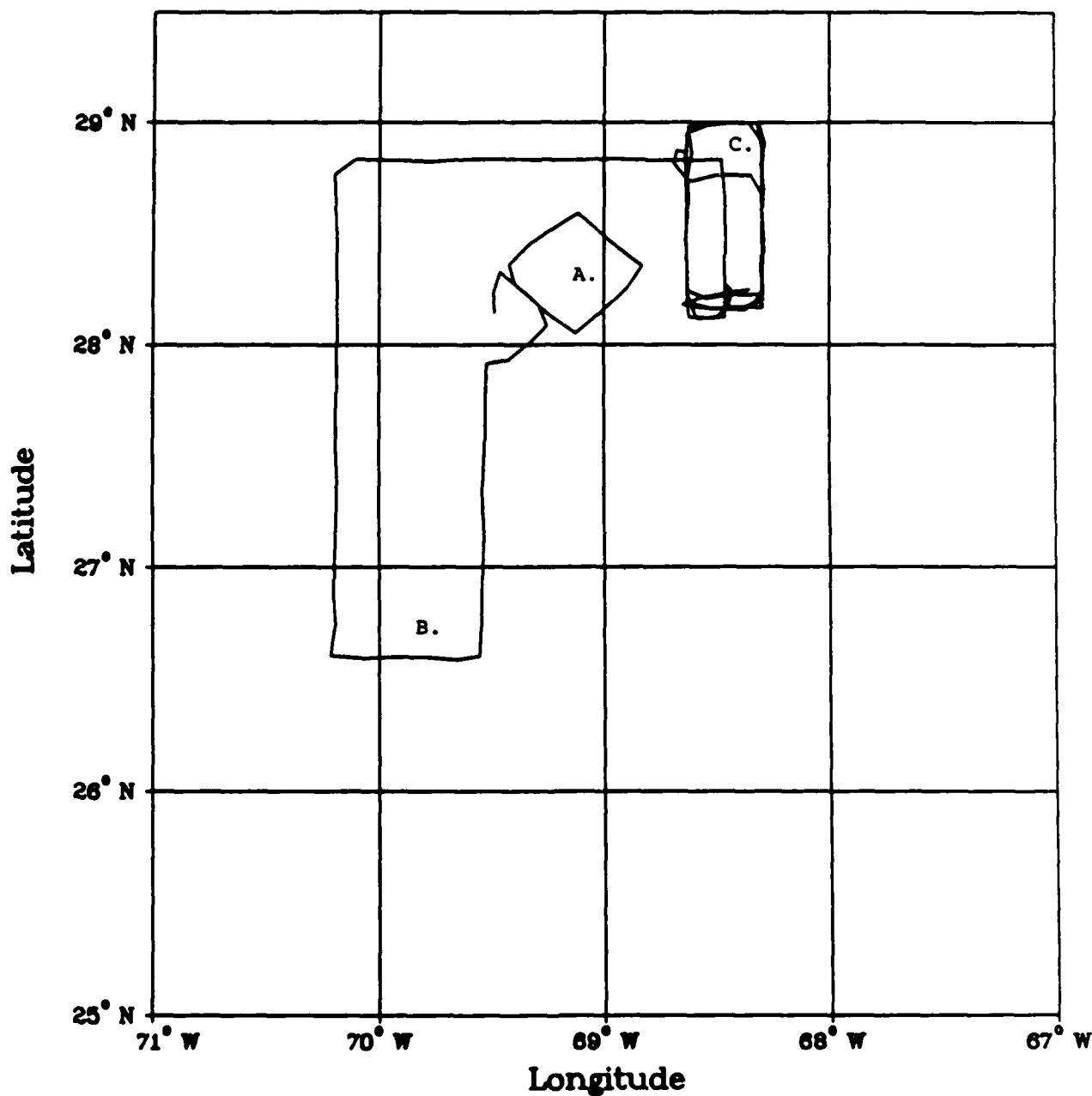
FASINEX Oceanus 175 SeaSoar Radiator

Figure IX-3: SeaSoar Radiator Pattern February 18-20.

FASINEX Oceanus 175 SeaSoar Boxes

- A. Aborted Pattern due to rough seas
- B. Mooring Box 2
- C. Boxing in front found March 2-3

Figure IX-4: SeaSoar Box Patterns February 25-March 4.

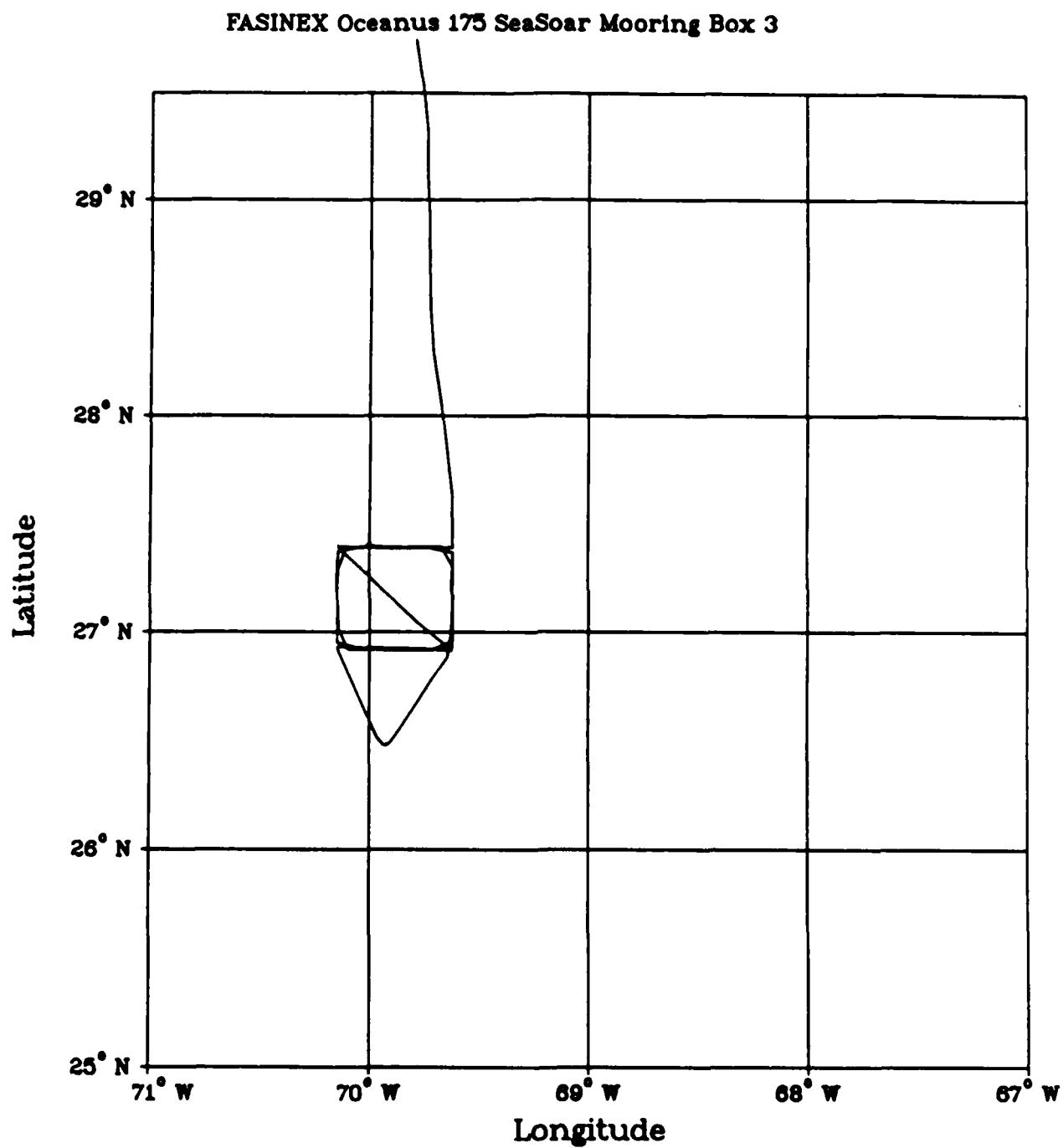


Figure IX-5: SeaSoar Mooring Survey #3 March 6-8.

Participant Summary:**X. Doppler Acoustic Current Profiles**
Lloyd Regier

The Doppler current profiler on OCEANUS operated nearly continuously throughout FASINEX. Reliable data returns were obtained from 20 meters depth to about 200 meters throughout the experiment. Due to equipment failures and operator errors there are several time gaps in the data.

14 Feb 1257Z
04 Mar 0033
05 Mar 0222
0559
1119
06 Mar 1959
2058
11 Mar 1145

We have yet to edit the LORAN-C fixes and are thus unable to compute the current profiles relative to the earth. A crude estimate of the ship velocity relative to the earth may be obtained from a vertical average of the profiles of water velocity relative to the ship. Plots of currents relative to this average will have the same vertical structure as that of currents measured relative to the earth but will not accurately reveal the horizontal structure of the currents. The horizontal shears of currents can only be obtained from the true currents relative to the earth.

The contour map shows the behavior versus depth and along-track distance of the North and East components of current in cm/sec relative to the vertical averaged discussed above. The plot covers 400 kilometers of ship track and shows currents from 20 to 200 meters depth. The along-track distance is in kilometers traveled through the water; the ship odometer is reset to zero at each of the data gaps shown above. The vertical lines show the along-track ship position at each hour; each line is labeled with the day-of-year and GMT time. Also shown are the ship's heading and water temperature at 5 meters depth as functions of along-track distances.

Figure X-1 Total Ships Track of OC 175 - Doppler Data
Figure X-2 Doppler Section Feb 16 1300 - Feb 17 1800
Figure X-3 Position of 400 Kilometer Section

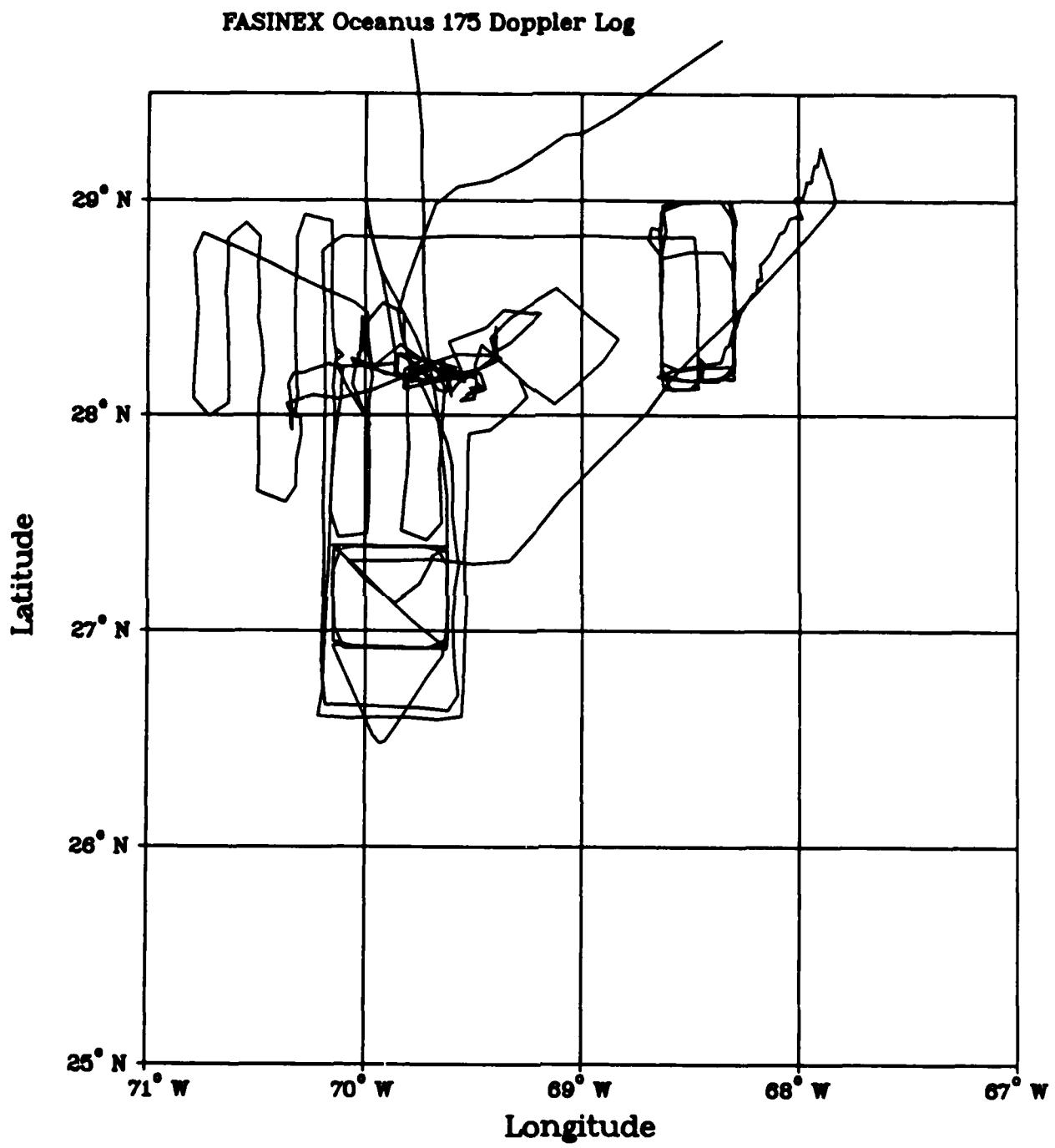


Figure X-1: Total Ships Track of OC 175 - Doppler Data.

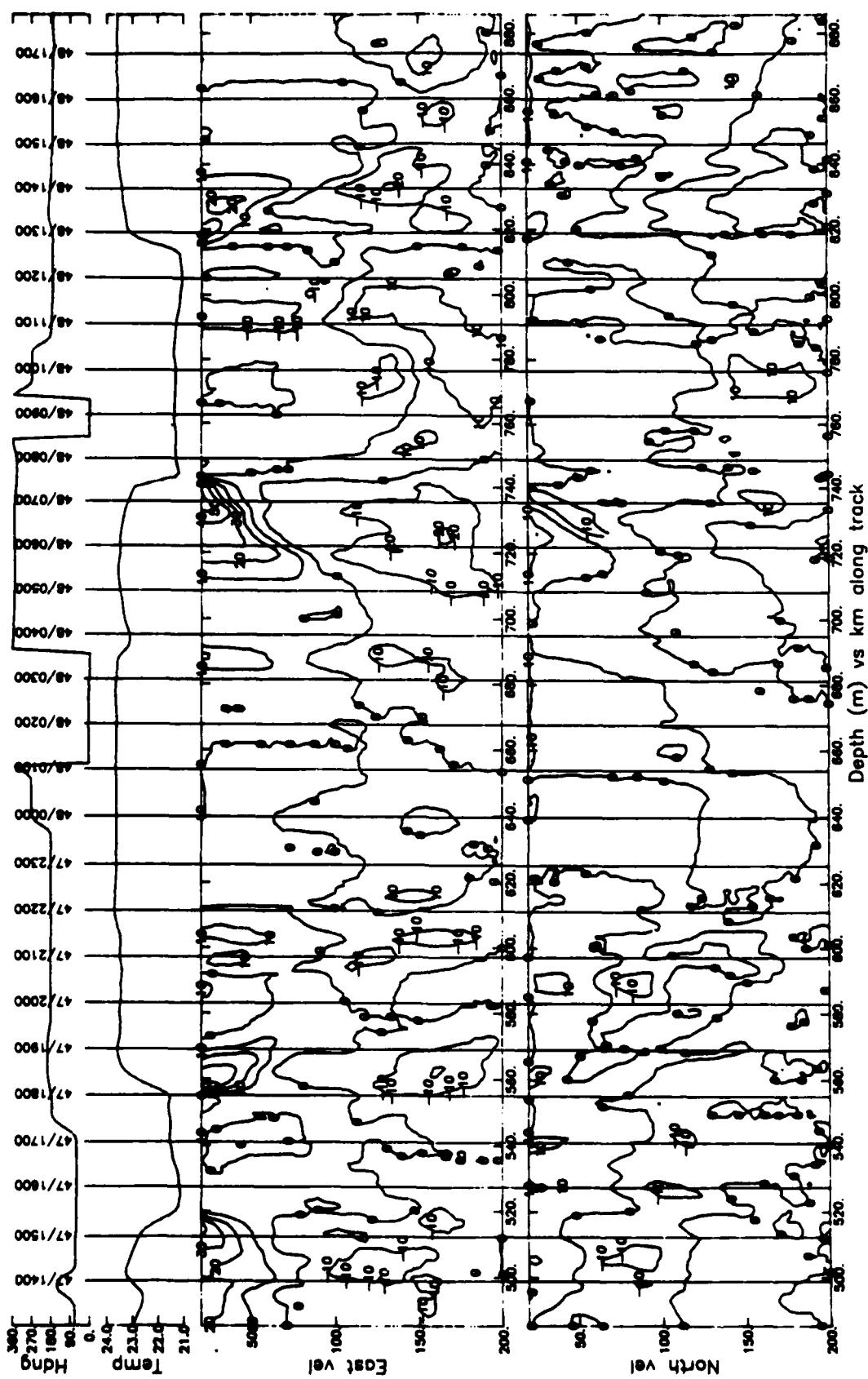


Figure X-2. Doppler Section February 16 1300 - February 17 1800.

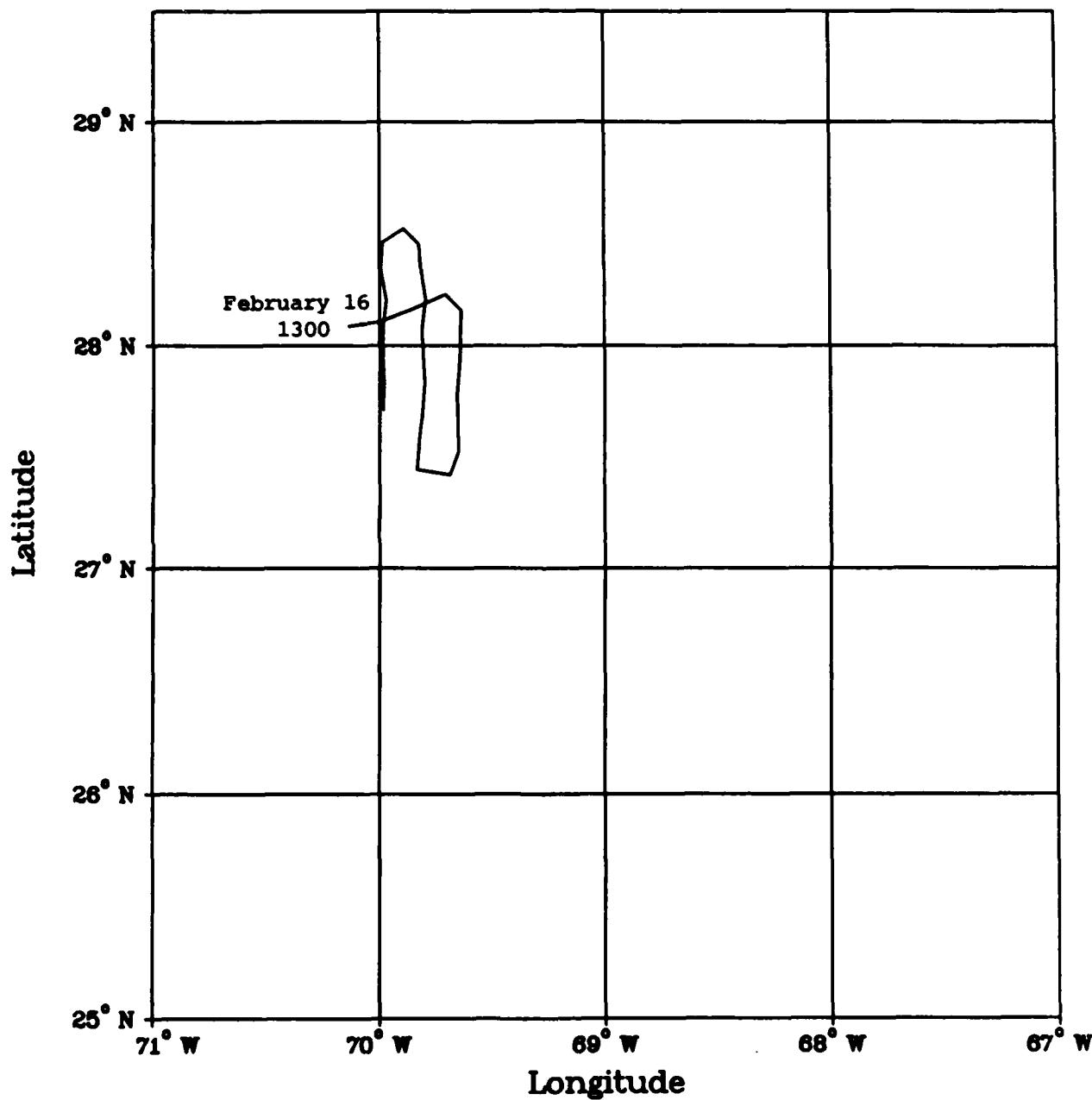
FASINEX Oceanus 175 Doppler Section

Figure X-3: Position of 400 Kilometer Section.

Participant Summary:**XI. Lagrangian Drifters Deployed from R. V. OCEANUS**
Lloyd Regier and Russ Davis

Radio-tracked drifters were deployed from OCEANUS in three groups. Each group consisted of eight drifters, four drogued at 1 meter depth and four at 50 meters. The buoys were deployed in pairs, one deep and one shallow, with two pairs on either side of the front. Each buoy measured water temperature at a depth of 1 meter. The accompanying figures show the observed trajectories of those buoys which were trackable. Arrows show the direction of motion away from the deployment position. "D" denotes a 50 meter drogue and "S" denotes a 1 meter surface drifter. The year-day and GMT time of launch and final positions are shown on the trajectory plots. The reduction of the temperature data is ongoing.

- Figure XI-1 SIO Drifter Deployments on Expanded scale chart**
Figure XI-2 SIO Drifter Deployment #1
Figure XI-3 SIO Drifter Deployment #2
Figure XI-4 SIO Drifter Deployment #3

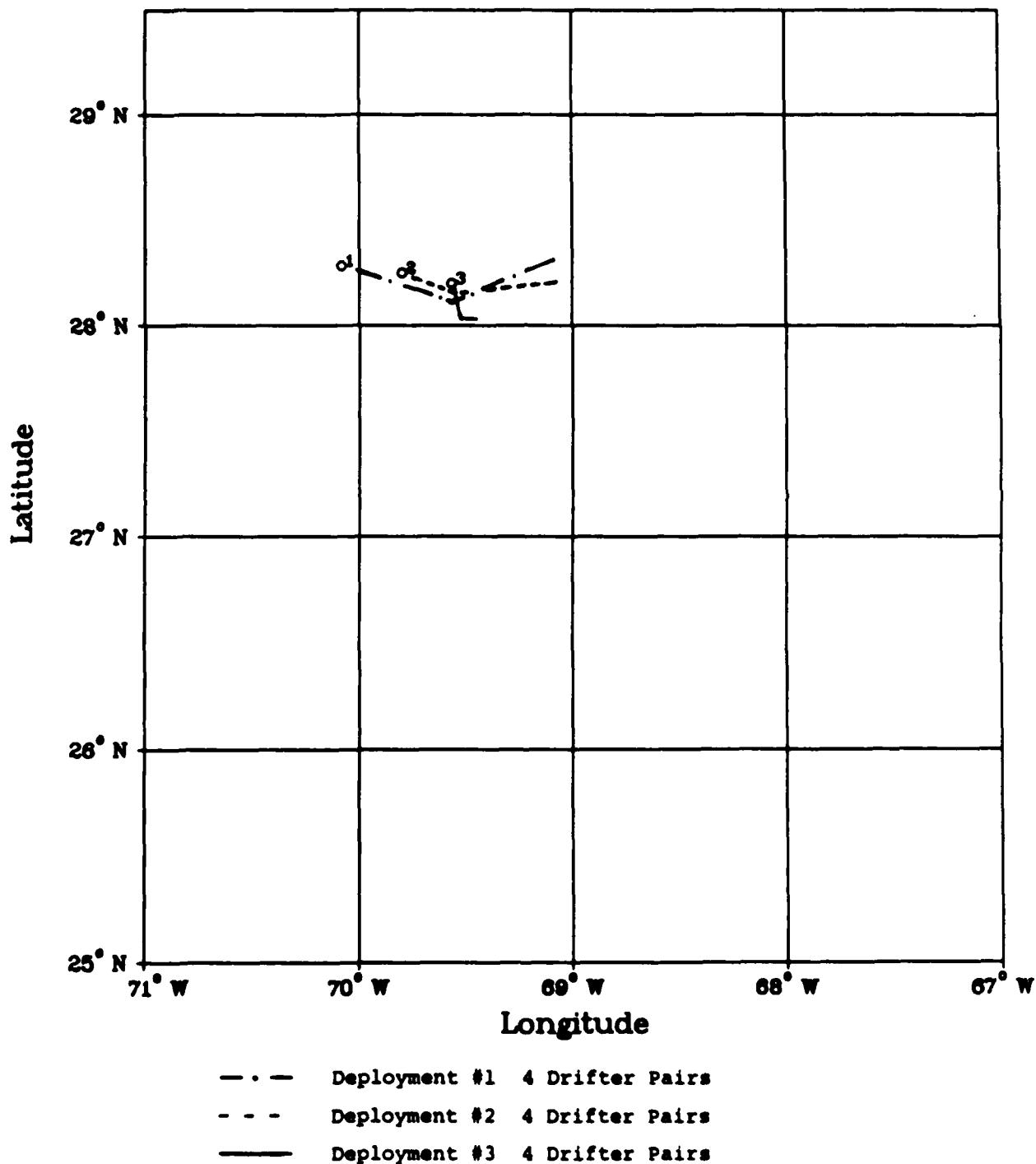
FASINEX Oceanus 175 SIO Drifters

Figure XI-1: SIO Drifter Deployments on Expanded Scale Chart.

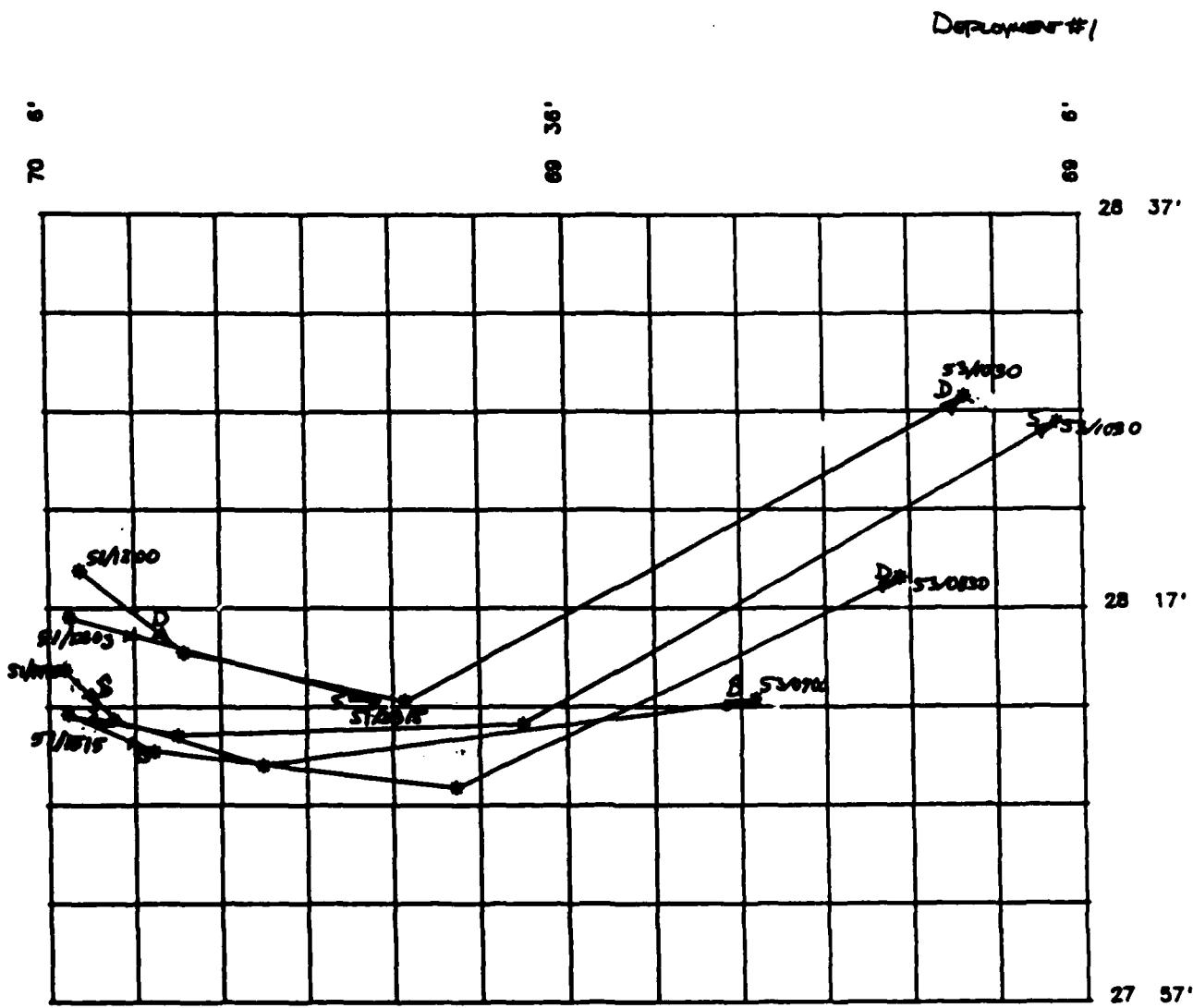


Figure XI-2. SIO Drifter Deployment #1.

DEPLOYMENT #2

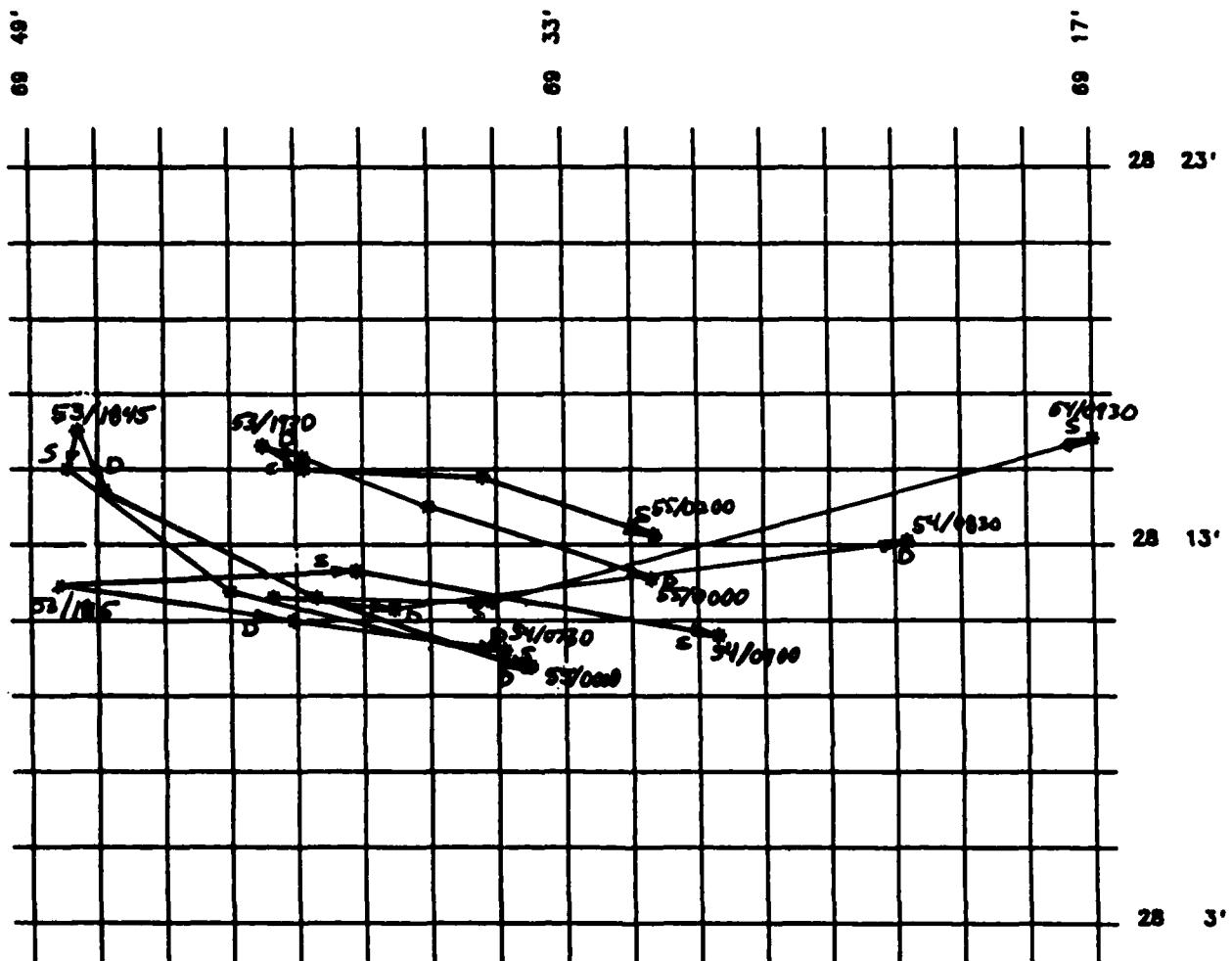


Figure XI-3. SIO Drifter Deployment #2.

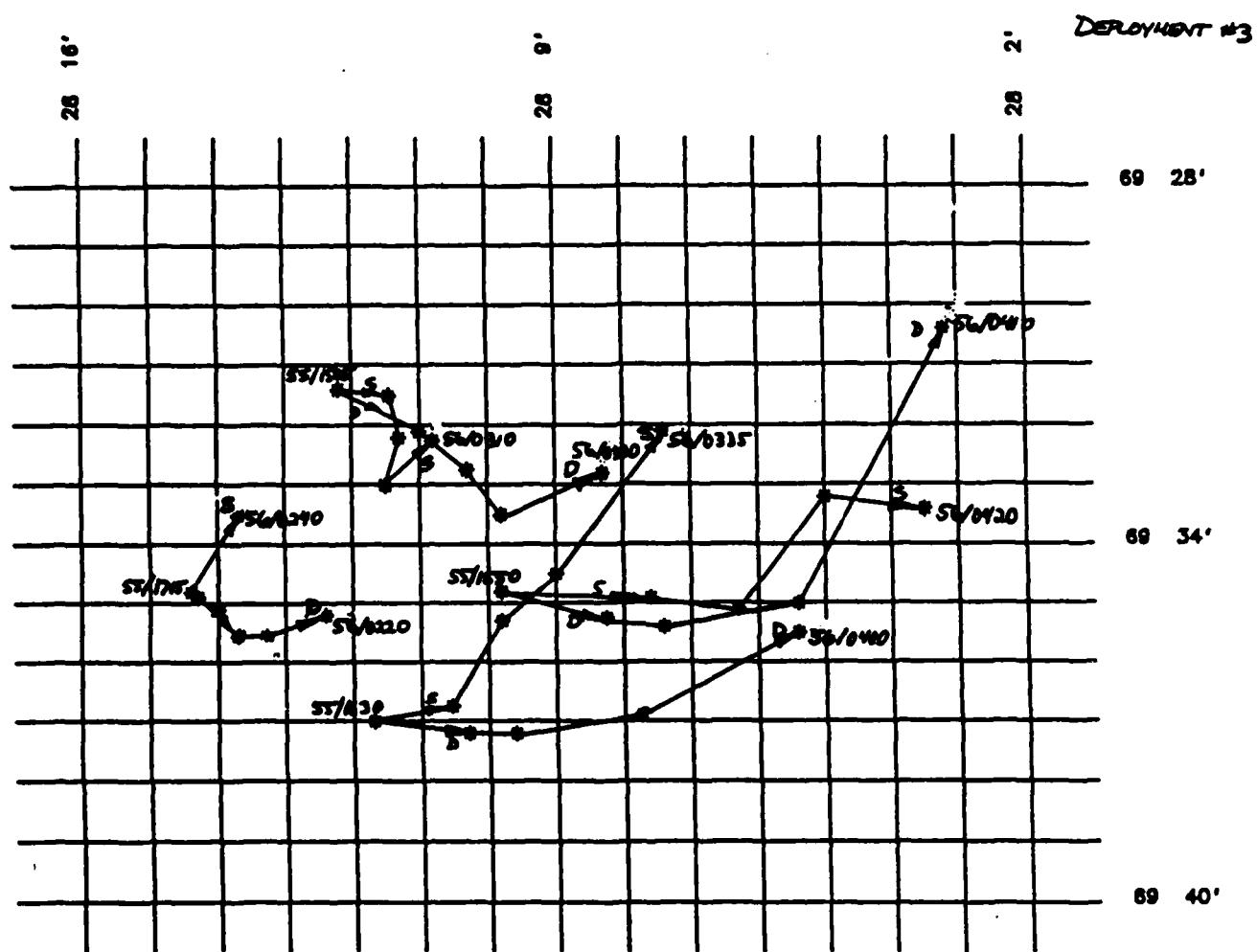


Figure XI-4. SIO Drifter Deployment #3.

Participant Summary:**XII. Shipboard Marine Radar Estimates of Wind Stress and Momentum Flux during FASINEX**
Dennis B. Trizna**OBJECTIVES:**

The objectives of our FASINEX participation are: (1) to better understand the scattering mechanisms responsible for low grazing angle sea scatter statistics by comparison with high quality in-situ measurements of wind stress and momentum flux; (2) to determine the effects on the marine radar sea scatter due to the sea surface temperature change associated with the thermal front, in concert with similar measurements made by the airborne active and passive remote sensors; (3) to develop empirical relationships between radar sea scatter statistics and the individual contributions to momentum flux which have been hypothesized based upon previous preliminary experiments.

In the FASINEX experiment, we are utilizing the marine radars on board the participating ships, the KNORR and the OCEANUS, for the measurement of low grazing angle sea scatter. Based upon previous measurements made aboard NOAA ships, a correlation was shown to exist between parameters of the cumulative distribution function of the normalized sea surface radar cross section (NRCS) and wind and wave conditions. This type of measurement appears to distinguish between sources of scatter due to small scale surface features generated by the wind, such as capillary waves, and more robust surface features generated by wave-wave interactions, such as breaking waves.

PRELIMINARY RESULTS:

Although some hardware difficulties were encountered on board the KNORR during the second leg of deployment of the buoy array, a sizable amount of X- and S-band radar data was successfully deployed aboard the OCEANUS and X-band data were collected for the entire cruise, resulting in 648 hourly files of data. In addition, photographs of the sea surface were taken by the met watch during daylight hours, from which white-cap coverage will be extracted. Professor Edward Monahan, University of Connecticut, has been contracted to analyze these data under internal NRL 6.1 core funds which recently came available.

First-pass processing of radar data statistics has been accomplished, producing azimuthal angle distributions of mean radar sea echo power levels. An example of such an azimuthal distribution is shown in Figure XII-1. A wide variety of angular widths of the mean echo distribution was observed, presumably associated with variation in the directional ocean wave spectrum angular spread.

Time histories of peak mean radar echo and direction from consecutive hourly angular distributions were also determined, as a preliminary catalogue of the data. Temporal variation of the echo with time, assumed to be

associated with wind speed variation, is quite dramatic, with a response faster than we had anticipated, indicating rapid rises in sea echo levels shorter than the hourly collections employed. Plots of peak mean signal power received and direction of the maximum radar return for two different 36-hour periods of time from aboard the OCEANUS are shown in Figure XII-2. Although these first-look results appear promising, radar calibration remains to be done before data analysis can proceed, currently scheduled for June. In addition, surface truth of sea surface temperature must be available before calibration of radar returns with the front can be made.

The second aspect of the experiment, the imaging of the ocean waves using a different data acquisition system, had a hardware failure several days into the KNORR cruise, allowing just three images to be collected. However, of the three images collected aboard the KNORR, one shows unusual sea echo distributions in range and azimuth. This image was presumably collected in the vicinity of the front, because of the observed spatial inhomogeneity. Final correlation will depend upon surface truth records from the KNORR.

Radar Propagation Staff, Radar Division
Naval Research Laboratory - Code 5303
Washington, D. C. 20375
(202) 767-2003

Figure XII-1 Azimuthal Angle Distribution
Figure XII-2 Peak Mean Signal Power Received and Direction of Maximum Return

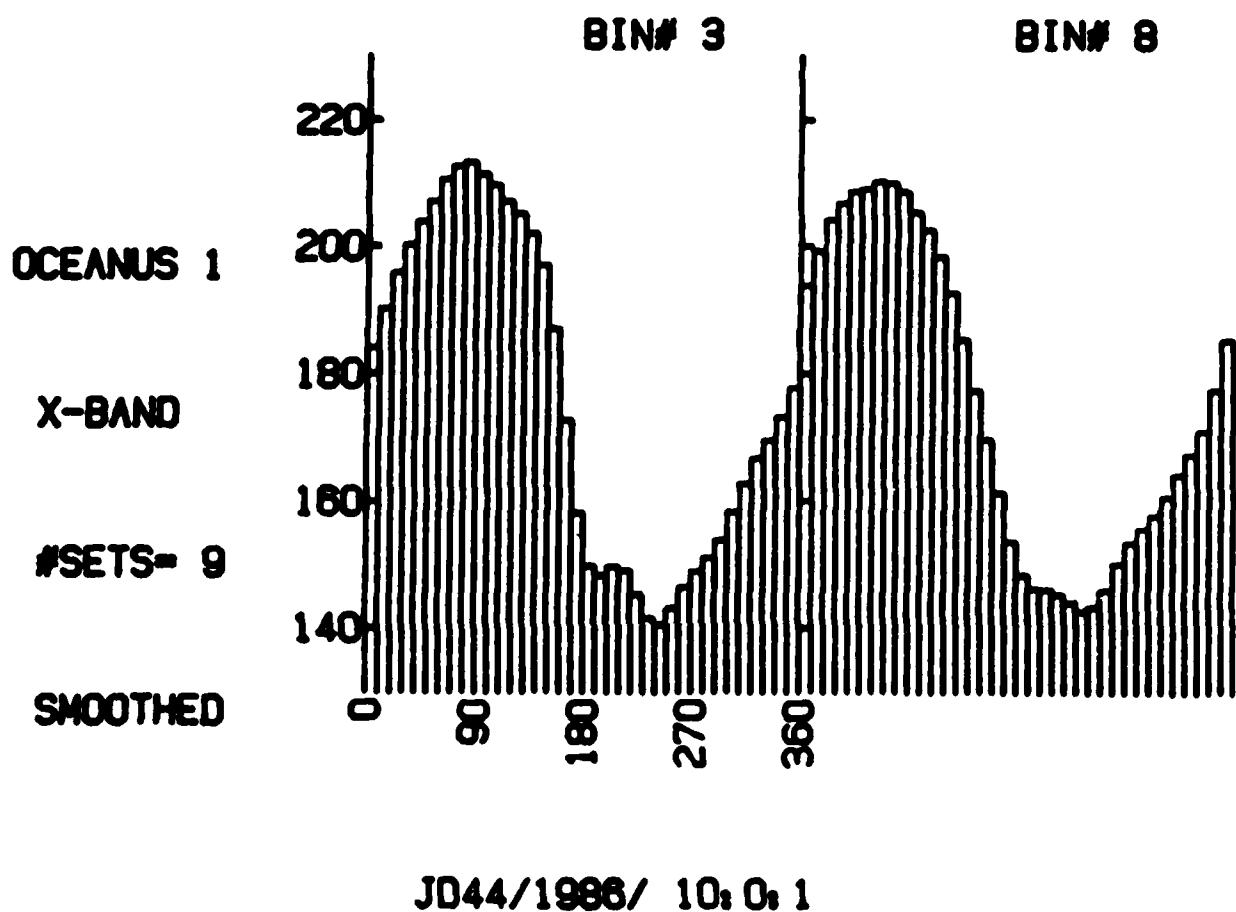


Figure XII-1: Azimuthal Angle Distribution.

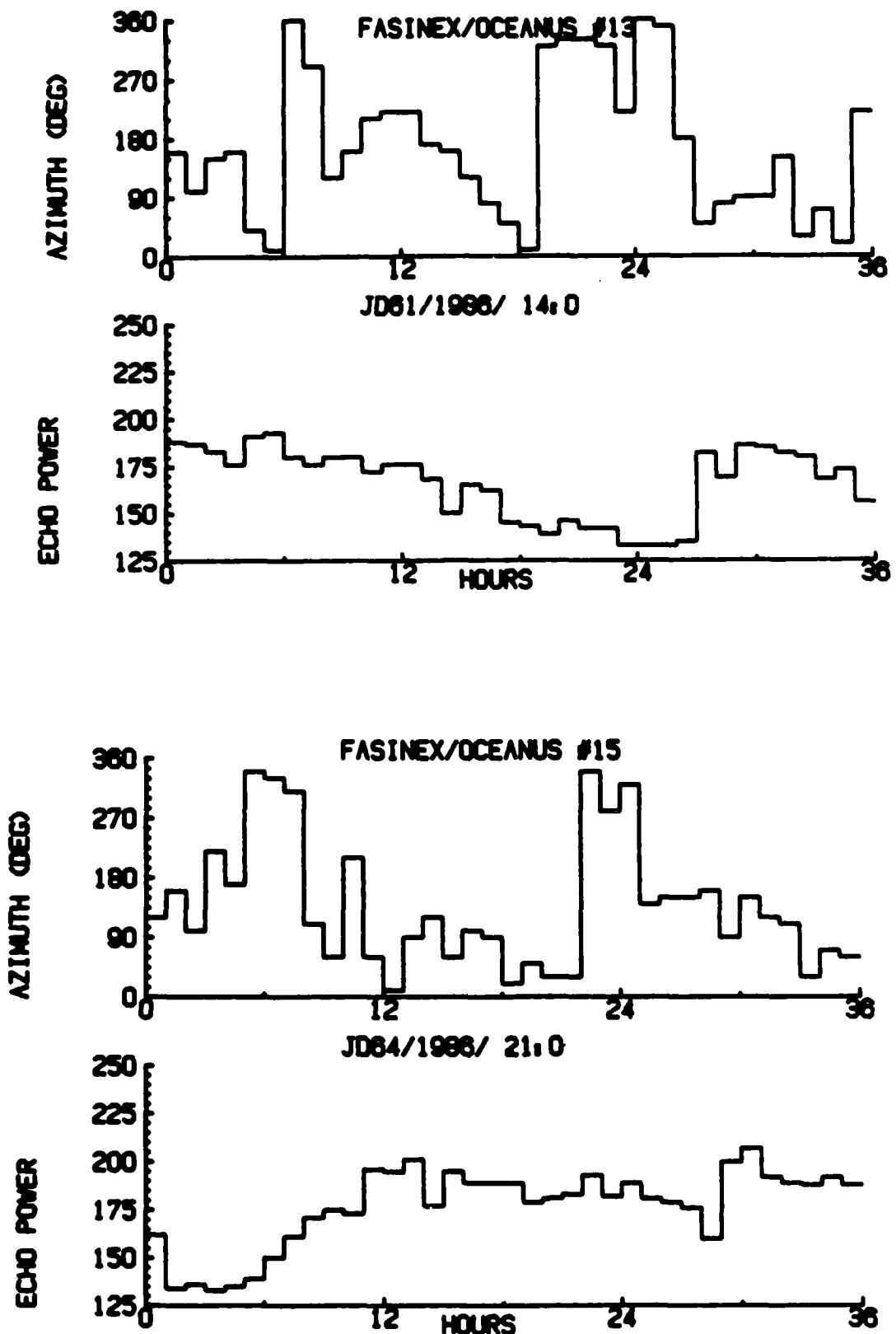


Figure XII-2: Peak Mean Signal Power Received and Direction of Maximum Return.

XII. AVHRR

During FASINEX Phase Two, a NEARSS (Northeastern Area Remote Sensing System) was set up at the Bermuda Biological Station office to receive AVHRR (Advance Very High Resolution Radiometer) satellite images. Using the ATS system, just as set up on KNORR, during Phase One, the images were processed at URI and sent via the Miami Vax to Bermuda.

Both the OCEANUS and ENDEAVOR had fax machines aboard. The plan had been to transmit frequent AVHRR images to the ships to help locate and track the front during the intensive scientific period. Unfortunately, the cloud cover was heavy much of the time. The fax machines did not work on OCEANUS and barely worked on ENDEAVOR. The NEARSS computer also suffered a damaged disk.

ENDEAVOR was able to receive satellite imagery via INMARSAT. This information was transferred to OCEANUS via the VHF radio when the ships were working closely together.

Peter Cornillon, having returned to URI for Phase Two, knowing the difficulty with transmissions to the ships digitized some AVHRR images and sent them to the ships via telemail whenever possible. This information was plotted up on the ships. With this means of mapping the frontal regions, along with the specific locations of frontal crossing seen from the aircraft, and the real time SST, the ships were able to coordinate their activities to survey along, across, or in the frontal regions.

Participant Summary:

XIV. CRUISE REPORT: ENDEAVOR 141
 February 5 - March 11, 1986
 A Component of FASINEX

Raymond W. Schmitt
 Woods Hole Oceanographic Institution
 April 15, 1986

PROJECT: EN-141 was a part of the FASINEX field program. Its goal was to examine the joint response of the atmosphere and ocean to the presence of the Subtropical Convergence Front.

SCHEDULE:

Depart Norfolk, Virginia	-	February 5, 1986
Arrive St. Georges, Bermuda	-	February 8, 1986
Depart St. Georges	-	February 11, 1986
Arrive Woods Hole, Mass.	-	March 10, 1986

REGION OF INVESTIGATION:

Western North Atlantic, Southwest of Bermuda.

FUNDING / PRINCIPAL INVESTIGATORS:

NSF:OCE 86-015336 / R. W. Schmitt and J. M. Toole

SCIENTIFIC PARTY (BERMUDA - WOODS HOLE):

Dr. Raymond W. Schmitt	WHOI	Co-Chief Scientist
Dr. Neil S. Oakey	BIO	Co-Chief Scientist
Dr. John M. Toole	WHOI	Scientist
Dr. Richard L. Koehler	"	Elec. Engineer
Ms. Mary Woodgate-Jones	"	Research Associate
Ms. Siobhan Knutel	"	Research Assistant
Mr. Richard Krishfield	"	Research Assistant
Mr. Jack Dellibovi	"	Electronic Technician
Dr. William Large	NCAR	Scientist
Mr. Peter Pozdnekoff	BIO	Marine Technician
Mr. Bruce Wile	"	Marine Technician
Mr. Stephan Borrman	NPS	Research Technician
Mr. Christopher A. Vaucher	"	Meteorologist
Mr. Paul Johnson	IOS	Marine Technician
Mr. Svein Vagle	"	Graduate Student
Mr. David Nelson	URI	Marine Technician

PURPOSE:

To study the physical structure of the Subtropical Convergence Front, using a ship mounted acoustic Doppler profiler, CTD and XBT surveys, and a new fine- and microstructure profiler (Schmitt/Toole). To examine spatial and temporal variability in upper ocean mixing rates (Oakey). To survey the characteristics of the atmospheric boundary layer near the front (Large, Borrman, Vaucher). To study wave breaking with acoustical and optical techniques (Johnson, Vagle).

CRUISE NARRATIVE:

The first leg of EN-141 was a transit from Norfolk Va. to St. Georges, Bermuda. Many of the scientists joined the ship in Norfolk in order to set up gear during the transit to Bermuda. Several technicians participated in the transit leg in order to test new data acquisition systems. During this leg word was received that the OCEANUS would be delayed getting to Bermuda, so that there was time for further testing. During the transit, four test CTD stations were done as well as two wire-lowered tests of the fine- and microstructure profiler. ENDEAVOR arrived in Bermuda at 1340 local time on Saturday, Feb. 8.

Additional science gear was aboard the OCEANUS, and the FASINEX plan called for joint work between ENDEAVOR and OCEANUS, so it was essential to wait for the arrival of the other ship. Departure was delayed from Monday morning to Tuesday afternoon. The arrival of the OCEANUS Tuesday morning initiated a very busy time for all concerned, as gear was transferred between the ships and instruments were set up, checked and secured. ENDEAVOR left St. Georges at 1700 local time and rounded the south side of Bermuda into 30 knot winds and heavy seas. OCEANUS departed a day later, in part because some chips for the repair of N. Oakey's computer were late arriving at the airport. These components were later transferred between the ships at sea. The heavy seas caused some discomfort amongst the scientific party, but since the FASINEX working area was two days steam from Bermuda, people were able to get acclimated before intensive work began.

Our first activity upon reaching the FASINEX area (28° N, 70° W) was to locate the front. Our initial survey area was near the moored array so we were unable to deploy XBTs. Using the acoustic Doppler current profiler and surface temperature and salinity observations, we were able to locate a very sharp front. It had a temperature contrast of $1.5 - 2.0$ deg. C, and a very pronounced shear on the warm (south) side of the front. We shifted our survey to the west and north in order to map the front, which had moved north of the moored array. When far enough from the array we began to deploy XBTs at 15 min. intervals. After two XBT sections we performed two CTD sections, all of them oriented north - south.

Throughout the cruise we had regular balloon launchings (Rawinsondes) at 0000, 1200 and 1800 hrs (GMT). There was also continuous measurement of meteorological parameters from a mast at the bow. An acoustic Sodar was used to measure wind profiles; this instrument eventually failed due to wave damage. Underway oceanographic measurements included acoustic Doppler currents, sea surface temperatures and conductivities. At times a drifting buoy (WOTAN) was deployed during daylight hours, for optical and acoustical studies of breaking waves and bubble formation. Microstructure measurements were made in the upper ocean with a loosely tethered profiler (EPSONDE) and the new free-fall fine- and microstructure profiler was deployed to greater depths (1000

m). For several hours during "Aircraft" days the ship would heave-to, bow to the wind, for intercomparisons between ship mounted and aircraft-born sensors. We found that we could profitably use the ship time with a mix of morning EPSONDE and profiler deployments, setting of the WOTAN drifter, meteorological station keeping from 1130-1530, afternoon profiler drops and EPSONDE work into the evening. Nights were then spent on surveys or tow-yo sections across the front.

Three times during the cruise we rendezvoused with the OCEANUS. The first time was to transfer some XBTs and computer chips from OCEANUS to ENDEAVOR by using a heaving line. This occurred at 1610 local on Feb. 15. The second meeting occurred from 1020 to 1435 on Feb. 23; six ENDEAVOR scientists visited the OCEANUS for scientific discussions. The final meeting occurred at 1830 on March 5 and involved the transfer of an ARGOS transmitter to the OCEANUS to repair a defective unit on one of the moorings. This was accomplished by casting over a buoyant package which the OCEANUS retrieved.

Our frontal surveys included close work with the OCEANUS during two periods. The first joint survey was a small diamond pattern in which the ENDEAVOR steamed parallel to the OCEANUS, 5 miles inside her track. This occurred from 1830 local on Feb. 25 to 0800 on Feb. 26. During the second period OCEANUS steamed a large rectangular box elongated in the north-south direction. Our intent was to do CTD tow-yo work at night and fine- and microstructure profiling during the day, but heavy weather forced us to stop work and heave to, from 1530 on March 1 to 1915 on March 2. The heartier souls on the OCEANUS were able to keep working with the towed "BATFISH". By the time we were permitted to work again, it was clear that the front was moving out of the survey box, so we continued with our mode of tracking the front at night and making microstructure profiles during the day.

Our final station was a deep CTD cast for calibration purposes at $29^{\circ}50'N$, $68^{\circ}00'W$ at 0900 on Mar. 7. Forecasts of heavy weather caused us to leave the area slightly earlier than planned, since it was important to have sufficient time to unload the ship in Woods Hole before it returned to Narragansett. Our northward progress was slowed to 6 knots at times but we did manage to tie up in Woods Hole at 1100 on March 10. Hard work by the science party and crew cleared the ship of gear by 1030 the next morning, when she set sail for Narragansett.

- Figure XIV-1 ENDEAVOR 141 Cruise Track
- Figure XIV-2 ENDEAVOR 141 CTD Station Positions
- Table XIV-1 CTD Station Log
- Figure XIV-3 ENDEAVOR 141 XBT Positions
- Table XIV-2 XBT Log

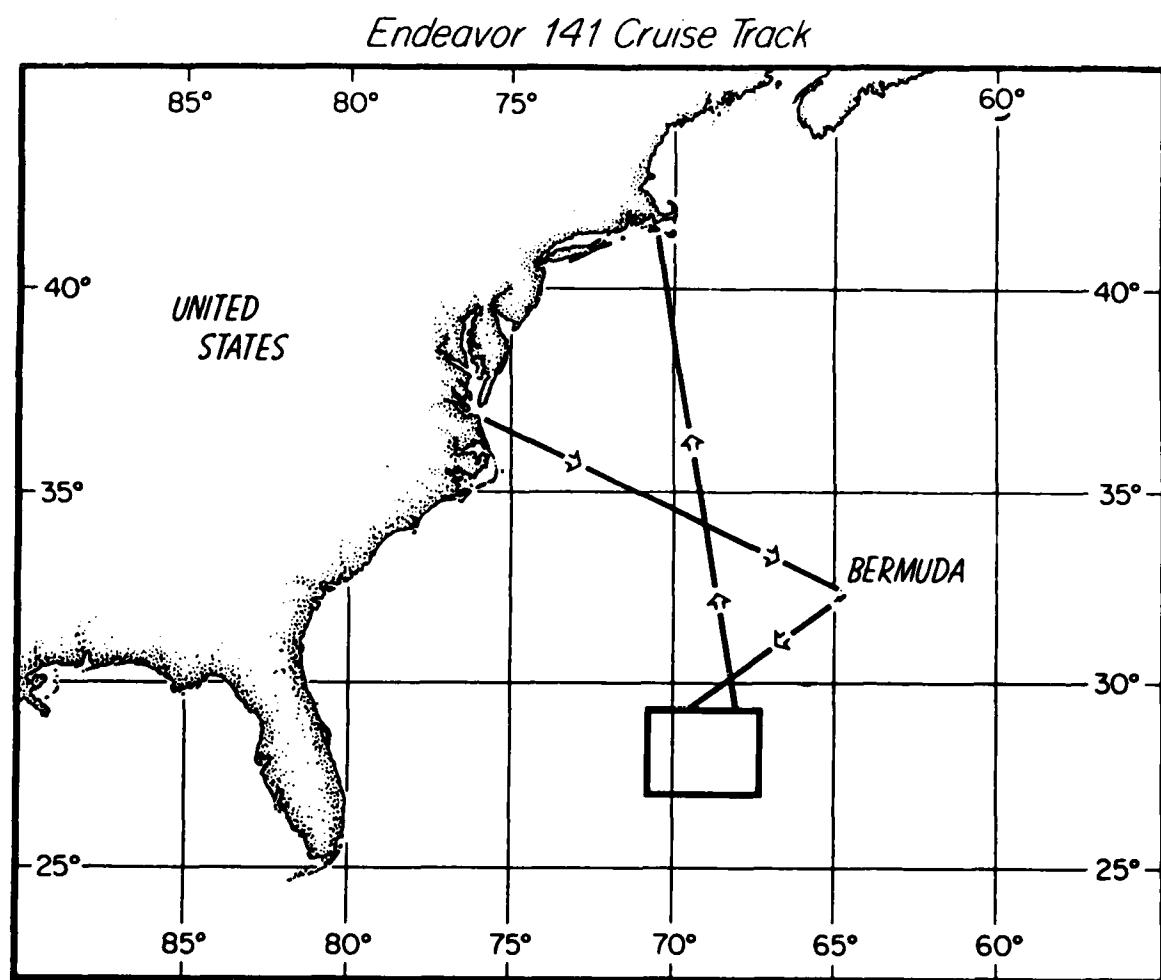


Figure XIV-1: ENDEAVOR 141 Cruise Track.

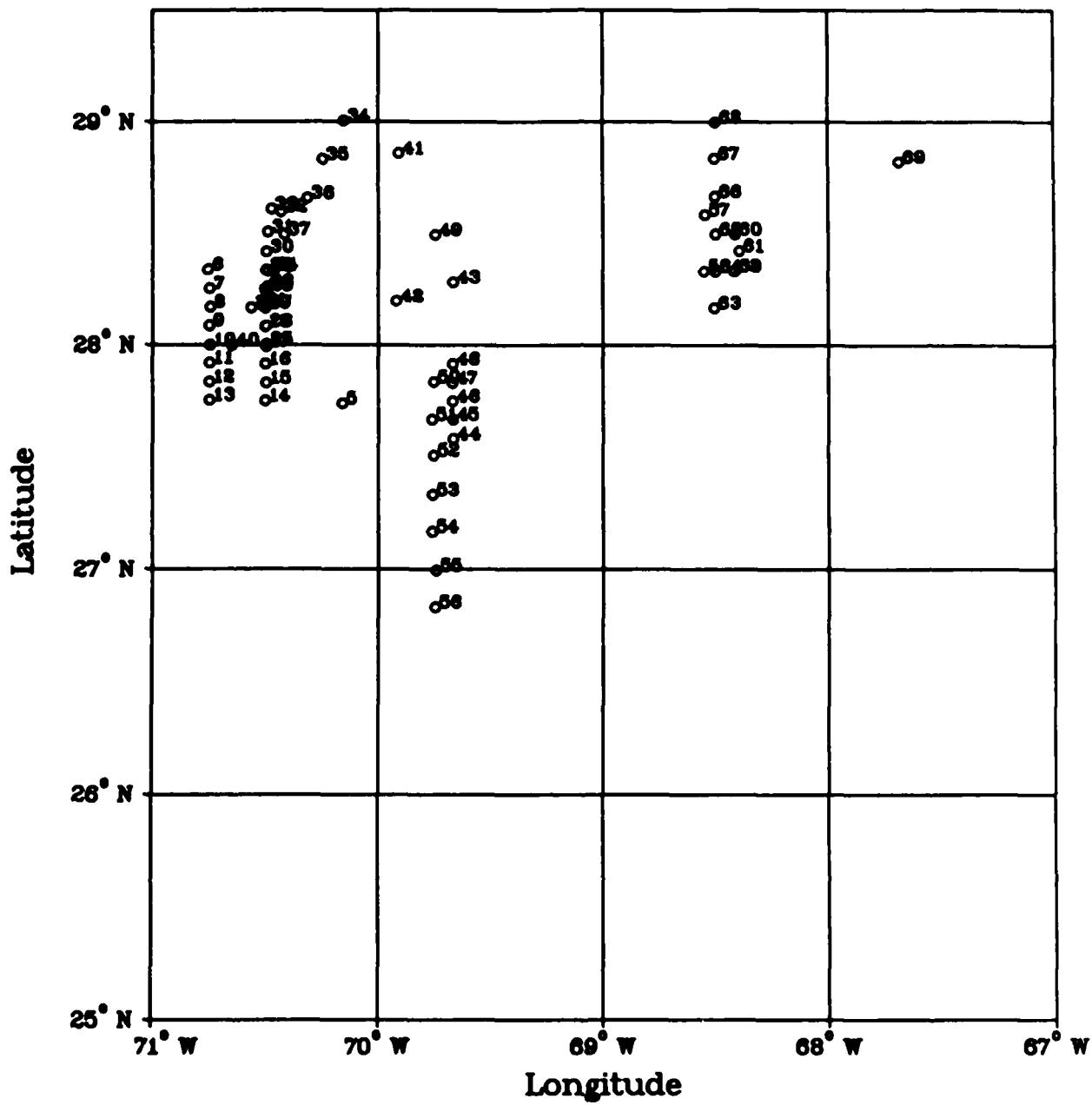
FASINEX Endeavor 141 CTD Stations

Figure XIV-2: ENDEAVOR 141 CTD Station Positions.

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 TABLE XIV-1
 EN-141 CTD STATION LOG

CTD #	YEAR DAY	START TIME GMT	NORTH LATITUDE (deg. min.)	WEST LONGITUDE (deg. min.)	MAX. PRESS. (db)	COMMENTS
1	37	1945	35 14.50	71 42.90	3821	CTD 7
2	38	1539	33 44.20	68 13.70	3005	CTD 8
3	38	1850	33 36.20	67 57.00	4137	CTD 7
4	38	2304	33 21.80	67 28.80	2658	CTD 9
5	44	1904	27 44.30	70 9.60	1009	CTD 7
6	45	1620	28 20.30	70 45.30	1405	CTD 9
7	45	1754	28 15.20	70 44.85	1215	
8	45	1921	28 10.20	70 44.75	1207	
9	45	2057	28 5.20	70 45.00	1205	
10	45	2225	28 0.00	70 44.80	1195	
11	46	6	27 55.20	70 44.80	1213	
12	46	133	27 50.10	70 44.90	1203	
13	46	334	27 45.20	70 44.90	1201	
14	46	552	27 45.05	70 30.10	1203	
15	46	719	27 49.80	70 29.80	1209	
16	46	855	27 54.90	70 30.00	1189	
17	46	1025	27 59.60	70 29.95	1183	
18	46	1204	28 4.95	70 30.10	1207	
19	46	1320	28 9.90	70 30.00	1207	
20	46	1652	28 14.70	70 29.75	1213	
21	47	1151	28 10.74	70 31.02	457	Tow-yo
22	47	2228	28 15.00	70 30.10	3513	
23	48	54	28 15.78	70 29.52	407	Tow-yo
24	48	2300	28 20.20	70 28.10	3993	
25	49	323	28 0.20	70 29.80	1201	CTD 7
26	49	442	28 5.00	70 29.90	1201	
27	49	557	28 10.10	70 29.90	1199	
28	49	712	28 14.70	70 29.90	1199	
29	49	830	28 20.10	70 29.90	1203	
30	49	958	28 25.10	70 29.85	1201	
31	49	1509	28 30.50	70 29.40	1201	
32	49	1826	28 35.90	70 25.90	1205	
33	50	101	28 36.60	70 28.50	1203	CTD 9
34	50	429	29 0.30	70 9.10	5539	GEOSAT
35	50	835	28 50.00	70 14.80	5543	SECTION
36	50	1306	28 39.60	70 18.80	5525	"
37	50	1657	28 29.80	70 25.00	5533	"
38	50	2139	28 19.90	70 29.40	5535	"
39	51	131	28 10.00	70 33.80	5527	"
40	51	528	27 59.90	70 39.00	5517	"
41	51	1803	28 51.60	69 54.50	1205	
42	52	129	28 11.82	69 55.14	405	Tow-yo (7)
43	54	138	28 16.98	69 40.02	399	Tow-yo (7)
44	55	642	27 34.80	69 40.10	1209	CTD 9
45	55	802	27 40.00	69 40.10	1205	
46	55	925	27 44.90	69 40.20	1193	
47	55	1044	27 49.80	69 40.20	1183	
48	55	1203	27 54.90	69 40.10	1205	

49	56	1452	28 29.75	69 44.85	3505	CTD	7
50	57	1813	27 50.10	69 45.20	1205	CTD	9
51	57	2013	27 40.00	69 45.70	1189		
52	57	2219	27 30.40	69 45.20	1193		
53	58	57	27 19.90	69 45.50	1209		
54	58	329	27 10.10	69 45.60	5553		
55	58	804	26 59.70	69 44.60	1203		
56	58	952	26 49.90	69 44.90	1193		
57	59	2310	28 35.10	68 32.80	1195	CTD	7
58	60	312	28 19.90	68 33.00	1209		
59	60	703	28 20.00	68 24.70	1201		
60	60	703	28 29.90	68 24.80	1205		
61	60	1506	28 25.40	68 23.70	1203		
62	60	1722	28 20.00	68 25.00	1203		
63	62	309	28 10.00	68 30.30	1205		
64	62	502	28 19.90	68 29.90	1217		
65	62	709	28 29.90	68 30.00	1203		
66	62	913	28 40.00	68 30.10	1217		
67	62	1108	28 50.20	68 30.20	1211		
68	62	1313	28 59.90	68 29.90	1209		
69	65	30	28 49.30	67 41.10	400	Tow-yo	
70	66	1256	29 49.70	68 0.60	4803		

FASINEX Endeavor 141 XBT Total Pattern

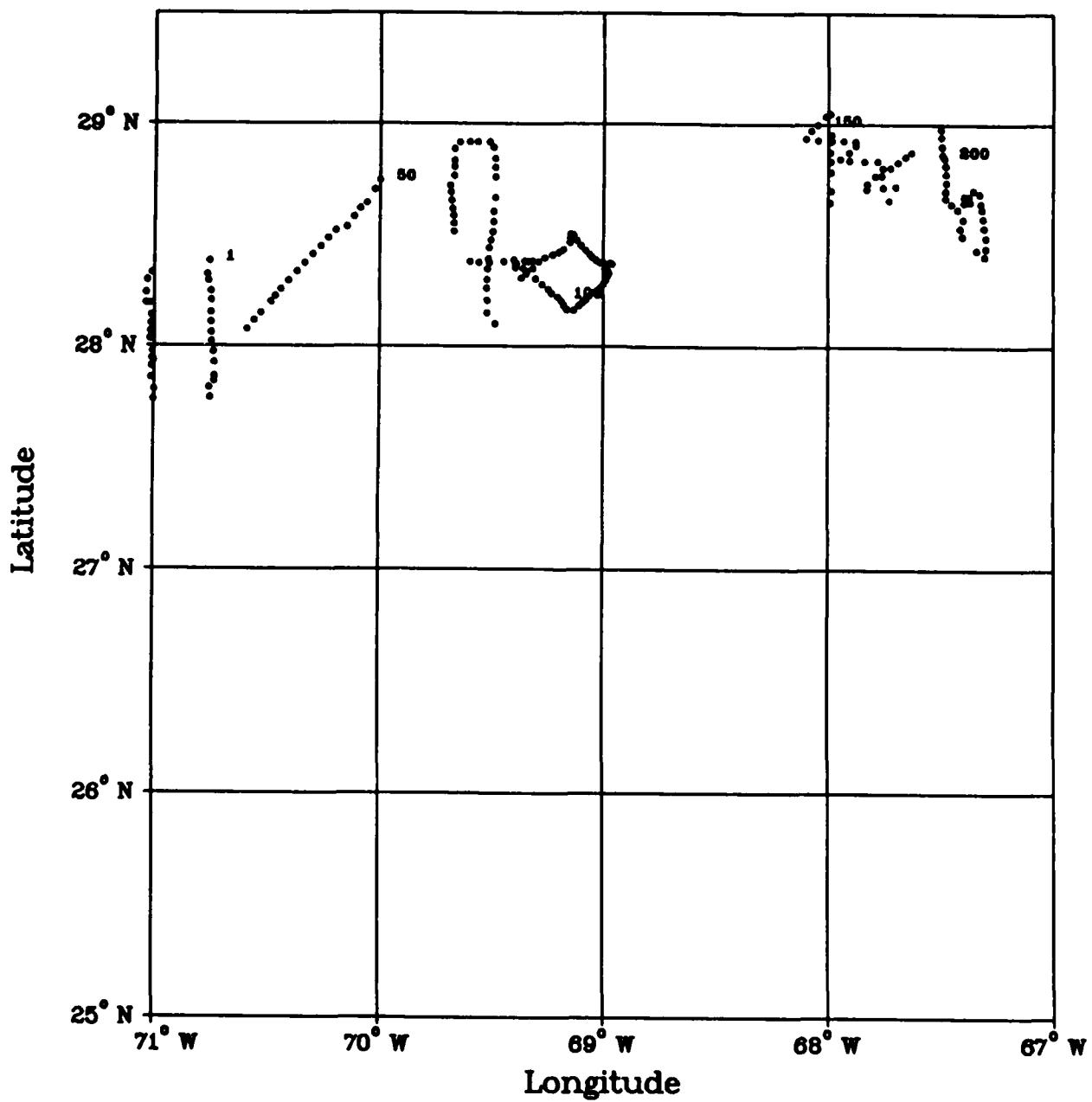


Figure XIV-3: ENDEAVOR 141 XBT Positions.

TABLE XIV-2
EN-141 XBT LOG

XBT #	YEAR	TIME	NORTH LATITUDE (deg. min.)	WEST LONGITUDE (deg. min.)	XBT SURF. TEMP. (deg.C)	BUCKET TEMP. (deg.C)	SURFACE SALINITY (PPT)
1	45	332	28 22.96	70 45.37	21.140	21.2	36.647
2	45	349	28 19.24	70 45.90	21.099	21.3	36.634
3	45	359	28 17.52	70 45.63	21.004	21.4	36.610
4	45	414	28 14.77	70 44.93	21.017	21.0	36.003
5	45	428	28 12.35	70 44.84	20.748	21.0	
6	45	459	28 9.06	70 45.06	21.126	21.4	36.605
7	45	513	28 6.42	70 45.03	21.485	21.5	36.619
8	45	528	28 3.67	70 44.99	22.821	21.5	36.685
9	45	543	28 1.20	70 44.84	23.455	23.2	36.677
10	45	559	27 58.46	70 44.30	23.455	23.4	36.663
11	45	614	27 55.66	70 44.16	23.593	22.7	36.649
12	45	635	27 51.90	70 44.04	23.332	23.5	36.637
13	45	643	27 50.60	70 44.10	23.348	21.8	36.661
14	45	658	27 48.84	70 45.48	23.075	23.0	36.655
15	45	713	27 46.18	70 45.10	23.332	23.3	36.650
16	45	855	27 45.63	71 0.12	22.970	23.1	36.710
17	45	915	27 48.30	71 0.18	22.970	23.0	36.656
18	45	935	27 51.54	71 0.99	23.045	23.2	36.648
19	45	1000	27 54.54	71 0.84	23.181	23.2	36.662
20	45	1020	27 56.61	71 0.78	23.166	23.2	36.665
21	45	1040	27 56.10	71 0.30	23.120	23.0	36.670
22	45	1100	27 58.53	71 0.69	23.060	23.1	36.673
23	45	1120	28 1.92	71 1.26	22.925	22.9	36.669
24	45	1140	28 3.96	71 1.14	22.806	22.8	36.665
25	45	12 0	28 6.00	71 1.02	22.540	22.7	36.663
26	45	1220	28 8.22	71 0.90	22.077	22.4	36.645
27	45	13 0	28 11.44	71 1.26	21.236	21.5	36.617
28	45	14 1	28 11.56	71 2.34	21.236	21.4	
29	45	1419	28 14.31	71 2.28	21.167	21.4	
30	45	1441	28 17.74	71 1.94	20.977	21.0	
31	45	15 1	28 19.75	71 0.79	20.788	21.0	
32	51	9 2	28 4.51	70 35.49	23.060	23.3	36.878
33	51	919	28 6.94	70 33.57	22.925	23.3	36.683
34	51	932	28 8.96	70 31.74	22.970	23.2	36.693
35	51	951	28 11.92	70 29.08	22.895	23.1	36.676
36	51	10 1	28 13.41	70 27.88	22.806	23.1	36.670
37	51	1014	28 15.34	70 26.39	22.806	23.0	36.661
38	51	1029	28 17.64	70 24.30	22.673	22.9	36.660
39	51	1045	28 20.13	70 22.03	22.599	22.9	36.656
40	51	11 0	28 22.32	70 20.01	22.717	22.9	36.657
41	51	1115	28 24.74	70 17.81	22.658	22.8	36.665
42	51	1130	28 26.96	70 15.74	22.408	22.7	36.658
43	51	1145	28 29.20	70 13.73	21.443	21.7	36.632
44	51	1159	28 31.25	70 11.78	21.360	21.7	36.641
45	51	1215	28 32.26	70 8.86	21.415	21.7	36.640
46	51	1231	28 34.95	70 6.96	21.415	21.8	36.642
47	51	1245	28 37.26	70 5.34	21.652	21.8	36.640
48	51	13 1	28 38.69	70 3.55	21.638	21.9	36.640

49	51	1315	28	42.28	70	1.44	21.778	22.0	36.643
50	51	1330	28	44.82	70	0.06	21.666	22.0	36.661
51	56	315	28	6.00	69	29.10	22.380	22.7	36.675
52	56	344	28	8.94	69	31.32	21.373	21.7	36.693
54	56	4 1	28	12.36	69	31.20	21.977	22.2	36.665
55	56	418	28	15.60	69	31.38	22.249	22.5	36.657
56	56	430	28	17.95	69	31.25	22.206	22.6	36.649
57	56	444	28	20.80	69	31.10	22.482	22.9	36.652
58	56	459	28	23.58	69	30.95	22.482	22.8	36.662
59	56	514	28	26.53	69	30.79	22.540	22.7	36.677
60	56	529	28	28.68	69	30.24	22.702	22.9	36.681
61	56	544	28	30.82	69	29.75	22.658	22.9	36.700
62	56	559	28	33.59	69	29.59	22.453	22.7	36.685
63	56	614	28	36.36	69	29.52	22.278	22.5	36.687
64	56	630	28	40.06	69	29.14	22.063	22.3	36.663
65	56	644	28	42.64	69	28.99	22.220	22.5	36.669
66	56	7 0	28	45.65	69	29.14	21.877	22.2	36.665
67	56	714	28	48.24	69	29.28	21.485	21.7	36.647
68	56	729	28	50.64	69	29.22	21.004	21.3	36.640
69	56	745	28	53.61	69	29.73	21.031	21.3	36.642
70	56	758	28	55.12	69	30.79	20.896	21.1	36.618
71	56	816	28	55.14	69	33.96	20.748	21.1	36.610
72	56	829	28	55.13	69	36.14	20.991	21.4	36.658
73	56	844	28	55.03	69	38.73	21.004	21.4	36.637
74	56	9 1	28	53.27	69	40.19	20.991	21.3	36.631
75	56	919	28	50.16	69	40.14	21.457	21.7	36.642
76	56	930	28	48.41	69	40.19	21.963	22.0	36.196
77	56	944	28	46.00	69	40.20	21.778	22.2	36.647
78	56	10 3	28	43.36	69	41.24	22.467	22.7	36.661
79	56	1015	28	41.51	69	41.06	22.263	22.8	36.670
80	56	1029	28	39.31	69	40.84	22.555	22.8	36.683
81	56	1045	28	37.08	69	40.56	22.496	22.8	36.665
82	56	1058	28	35.20	69	40.30	22.453	22.7	36.655
83	56	1112	28	33.14	69	40.20	22.162	22.4	36.670
84	56	1129	28	30.91	69	40.14	22.063	22.4	36.667
85	56	20 6	28	22.70	69	35.84	22.526	22.7	36.666
86	56	2031	28	22.51	69	33.45	21.991	22.4	36.678
87	56	2044	28	22.58	69	30.61	22.613	22.5	36.674
88	56	21 1	28	22.70	69	26.76	22.263	22.3	36.523
89	56	2113	28	23.25	69	24.06	22.613	22.8	36.654
90	56	2130	28	22.86	69	20.28	22.687	22.7	36.656
91	56	2144	28	22.98	69	19.08	22.569	22.7	36.660
92	56	2158	28	22.90	69	21.12	22.599	22.6	36.642
93	56	2214	28	22.20	69	23.44	22.628	22.8	36.659
94	56	2228	28	21.26	69	23.68	22.540	22.8	36.659
95	56	2245	28	20.95	69	21.67	22.613	22.6	36.668
96	56	23 0	28	20.16	69	20.58	22.555	22.7	36.663
97	56	2313	28	18.12	69	18.26	22.526	22.7	36.647
98	56	2329	28	16.61	69	16.42	22.453	22.7	36.661
99	56	2344	28	15.34	69	14.77	22.365	22.4	36.678
100	57	0 1	28	14.35	69	13.98	22.191	22.4	36.675
101	57	014	28	13.23	69	12.24	22.599	22.8	36.652
102	57	029	28	12.29	69	11.30	22.910	23.1	36.647
103	57	044	28	10.93	69	10.74	22.925	23.2	36.669
104	57	1 0	28	9.84	69	9.82	23.060	23.4	36.597

105	57	115	28	9.72	69	8.10	23.135	23.3	36.609
106	57	130	28	10.92	69	6.78	23.195	23.3	36.600
107	57	145	28	11.85	69	5.76	23.060	23.3	36.603
108	57	159	28	12.66	69	4.80	23.150	23.3	36.612
109	57	215	28	13.69	69	3.83	23.150	23.3	36.629
110	57	231	28	14.54	69	2.92	22.985	23.3	36.639
111	57	244	28	15.00	69	1.62	22.940	23.2	36.648
112	57	3 0	28	15.90	69	0.72	22.985	23.2	36.639
113	57	314	28	16.81	69	0.07	22.821	23.1	36.640
114	57	329	28	17.82	68	59.49	22.673	23.1	36.667
115	57	344	28	18.81	68	58.98	22.702	23.0	36.660
116	57	359	28	19.79	68	58.59	22.555	22.8	36.683
117	57	413	28	20.36	68	58.81	21.877	22.1	36.637
118	57	429	28	20.83	68	59.62	21.485	21.8	36.647
119	57	444	28	22.14	68	57.72	21.250	21.6	36.658
120	57	458	28	22.44	68	58.26	21.332	21.5	36.648
121	57	512	28	22.32	68	59.94	21.388	21.5	36.655
122	57	528	28	22.55	69	0.90	21.388	21.6	36.640
123	57	548	28	23.24	69	2.06	21.568	21.7	36.653
124	57	6 1	28	24.02	69	3.04	21.680	21.9	36.653
125	57	614	28	24.84	69	3.78	21.764	22.0	36.655
126	57	630	28	25.86	69	4.88	21.806	22.1	36.659
127	57	644	28	27.10	69	6.08	21.906	22.2	36.679
128	57	659	28	28.54	69	7.14	21.694	22.1	36.687
129	57	715	28	30.00	69	8.04	21.652	22.0	36.716
130	57	730	28	30.28	69	8.80	21.666	21.9	36.670
131	57	744	28	29.14	69	8.93	21.849	22.0	36.767
132	57	759	28	27.91	69	9.05	21.736	22.0	36.747
133	57	815	28	26.04	69	10.82	21.835	22.1	36.692
134	57	830	28	25.36	69	12.03	22.005	22.2	36.678
135	57	843	28	24.66	69	13.68	22.063	22.3	36.669
136	57	859	28	23.81	69	15.78	22.365	22.6	36.695
137	57	913	28	22.72	69	17.42	22.365	22.7	36.751
138	57	928	28	20.94	69	18.90	22.453	22.6	36.675
139	57	946	28	19.54	69	20.79	22.365	22.6	36.691
140	57	10 0	28	18.30	69	22.01	22.423	22.6	36.663
141	64	129	28	39.64	67	43.72	22.177	22.5	36.700
142	64	145	28	39.08	67	59.46	22.336	22.5	36.704
143	64	2 2	28	42.29	67	59.27	22.162	22.5	36.683
144	64	229	28	47.24	67	59.28	22.394	22.6	36.676
145	64	244	28	50.10	67	59.34	22.292	22.5	36.685
146	64	259	28	52.68	67	59.46	22.365	22.5	36.684
147	64	314	28	55.43	67	59.36	22.249	22.4	36.689
148	64	329	28	57.31	67	59.16	21.948	22.2	36.684
149	64	4 1	29	3.03	67	59.40	20.936	21.2	36.693
150	64	414	29	2.30	68	0.78	21.004	21.2	36.669
151	64	429	29	0.06	68	2.85	22.134	21.2	36.696
152	64	443	28	58.44	68	4.50	22.162	21.3	36.712
153	64	459	28	56.30	68	5.95	22.249	22.4	36.729
154	64	515	28	55.95	68	2.79	22.148	22.4	36.699
155	64	531	28	55.80	67	59.04	22.105	22.4	36.726
156	64	545	28	55.74	67	55.94	21.208	21.6	36.688
157	64	559	28	55.56	67	52.70	21.250	21.4	36.680
158	64	614	28	54.42	67	52.68	21.154	21.4	36.694
159	64	629	28	52.63	67	54.41	21.638	21.9	36.692

160	64	644	28 50.83	67 56.74	22.249	22.4	36.716
161	64	659	28 50.45	67 54.38	22.148	22.4	36.694
162	64	715	28 50.28	67 50.32	21.429	21.5	36.679
163	64	729	28 50.22	67 46.88	21.263	21.5	36.693
164	64	745	28 48.36	67 45.46	21.236	21.4	36.686
165	64	8 0	28 46.27	67 47.47	21.099	21.6	36.661
166	64	815	28 44.12	67 49.54	22.091	22.4	36.680
167	64	829	28 42.64	67 49.70	22.220	22.4	36.677
168	64	846	28 43.10	67 45.32	21.540	21.4	36.673
169	64	9 0	28 43.34	67 42.05	20.775	20.9	36.649
170	65	11 5	28 46.32	67 45.74	22.235	22.4	
171	65	1120	28 48.48	67 43.42	22.091	22.4	
172	65	1132	28 49.94	67 41.42	22.120	22.4	
173	65	1143	28 51.42	67 39.40	22.048	22.2	
174	65	1153	28 52.62	67 37.80	21.195	21.4	
175	65	2315	28 40.74	67 23.76	21.017	21.4	36.703
176	65	2328	28 42.32	67 21.32	21.250	21.4	36.705
177	65	2343	28 41.40	67 19.68	21.126	21.3	36.682
178	66	0 1	28 38.78	67 19.35	21.126	21.4	36.687
179	66	015	28 37.27	67 19.01	21.208	21.5	36.682
180	66	030	28 34.73	67 18.70	21.126	21.3	36.676
181	66	044	28 32.20	67 18.40	21.086	21.3	36.679
182	66	059	28 29.58	67 17.98	21.457	21.7	
183	66	115	28 26.73	67 17.96	21.934	22.3	36.706
184	66	130	28 24.58	67 18.29	22.249	22.4	36.742
185	66	147	28 26.22	67 20.42	22.134	22.4	36.696
186	66	216	28 29.96	67 24.22	22.091	22.4	36.706
187	66	230	28 32.12	67 24.88	22.206	22.4	36.692
188	66	244	28 34.52	67 24.08	22.177	22.3	36.699
189	66	3 1	26 53.02	63 16.62	22.005	22.2	36.715
190	66	315	28 39.21	67 22.23	21.610	21.8	36.732
191	66	331	28 40.62	67 22.50	21.181	21.2	36.706
192	66	343	28 39.06	67 23.82	22.134	22.3	36.699
193	66	359	28 37.26	67 25.52	22.235	22.4	36.698
194	66	414	28 38.67	67 27.15	22.220	22.4	36.687
195	66	429	28 40.23	67 28.74	22.220	22.4	36.724
196	66	444	28 42.15	67 28.77	22.134	22.4	36.707
197	66	459	28 44.49	67 28.53	22.220	22.5	36.694
198	66	514	28 46.87	67 28.63	22.322	22.5	36.700
199	66	529	28 49.04	67 28.79	22.380	22.5	36.695
200	66	543	28 51.14	67 29.00	22.105	22.4	36.694
201	66	559	28 51.66	67 29.40	22.278	22.4	36.684
202	66	614	28 52.02	67 29.50	22.336	22.4	36.676
202B	66	628	28 54.21	67 29.71	22.019	22.4	36.696
203	66	644	28 56.70	67 29.94	21.963	22.2	36.696
204	66	659	28 58.82	67 30.00	21.638	21.8	36.700

Participant Summary:**XV. FINE- AND MICROSTRUCTURE PROFILING DURING FASINEX**

Raymond W. Schmitt and John M. Toole
Woods Hole Oceanographic Institution
April 30, 1986

Project Objectives:

The FASINEX cruise of the R/V ENDEAVOR was the first use of a new free-fall fine- and microstructure profiler developed at WHOI with DoD and ONR support. The experimental goal was to study the detailed velocity structure of the front, inertial wave climatology, and mixing processes which occur in and around the front.

Vessel:

R/V ENDEAVOR, February 11 - March 10, 1986

Scientific Party Involved:

Dr. R. W. Schmitt	Chief Scientist
Dr. J. M. Toole	Scientist
Dr. R. L. Koehler	Engineer
Mr. J. Dellibovi	Technician

Narrative:

This cruise culminated an intensive two year effort to construct a new fine- and microstructure profiler which incorporates a variety of sensors into one computer-controlled instrument. Profiler features include: full ocean depth capability, computer control of sampling, data storage and operations, four megabytes of solid state memory, and commercially available sensors. The finescale sensors include a CTD, acoustic velocimeter, accelerometers and compass, all sampled at 10 Hz. The microstructure sensors included downward directed fast temperature and conductivity probes, two airfoil shear probes, and wing mounted fast conductivity probes which sample a helical path as the rotating instrument falls through the water. The microstructure sensors are sampled at 200 Hz. The 5 m long cylindrical instrument is launched and deployed with a specially designed cradle which lifts the profiler out of the water, tilts it to a horizontal position and allows it to be moved along rails mounted on the deck. (Figure 1)

All gear for the profiler was loaded aboard ENDEAVOR in Norfolk, Va., Feb. 3-5, 1986. Toole, Koehler and Dellibovi participated in the Norfolk - Bermuda transit in order to test the profiler. This was done with two wire lowerings on Feb. 6 and 8. The instrument was opened for testing and examination in Bermuda; then closed up before we left port. A substantial battery and the use of low power components insured that there would be minimal opening of the instrument at sea. We were able to get 36 dives, all but three to 1000 m, with a single battery pack. An additional three dives were collected after battery replacement. The only other time the instrument was opened was to change gain settings on

the accelerometers. This type of trouble free performance is remarkable for the first use of an instrument and reflects the high quality of the design and workmanship that went into the instrument and the thorough pre-cruise trouble-shooting.

Our sampling strategy was to profile as close as possible to deployments of "EPSONDE", Dr. Neil Oakey's microstructure instrument. A typical station constituted 3-5 EPSONDE casts to 200 m and one profiler dive to 1000 m. We usually attempted to occupy 3 or 4 stations across the front during daylight hours; however, the weather, other FASINEX logistical requirements, and emergencies sometimes prevented complete transects. As many as 5 profiles were made in one day. Two dives were recovered in early morning darkness; these recoveries were risky because of the difficulty in judging distances between profiler and ship. Nevertheless, nighttime operations do appear feasible under good weather conditions. During the cruise there were occasional impacts between the profiler and the ship. Damage to the profiler was minimal, however, because all of the delicate sensors were well below the depth of the bilge keel on ENDEAVOR. The handling rig allowed us to work in a moderate sea state (winds to 20 knots), and one recovery was made in 35 knot winds.

Because of Neil Oakey's participation on this cruise we were able to implement use of the airfoil shear probes developed by T. Osborn. These were used on a total of 10 dives. We found that the profiler had a certain amount of vibrational noise near 60 hz, marginally above the geophysical shear cutoff, which should be eliminated with appropriate filtering of the data. Strong mixing events were quite apparent in the raw record and attempts to isolate the probes from body vibrations were moderately successful in later dives.

The times, deployment and recovery locations, ENDEAVOR event numbers, pressure ranges of fine- and microstructure data recording, and the microsensors used on the various dives are given in Table 1. Acoustic transponders for instrument tracking were tested at two stations but they failed to respond reliably to the signals from the profiler. We will have to use a different type of transponder in future experiments. Dives 19, 20, and 21 were made near Profiling Current Meter (PCM) moorings of C. Eriksen, near the times when the PCM would be making its excursion. These will allow us to intercompare velocity profiles, which is very useful for checking data analysis schemes.

Several exciting features were sampled by the profiler near the FASINEX front. Preliminary data processing conducted on the cruise yielded estimates of the ocean temperature, salinity and east and north velocity profiles versus pressure. Such profiles were available about 2 hours after a dive was completed. Accompanying these data are the microscale quantities of temperature, conductivity and shear. Dive 17 (Figure XV-3) sampled a particularly energetic, short vertical scale internal wave at about 200 m depth

on the warm side of the front. The velocity vector in this feature is seen to rotate clockwise with depth, suggesting a downward propagating near-inertial wave. Strong microstructure activity at the depth of this feature was observed by both the profiler and EPSONDE. Later in the cruise a set of profiles from the warm side of the front revealed a series of well mixed layers stacked in the vertical (Dive 34, Fig XV-4). The surface mixed layer was roughly 75 m deep with a temperature near 22.5 C. Below was found a second weakly stratified zone some 100 m thick with a temperature near 21.2 C. This thermostad could be traced to the surface mixed layer on the cold side of the front. Still deeper was the 18 C thermostad. The velocity profile through the two layers was quite remarkable. Each layer appeared to exhibit slab-like flow with shear zones at the steps between layers. Energetic microstructure was observed in these shear zones. A short time series at this site revealed time dependency to the flow, possibly near-inertial oscillations.

FASINEX was thus a highly successful first cruise for the profiler. The large number of deployments were obtained in spite of frequent episodes of bad weather and the other shipboard activities that were conducted. We are now looking forward to the analysis phase of the experiment and collaborative work with Neil Oakey and the other FASINEX investigators.

Acknowledgments:

The primary engineers working on the new profiler were R. Koehler, E. Mellinger and K. Doherty. They were assisted by K. Fairhurst, K. Wannop, M. Woodward and J. Dellibovi. T. Danforth, K. Prada and T. Sgouros and M. Woodgate-Jones helped to develop software. A. Martin assisted with the Micro-VAX computer. Neil Oakey provided the airfoil shear probes and advice on their electronics. The development of such a complex device as this was no small task and all concerned are thanked for their contributions. We acknowledge the Captain and crew of ENDEAVOR for their ship handling. The profiler was developed with funds from the DoD Instrumentation Program and the Office of Naval Research.

Captions:

Figure XV-1. Schematic of Microstructure Profiler

Figure XV-2. Microstructure profiler drop sites

Table XV-1. The dive numbers, ENDEAVOR event numbers, the 1986 year day and the deployment and retrieval times and positions, for the fine- and microstructure profiler. Also shown are the pressure ranges for the recording of fine and microstructure variables. The microstructure sensors are coded as: T = nose fast temperature, C = nose fast conductivity, S = shear probes, W = wing fast conductivities.

Figure XV-3. Profiles of Temperature (deg. C), Salinity (ppt), and the North and East components of velocity (m/s), for Dive 17.

Figure XV-4. Profiles of Temperature (deg. C), Salinity (ppt), and the North and East components of velocity (m/s), for Dive 34.

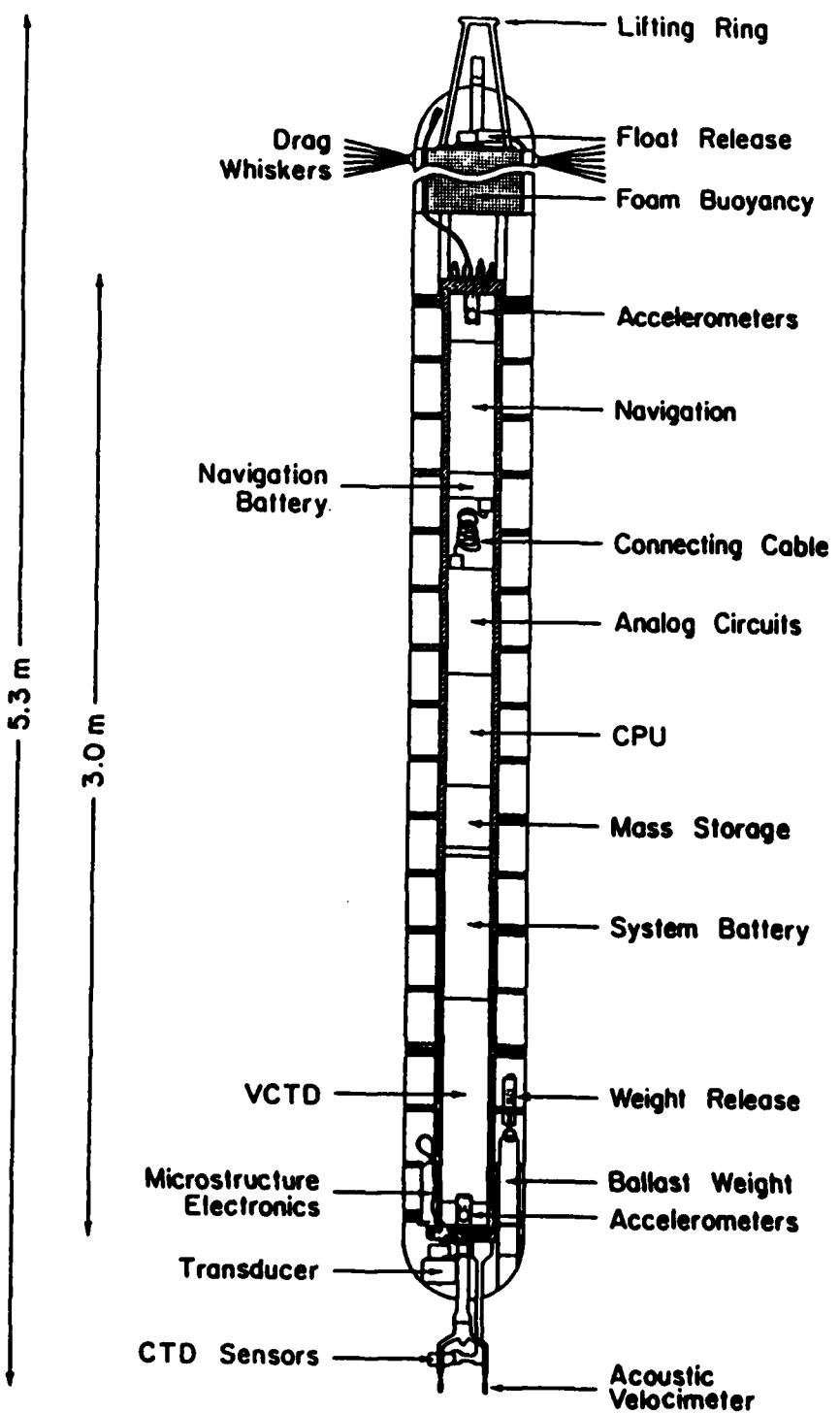


Figure XV-1: Schematic of Microstructure Profiler.

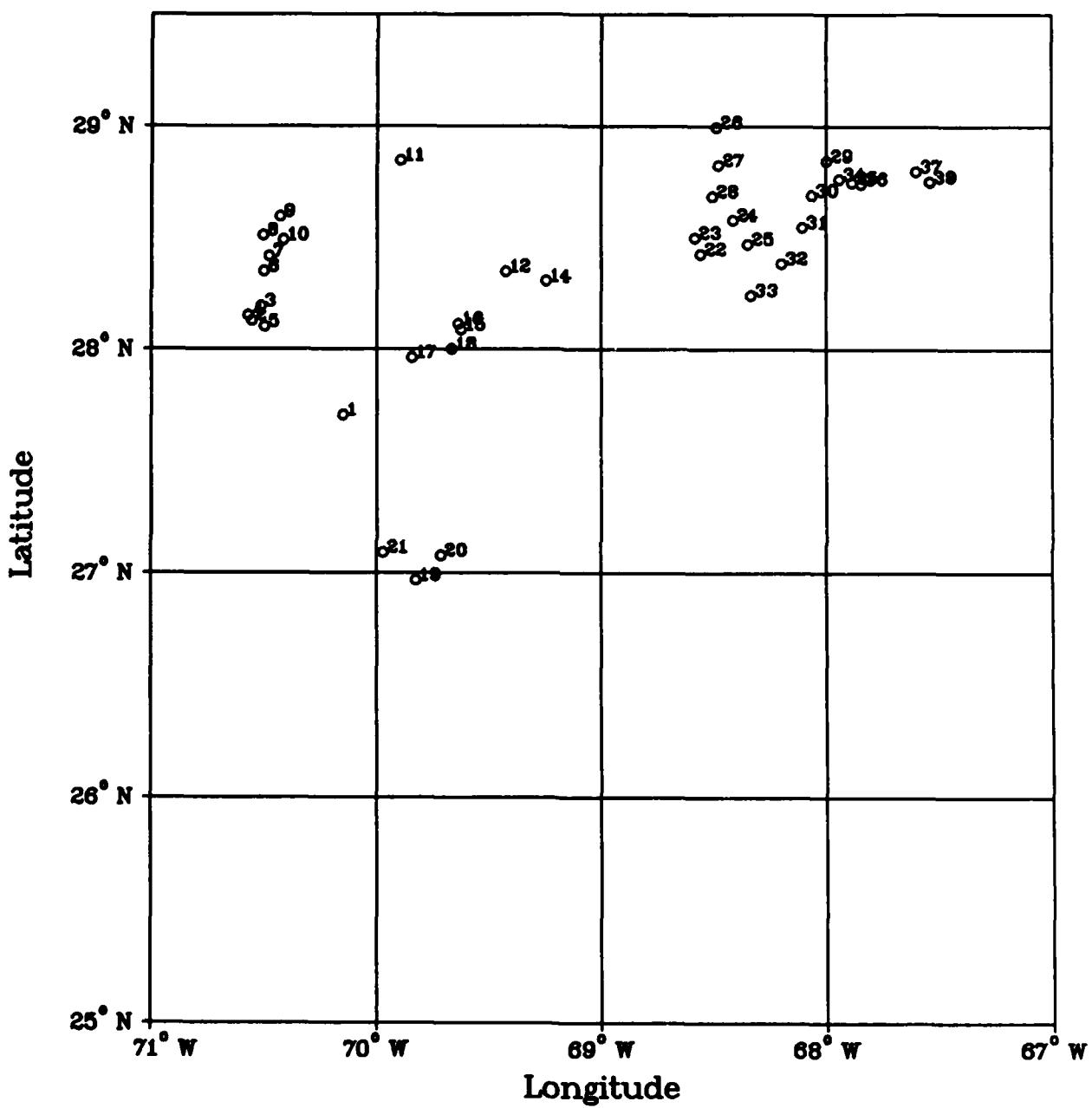
FASINEX Endeavor 141 Microprofiler Dives

Figure XV-2: Microstructure Profiler Drop Sites.

TABLE XV-1

EN - 141
FINE- AND MICROPROFILER DIVES

DIV #	EV #	'86 DAY	TIME GMT	DEPLOY				TIME GMT	RETRIEVE				FINE MAX PRES	MICRO			COMMENT
				LAT. deg	LONG. min	LAT. deg	LONG. min		PRES	SENS	P MIN	P MAX					
A	-	37	2100	35 15.6	71 43.2	2125	35 15.6	71 43.2	100	TC	25	100	Wire				
B	-	39	1430	32 14.0	64 37.8	1540	32 14.3	64 38.0	1000	TC	25	1000	Wire				
1	7	44	1833	27 42.3	70 09.0	1930	27 44.4	70 09.6	500	TC	25	500	Zodiac				
2	86	47	1725	28 07.6	70 33.3	1820	28 07.6	70 32.1	1000	TC	25	1000					
3	92	47	2043	28 11.5	70 30.8	2149	28 11.2	70 30.8	1000	TC	25	1000					
4	103	48	1358	28 09.0	70 34.2	1508	28 09.0	70 34.1	1000	TC	25	1000					
5	107	48	1658	28 06.0	70 29.9	1800	28 06.0	70 29.9	1000	TC	25	1000					
6	111	43	2100	28 20.9	70 30.1	2154	28 20.2	70 29.2	1000	TC	25	1000					
7	128	49	1050	28 25.0	70 28.7	1155	28 24.6	70 28.1	1000	TC	25	1000					
8	136	49	1532	28 30.6	70 30.3	1620	28 30.6	70 30.3	1000	TC	25	1000					
9	140	49	1858	28 35.7	70 25.8	2000	28 36.3	70 25.8	520	TC	25	520	Bln snag				
10	159	50	1935	28 29.4	70 24.9	2035	28 29.4	70 24.9	1000	TC	25	1000					
11	194	51	1900	28 50.9	69 53.8	1942	28 50.8	69 53.6	1000	TC	25	1000					
12	213	53	1620	28 20.9	69 25.6	1710	28 21.5	69 24.9	1000	TC	25	1000					
14	218	53	2110	28 18.4	69 14.8	2206	28 18.6	69 15.4	1000	TC	25	1000					
15	227	54	1305	28 05.2	69 37.5	1354	28 04.5	69 38.2	1000	TCS	25	500	Trnsrndr				
16	230	54	1523	28 06.8	69 38.2	1625	28 08.0	69 38.2	1000	TCS	25	500	Bln Snag				
17	248	55	1419	27 57.7	69 50.6	1508	28 57.5	69 49.6	1000	TCS	25	500					
18	255	55	2101	28 00.0	69 40.0	2155	27 59.8	69 40.8	250	TCS	25	250	Con Short				
19	377	58	1213	26 58.1	69 49.5	1303	26 58.4	69 49.6	1000	TC	25	1000	F5				
20	381	58	1612	27 04.7	69 42.8	1705	27 04.7	69 42.8	1000	TC	25	1000	F3				
21	387	58	2036	27 05.5	69 58.2	2125	27 05.7	69 58.3	1000	TC	25	1000	F9				
22	396	59	1640	28 25.6	68 33.5	1736	28 25.4	68 33.7	1000	TC	25	1000					
23	399	59	2010	28 30.0	68 35.0	2107	28 28.6	68 34.0	1000	TC	25	1000					
24	412	60	0909	28 34.8	68 24.8	1000	28 33.8	68 24.9	1000	TC	25	1000					
25	416	60	1217	28 28.3	68 20.9	1304	28 31.1	68 23.3	1000	TC	25	1000					
26	442	62	1347	28 59.8	68 29.3	1445	28 59.2	68 28.6	1000	TC	25	1000					
27	449	62	1735	28 49.6	68 28.7	1427	28 49.6	68 28.7	1000	TC	25	1000					
28	451	62	1950	28 41.2	68 30.3	2050	28 41.3	68 28.8	1000	TC	25	1000					
29	458	63	1014	28 50.8	67 59.9	1120	28 50.6	67 59.1	1000	TC	25	1000					
30	462	63	1301	28 41.5	68 03.8	1340	28 41.0	68 02.9	1000	TC	25	1000					
31	468	63	1618	28 32.9	68 06.3	1705	28 32.7	68 05.6	1000	TC	25	1000					
32	473	63	1850	28 23.1	68 11.9	1938	28 23.2	68 12.0	1000	TC	25	1000					
33	478	63	2135	28 14.5	68 20.0	2225	28 14.7	68 19.9	1000	TC	25	1000					
34	516	64	1035	28 45.9	67 56.4	1130	28 46.4	67 56.2	1000	TCS	25	500					
35	522	64	1415	28 45.0	67 53.0	1513	28 44.3	67 53.7	1000	TCS	25	500					
36	526	64	1650	28 44.6	67 50.6	1745	28 44.3	67 49.6	1000	TCS	25	500					
37	543	65	1416	28 48.0	67 36.0	1500	28 48.0	67 35.5	500	TCSW	25	500					
38	546	65	1717	28 45.2	67 32.4	1754	28 45.2	67 32.3	500	TCSW	25	500					
39	549	65	2008	28 45.1	67 32.3	2050	28 43.8	67 31.7	500	TCSW	25	500	Trnsrndr				

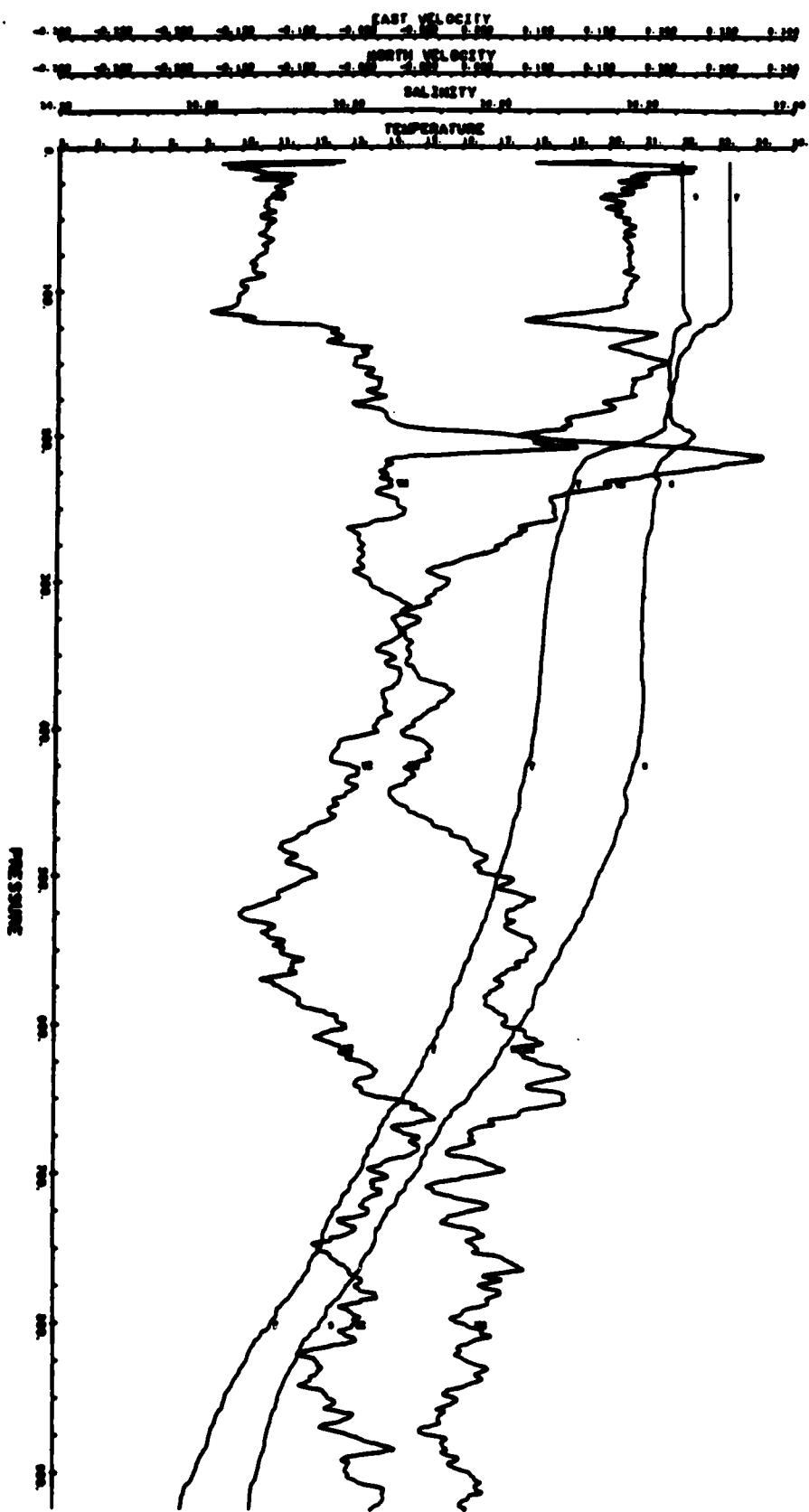


Figure XV-3: Profiles of Temperature (deg. C), Salinity (ppt), and the North and East components of velocity (m/s), for Dive 17.

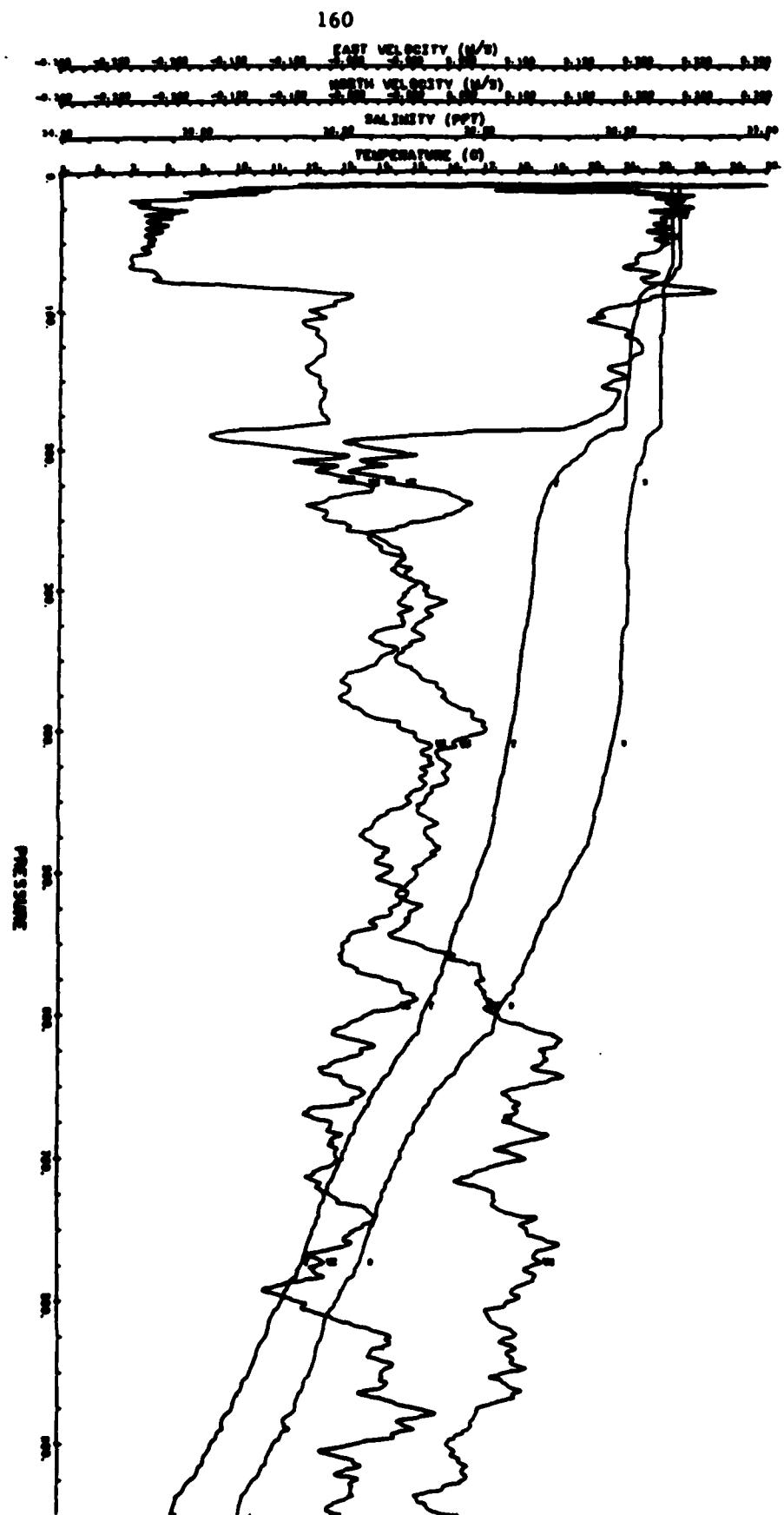


Figure XV-4: Profiles of Temperature (deg. C), Salinity (ppt), and the North and East components of velocity (m/s), for Dive 34.

Participant Summary:**XVI. EPSONDE Microstructure Profiling During FASINEX**
N. S. Oakey, Bedford Institute of Oceanography**Project Objectives:**

The FASINEX cruise of the R/V ENDEAVOR provided an opportunity to examine the spatial and temporal variability of microstructure in the upper few hundred meters of an oceanic front in response to atmospheric forcing. Data are to be analyzed to provide estimates of vertical eddy diffusivity, dissipation and χ_T as a function of depth at, and near, a front.

Vessel: R/V ENDEAVOR, February 11-March 10, 1986

Scientific Party Involved:

Dr. N. S. Oakey	Chief Scientist
Mr. P. Pozdnekoff	Technician
Mr. B. Wile	Technician

Narrative:

This cruise used the tethered free fall instrument EPSONDE developed at the Bedford Institute of Oceanography by N. Oakey over the past three years. EPSONDE has been used in three major cruises prior to FASINEX, but was upgraded to include a CTD for the FASINEX study. EPSONDE consists of a tethered free fall vehicle, handling system and computer data logger used to measure microstructure to dissipation scales. The instrument has two airfoil shear probes, a thin film thermometer, fast thermistor (FP07), a CTD using a strain gauge pressure transducer, Neil Brown 3 cm conductivity cell and an FP14 thermistor. A variety of engineering measurements, such as tilt, are also recorded. For the microstructure sensors, both the time varying and the derivative signal are recorded to increase dynamic range. Sensor channels are multiplexed at a rate of 256 HZ and submultiplexed at 1/2 speed or 1/8 speed, depending on the sensor capability. A 12-Bit digitizer is used with range selection for conductivity, temperature and pressure. A USART pair is used to telemetry the data (at 38.4 K baud) from the EPSONDE profiling vehicle through a Kevlar four conductor wire to the surface. A deck unit reconstructs parallel data words with ID bits and synchronizing bits for data logging on a computer. The deck unit also reconstructs analog signals for viewing in real time on multichannel analog recorders. The computer used to log data is an INTEL 310/40R, but during FASINEX it failed before the cruise started and an EAGLE-PC was used. The system also includes a winch, sheave-block, capstan system for handling the Kevlar wire without damage.

The equipment was loaded on the R/V ENDEAVOR in Norfolk, Virginia, February 3-5, 1986. Oakey, Pozdnekoff and Wile participated in the Norfolk-Bermuda transit, though no over-the-side tests were done. All systems were thoroughly bench tested and operational.

A major setback occurred in Bermuda when the principal computer (INTEL 310) failed. (It was repaired at the chip level aboard ship, but only very near the end of the experiment.) Data were recorded on an EAGLE-PC computer, but the quality of the data was reduced by signal loss during disk writes. Because of the small disk available, and difficulty in storing on streamer tapes, the quantity of data was also reduced.

A second setback occurred in the first station when the bilge keel intercepted EPSONDE and destroyed all sensors except conductivity. These were replaced with spares and the instrument fitted with a probe guard manufactured on the ENDEAVOR by the Chief Engineer. Thanks to his efforts, the danger of damaging probes was very reduced and, in fact, did not happen again. The guard ring, however, probably increased the vehicle vibration noise.

The only other problem experienced was related to slip rings and related data telemetry, which failed two or three times. This problem has never occurred before, and no spare slip rings were in our supplies which required rebuilding the ones we had. No problems were experienced with the winch, capstan or sheave-block.

During the experiment 39 stations were attempted with a total of 157 profiles, most to deeper than 200 m. These were at various positions with respect to the front, and they are listed in the EPSONDE STATION LOG (Table XIX-1) at the end.

For analysis, data were transferred from the streamer tape medium used on the EAGLE-PC to the streamer tape medium used on the INTEL 310 system. Because of the differences in formats, this could only be done efficiently by developing a special data link between the two machines. This job, done after the equipment returned to the Bedford Institute, required several weeks. There has been no attempt to date to do spectral analysis of the data to obtain ϵ and X_T . This will be done starting this fall.

Several stations were done simultaneously with the Fine and Microstructure Profiler (Schmitt and Toole), and it is hoped that data from both instruments may be compared.

The FASINEX study thus provided a significant number of microstructure profiles at and near an oceanic front. The data appears to be of high enough quality that meaningful estimates of ϵ and X_T may be made and used to examine frontal mixing processes.

Acknowledgements:

We would like to thank the Captain, Chief Engineer and crew of the R/V ENDEAVOR for their assistance during operations. A particular thank-you is also directed to the URI marine technicians, who were instrumental in repairing our computer.

Figure XVI-1 EPSONDE Profile Positions
Table XVI-1 EPSONDE Profile Information

FASINEX Endeavor 141 EPSONDE Profiles

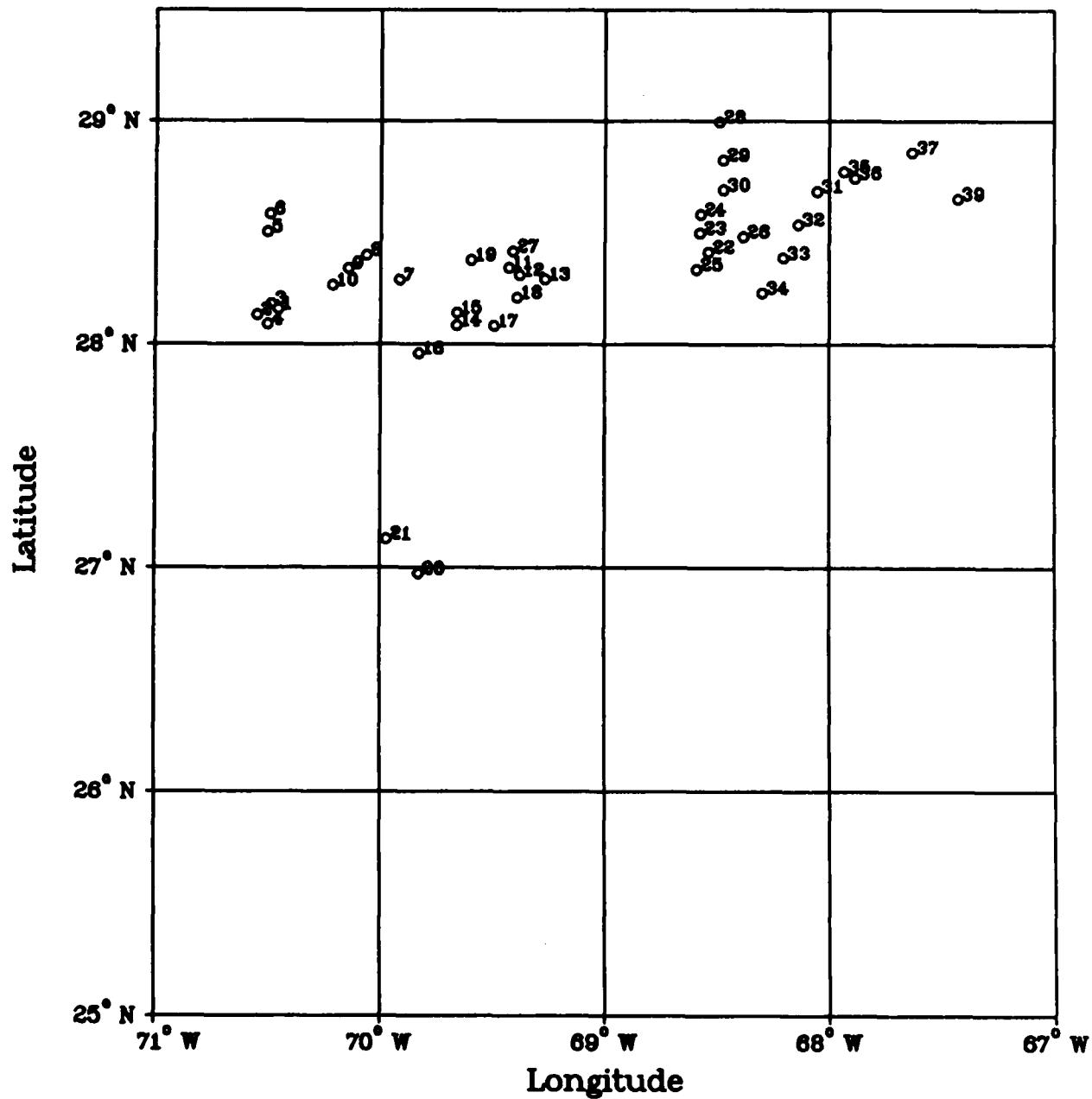


Figure XVI-1: EPSONDE Profile Positions.

TABLE XVI-1

EPSOMIDE STATION LOG

PASIMEX FEBRUARY-MARCH 1986

STATION	DAY	HOUR GMT	EN141 EVENT	LAT. ON	LONG. OW	PROFILES	DEPTH (m)	COMMENTS
1	46	1502	75	28°09.4'	70°27.3'	2	55	Broke sensors on Bilge keel.
2	47	1846	88	28°07.9'	70°33.0'	1	200	
3	48	1225	101	28°10.8'	70°29.2'	6	200	Noisy on way up.
4	48	1600	105	28°05.4'	70°30.2'	4	225	Noisy data.
5	49	1340	132	28°30.2'	70°30.3'	6	250	
6	49	2156	145	28°35.0'	70°29.6'	12	250	
7	52	1145	200	28°17.3'	69°54.9'	4	260	
8	52	2130	206	28°24.0'	70°03.7'	4	240	Cold side of front.
9	52	2250	207	28°20.4'	70°08.6'	4	240	At the front.
10	53	0032	209	28°15.9'	70°12.8'	4	240	Warm side of front.
11	53	1545	212	28°20.6'	69°25.6'	4	240	Cold side of front.
12	53	1745	215	28°18.6'	69°22.7'	4	240	In front.
13	53	2020	217	28°17.5'	69°15.9'	4	220	Warm side of front.
14	54	1145	225	28°05.1'	69°39.6'	8	240	Warm side of front.
15	55	0040	235	28°08.4'	69°39.5'	10	150	
16	55	1515	250	27°57.5'	69°49.6'	5	260	Long way from front.
17	55	2305	257	28°04.9'	69°29.6'	5	180	
18	56	0056	259	28°12.6'	69°23.4'	2	290	Lost signal during 2nd profile.
19	56	-						Aborted bad Slip Rings.
20	58	1310	380	26°58.4'	69°49.6'	2	250	Poor data; data lost.
21	58	2140	389	27°07.7'	69°58.2'	4	230	
22	59	1756	397	28°24.8'	68°32.2'	4	230	
23	59	1932	398	28°29.9'	68°34.6'	4	250	
24	59	2215	401	28°34.9'	68°34.4'	4	260	
25	60	0205	405	28°20.1'	68°35.4'	4	220	South on warm side of front.
26	60	1123	414	28°28.9'	68°23.0'	4	240	
27	60	1412	419	28°25.0'	68°24.5'	2	200	
28	62	1500	446	28°59.8'	68°29.4'	4	260	Cold side of front.
29	62	1700	448	28°49.5'	68°28.3'	4	240	Just on warm side of front.
30	62	1940	453	28°41.5'	68°28.3'	4	240	Warm side of front.
31	63	1350	466	28°41.1'	68°03.2'	4	240	Just on warm side of front.
32	63	1545	467	28°32.2'	68°08.3'	4	260	10 miles further into warm side.
33	63	1828	472	28°23.2'	68°12.2'	4	260	Warm side far from front.
34	63	2044	476	28°13.8'	68°17.8'	4	250	
35	64	1145	519	28°46.4'	67°56.0'	4	260	
36	64	1418	521 524 528	28°44.7'	67°53.1'	5	240	Drifting stn., 1 or 2 drops at 1 hr. spacing.
37	65	1255	-	28°51.6'	67°37.8'	1	200	Bad wire angle - astern
38	65	1325	-					Aborted too near ship.
39	65	2230	552	28°39.1'	67°25.7'	1	240	Aborted, wire astern.

Participant Summary:**XVII. The "WOTAN Drifter"**
Sven Vagle, IOS, Canada

This part of FASINEX has to be described as a complete success even though we had some minor technical problems. During the four weeks on the R/V ENDEAVOR we had twelve deployments with an average deployment time of seven hours, which is well over the number of hours we had been allocated before the cruise. We had one deployment at the front, four deployments on the north (cold) side, six deployments on the south (warm) side of the front, and one deployment at $26^{\circ} 52.4'N$, $69^{\circ} 44.1'W$ near the FASINEX mooring containing a 13 channel WOTAN instrument.

We experienced a wide range of weather conditions. During the time the drifter was deployed we had weather conditions ranging from calm sea, no wind, to wind speeds reaching 15 m/s and quite high seas. The amount of precipitation was not as much as one would have hoped but we should have some data from periods when it was raining.

We obtained acoustic backscatter data using four different transducers (28 kHz, 50 kHz, 88 kHz and 200 kHz) from a depth of 24 meters looking up. In addition to this we recorded the ambient sound with two different instruments. One was a broad band ambient sound instrument recording continuously the whole frequency band from 100-40,000 Hz. The other instrument was a Sea Data Corporation WOTAN (Wind Observation Through Ambient Noise) recorder recording 13 channels with narrow band filters entered at 3.0, 4.3, 5.3, 6.5, 8.0, 9.3, 10.8, 12.5, 14.5, 16.8, 19.5 and 25.0 kHz with a sampling interval of 0.87 second. We have more than 75 hours worth of, mostly good, data.

We observed bubble clouds reaching as far as 8-10 meters below the surface during the most windy conditions (12-15 m/s).

As far as the surface wave spectrum is concerned it looks like we might be able to get some useful information out of our echo-sounder data. A computer program has been written to model the vertical motion of the instruments at the end of the rubber cord. The preliminary results suggest that the instrument motion is very small compared to the surface wave motion. Therefore we may be able to obtain wave spectra estimates.

We look forward to the possibility of comparing our measurements with the directional wave spectra obtained by one of the aircraft.

Figure XVII-1
Table XVII-1**WOTAN Deployment Positions**
WOTAN Deployment/Recovery Information

FASINEX Endeavor 141 WOTAN Deployments

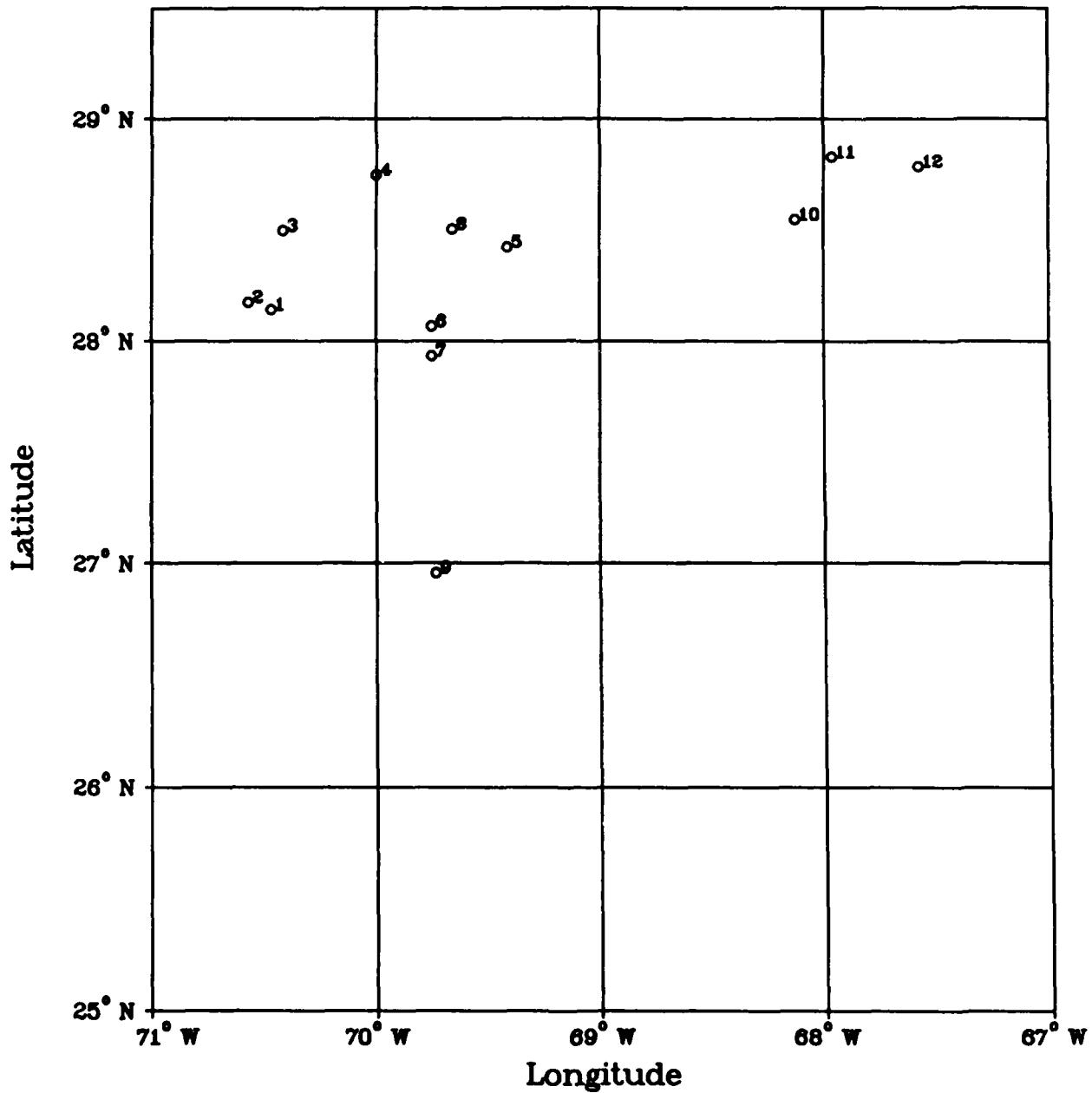


Figure XVII-1: WOTAN Deployment Positions.

TABLE XVII-1

Deployment Number	Date	Deployment Position Latitude	Deployment Position Longitude	Recovery Position Latitude	Recovery Position Longitude	Deployment Time(GMT)	Recovery Time(GMT)	Drift Dir.	Drift Dist.	Drift Speed
1 #	15/2	28 08.5N	70 28.1W	28 09.1N	70 15.8W	14:35	23:05	087°	11 nm	1.34 kn.
2 \$	17/2	28 10.4N	70 34.2W	28 11.2N	70 36.6W	11:37	19:43	294°	2.3nm	0.28 kn.
3 *	18/2	28 29.8N	70 24.9W	28 31.7N	70 24.4W	12:49	21:05	012	2.0	0.24
4 *	20/2	28 44.9N	70 00.1W	28 43.4N	69 54.1W	13:41	20:53	106	5.4	0.76
5 *	22/2	28 25.3N	69 24.8W	28 27.2N	69 22.5W	15:06	23:25	045	2.7	0.33
6 \$	23/2	28 04.0N	69 45.1W	28 00.5N	69 36.0W	11:11	22:50	114	8.4	0.72
7 \$	24/2	27 56.0N	69 45.2W	27 52.7N	69 43.2W	13:28	19:45	151	3.7	0.59
8 *	25/2	28 30.2N	69 39.6W	28 25.4N	69 37.5W	13:21	17:51	155	5.3	1.18
9 %	27/2	26 57.4N	69 44.1W	28 58.6N	69 42.6W	11:26	18:10	048	1.8	0.31
10\$	4/3	28 32.8N	68 07.6W	28 33.6N	68 03.5W	17:10	00:50	076	3.7	0.49
11\$	5/3	28 49.8N	67 57.8W	28 47.0N	67 47.8W	13:35	20:35	107	9.2	1.31
12\$	6/3	28 47.2N	67 34.7W	28 40.6N	67 27.6W	15:35	21:42	136	9.1	1.52

General information about the drifter. Deployments marked with a # were deployments at the front. Deployments marked with a \$ were at the warm(south) side of the front, and deployments marked with a * were at the cold(north) side of the front. The deployment marked with a % (Number 9) was a deployment close to a FASINEX mooring containing a WOTAN instrument.

Acknowledgements

The work done on these cruises was successful, in part, due to the cooperation and skill of the crew of R/V OCEANUS and R/V ENDEAVOR. Funding for the work summarized here was provided by the Office of Naval Research, Contract N00014-84-C-0134 (R. Weller), Contract N000014-85-C-0104 (L. Regier and R. Davis), Contract N00014-86-G-0023 (R. Pollard), Contract N00014-86-WR-24027 (K. Davidson) and by the National Science Foundation, Contract NSF:OCE 86-015336 (R. Schmitt and J. Toole).

We thank Paul Eden who assisted us throughout the cruises with the Applied Technology Satellite (ATS) system. His help and input, almost daily, allowed for a successful communication link for KNORR during the Phases One and Three mooring cruises and between the ships and the Bermuda Biological Station office, where the aircraft scientists were able to pass their flight schedules and observations to the ships during Phase Two.

Cdr. Frank Bub handled the weather forecasting for the aircraft and ships during Phase Two. Some data were input from the ships and along with the Naval Airstation meteorological data, Cdr. Bub prepared a briefing each evening for the aircraft scientists and sent out a report on telemail to the ships. His time and effort was greatly appreciated.

Our thanks to Mary Ann Lucas for her assistance with many tedious aspects of the typing, editing and data processing of the data sets for all the field work included in this document and for her help with the final preparation of this document.

Appendix A: FASINEX Julian Day Conversion Table

The FASINEX field program began in January 1986 and concluded late in June 1986. Several of the data sets have a Julian Day time base. This table is a conversion table from calendar days to Julian Days.

Jan 1 - 001	Feb 1 - 032	Mar 1 - 060	Apr 1 - 091	May 1 - 121	Jun 1 - 152
2 - 002	2 - 033	2 - 061	2 - 092	2 - 122	2 - 153
3 - 003	3 - 034	3 - 062	3 - 093	3 - 123	3 - 154
4 - 004	4 - 035	4 - 063	4 - 094	4 - 124	4 - 155
5 - 005	5 - 036	5 - 064	5 - 095	5 - 125	5 - 156
6 - 006	6 - 037	6 - 065	6 - 096	6 - 126	6 - 157
7 - 007	7 - 038	7 - 066	7 - 097	7 - 127	7 - 158
8 - 008	8 - 039	8 - 067	8 - 098	8 - 128	8 - 159
9 - 009	9 - 040	9 - 068	9 - 099	9 - 129	9 - 160
10 - 010	10 - 041	10 - 069	10 - 100	10 - 130	10 - 161
11 - 011	11 - 042	11 - 070	11 - 101	11 - 131	11 - 162
12 - 012	12 - 043	12 - 071	12 - 102	12 - 132	12 - 163
13 - 013	13 - 044	13 - 072	13 - 103	13 - 133	13 - 164
14 - 014	14 - 045	14 - 073	14 - 104	14 - 134	14 - 165
15 - 015	15 - 046	15 - 074	15 - 105	15 - 135	15 - 166
16 - 016	16 - 047	16 - 075	16 - 106	16 - 136	16 - 167
17 - 017	17 - 048	17 - 076	17 - 107	17 - 137	17 - 168
18 - 018	18 - 049	18 - 077	18 - 108	18 - 138	18 - 169
19 - 019	19 - 050	19 - 078	19 - 109	19 - 139	19 - 170
20 - 020	20 - 051	20 - 079	20 - 110	20 - 140	20 - 171
21 - 021	21 - 052	21 - 080	21 - 111	21 - 141	21 - 172
22 - 022	22 - 053	22 - 081	22 - 112	22 - 142	22 - 173
23 - 023	23 - 054	23 - 082	23 - 113	23 - 143	23 - 174
24 - 024	24 - 055	24 - 083	24 - 114	24 - 144	24 - 175
25 - 025	25 - 056	25 - 084	25 - 115	25 - 145	25 - 176
26 - 026	26 - 057	26 - 085	26 - 116	26 - 146	26 - 177
27 - 027	27 - 058	27 - 086	27 - 117	27 - 147	27 - 178
28 - 028	28 - 059	28 - 087	28 - 118	28 - 148	28 - 179
29 - 029		29 - 088	29 - 119	29 - 149	29 - 180
30 - 030		30 - 089	30 - 120	30 - 150	30 - 181
31 - 031		31 - 090		31 - 151	

Appendix B: Mooring Designations

The FASINEX moorings have several different designations. FASINEX identified each mooring with a letter and number. There was a WHOI Buoy Group designation. There was a buoy identifier. And there was an ARGOS transmitter number. Of the eleven moorings, there were three different types of mooring. The following table summarizes the above-mentioned information:

DESIGNATION	F1	F2	F3	F4	F5	F6	F7	F8	F9	F10	F12
FASINEX											
WHOI Mooring	829	845	-	846	-	847	-	848	-	849	830
Buoy Identifier		A	PGH-1	C	PGH-2	S	PGH-3	E	PGH-4	D	
ARGOS #	6430			6432		6431		6434		6433	
Moorings Type	subsurface	surface	near-surface	surface	near-surface	surface	near-surface	surface	near-surface	surface	subsurface
Latitude	27°58.90	27°18.95	27°05.34	27°05.35	26°58.58	27°12.59	27°12.53	26°58.66	27°05.45	27°19.63	25°29.10
Longitude	69°58.80	70°05.86	69°42.73	69°50.30	69°50.40	69°58.48	69°51.03	69°43.19	69°50.33	69°42.52	70°00.70
Deployment	28 Oct 84 2238	15 Jan 86 2020	17 Jan 86 1811	16 Jan 86 1947	16 Jan 86 1840	26 Jan 86 1713	28 Jan 86 1832	27 Jan 86 1748	29 Jan 86 1806	1 Feb 86 1801	29 Oct 84 1724
Recovery	18 Jun 86 1721	14 Jun 86 0950	16 Jun 86 1352	15 Jun 86 2133	16 Jun 86 2011	14 Jun 86 2151	17 Jun 86 1108	15 Jun 86 1333	Lost	10 Jun 86 0543	13 Jun 86 1957
Data Days	598	150	150	150	149	139	139	139	0	103	592
Instrument Depths		met	20	met	20	met	20	met	20	met	
		10		10		10		10		10	
		20		20		20		20		20	
		30		30		30		30		30	
		40		40		40		40		40	
		50		50		50		50		50	
		120	↓	120	↓	120	↓	120	↓	120	
	225	160	200	160	200	160	200	160	200	160	225
	325										325
	550										550
	625										625
	700	700		700		700		700		700	700
	1100			1000				1000			1100
	4100			4000				4000			4100

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REPORT DOCUMENTATION PAGE		1. REPORT NO. WHOI-86-36	2.	3. Recipient's Accession No. AD-A177776
4. Title and Subtitle FASINEX Frontal Air-Sea Interaction Experiment (January - June 1986) Cruise Summaries for FASINEX Phase Two R/V OCEANUS Cruise 175 R/V ENDEAVOR Cruise 141		5. Report Date September 1986		
7. Author(s) Nancy J. Pennington, Robert A. Weller		8. Performing Organization Rep't. No. WHOI-86-36		
9. Performing Organization Name and Address Woods Hole Oceanographic Institution Woods Hole, Massachusetts 02543		10. Project/Tech/Work Unit No.		
		11. Contract(C) or Grant(G) No. (C) N00014-84-C-0134, NR 083-400		
12. Sponsoring Organization Name and Address Office of Naval Research		13. Type of Report & Period Covered Technical Report		
14.				
15. Supplementary Notes This report should be cited as: Woods Hole Oceanog. Inst. Tech. Rept. WHOI-86-36.				
16. Abstract (Limit: 200 words) The Frontal Air-Sea Interaction Experiment (FASINEX) was a study of the response of the upper ocean to atmospheric forcing in the vicinity of an oceanic front in the subtropical convergence zone southwest of Bermuda, the response of the lower atmosphere in that vicinity to the oceanic front, and the associated two-way interaction between ocean and atmosphere. FASINEX began in the winter (January 1986), concluded in the early summer (June 1986) and included an intensive period in February and March. The experiment took place in the vicinity of 27°N, 70°W where sea-surface-temperature fronts are climatologically common. Measurements were made from buoys, ships, aircraft and spacecraft. This report summarizes the shipboard work done on R/V OCEANUS and R/V ENDEAVOR during Phase Two, the dual ship/multi-aircraft measurement period. The two ships worked individually, jointly and as ground truth for the aircraft during the month. Each ship carried specialized instrumentation for measuring oceanographic and meteorological parameters. Information describing the sampling strategy, station positions and times are included. This report contains summaries of the data collected and some preliminary results.				
17. Document Analysis a. Descriptors 1. air-sea interaction 2. FASINEX 3. oceanic front				
b. Identifiers/Open-Ended Terms				
c. COSATI Field/Group				
18. Availability Statement: Approved for publication; distribution unlimited.		19. Security Class (This Report) UNCLASSIFIED	21. No. of Pages 174	
		20. Security Class (This Page)	22. Price	

END

4 - 87

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